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Modeling of Susceptor Assisted Microwave Heating in Domestic Ovens

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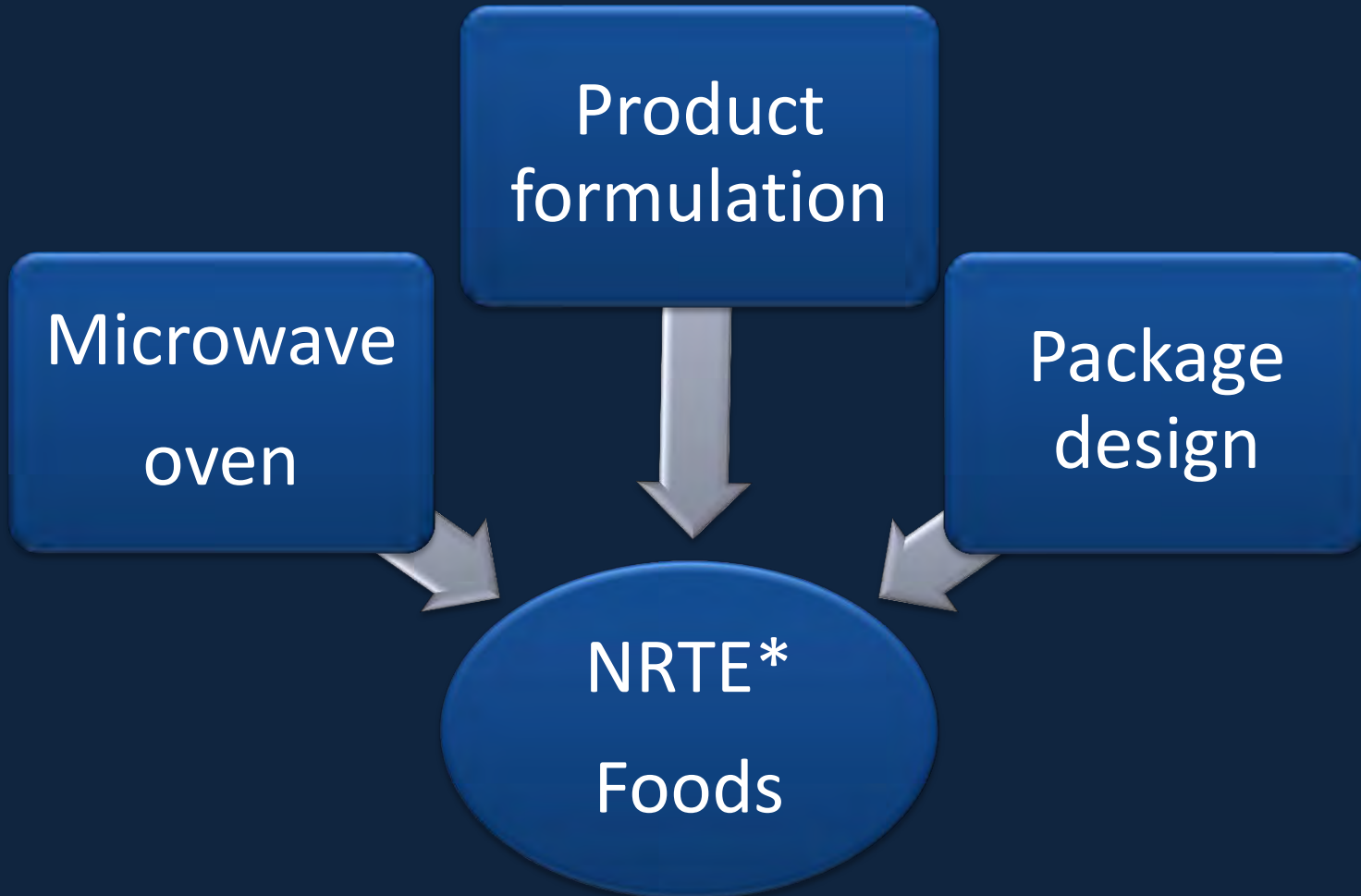
Session : Electromagnetic Heating

University of Nebraska - Lincoln

Outline

- Background
- Objective
- Simulation strategy
- Experimental setup
- Results
- Conclusion

Background



*Not - ready-to-eat foods which may contain foodborne pathogens

Why package is important in microwavable product?

- Extend the shelf life of the product
- Provide structural and holding facility
- Preferential heating
- Active package facilitates
 - crispiness
 - browning

Package type

- Passive package - PET
- Active package - Susceptor
- Shielding

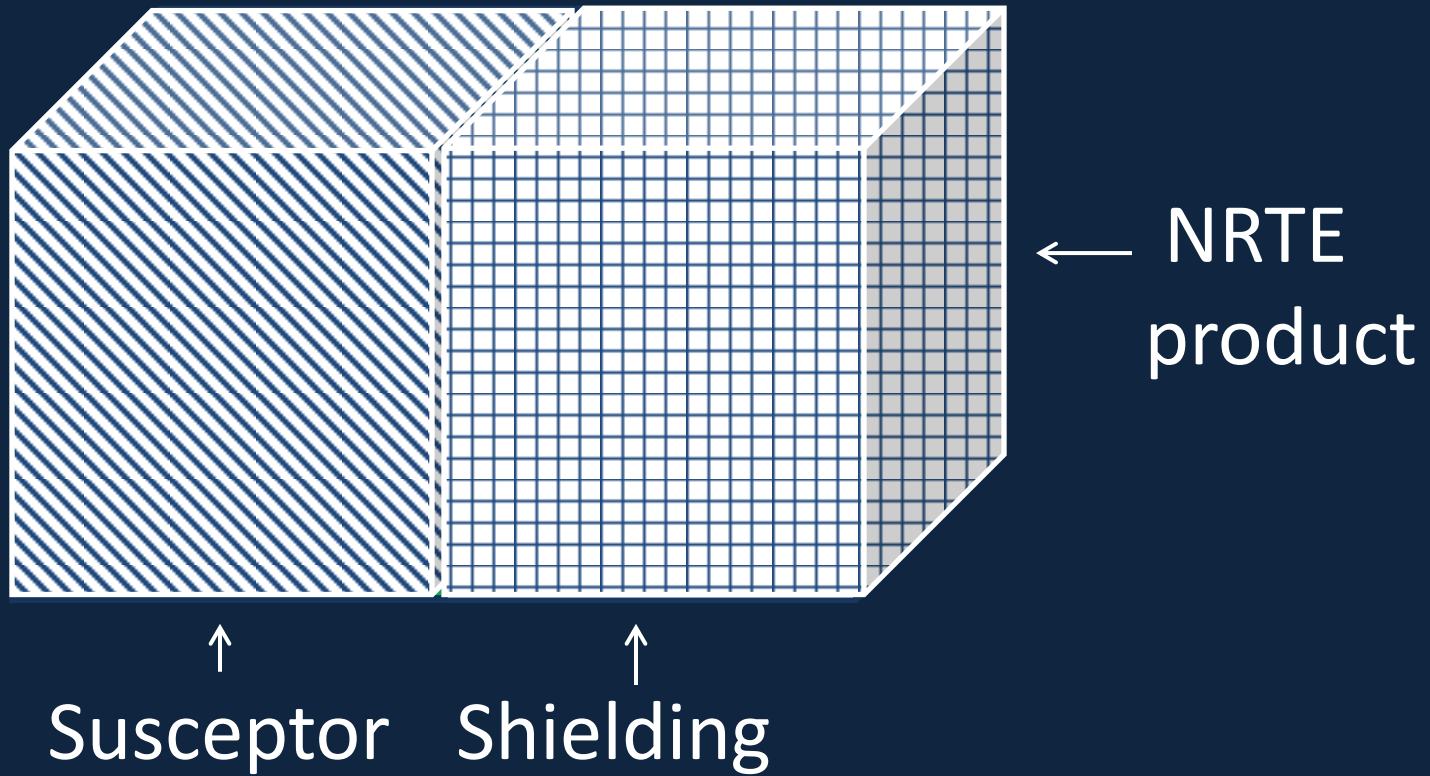


Passive package



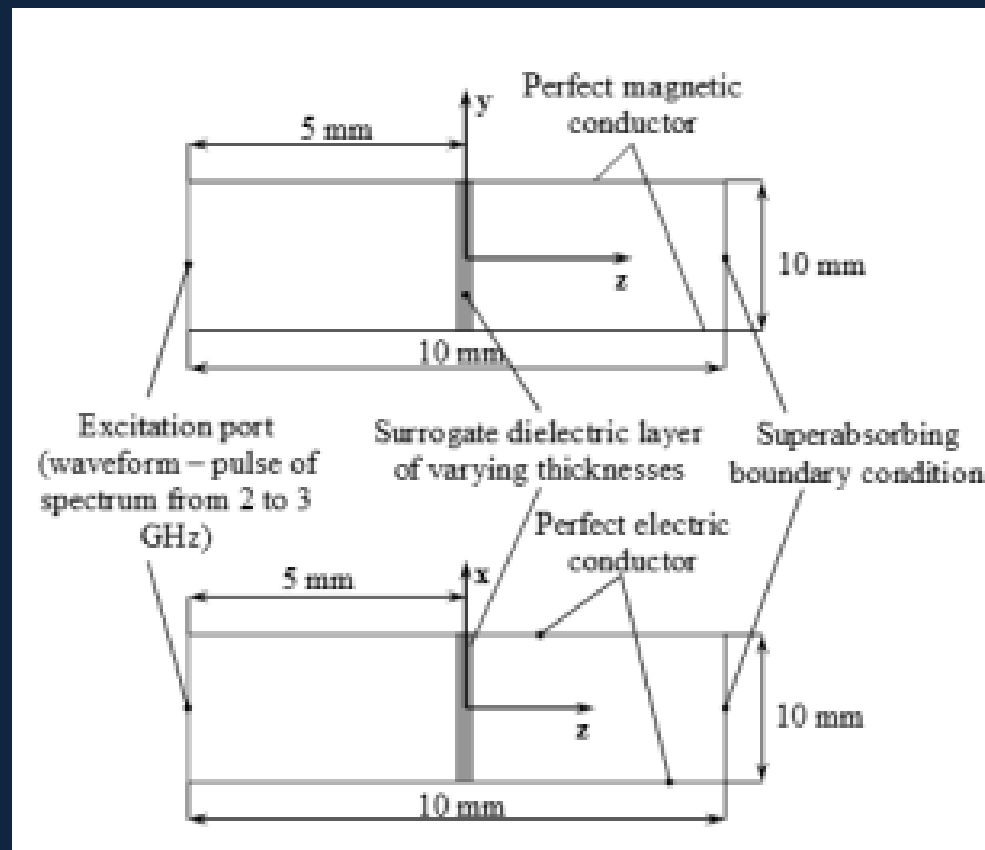
Active package

Susceptor & Shielding



Previous work

- Soltysiak et al. 2008 and Celuch et al. 2008



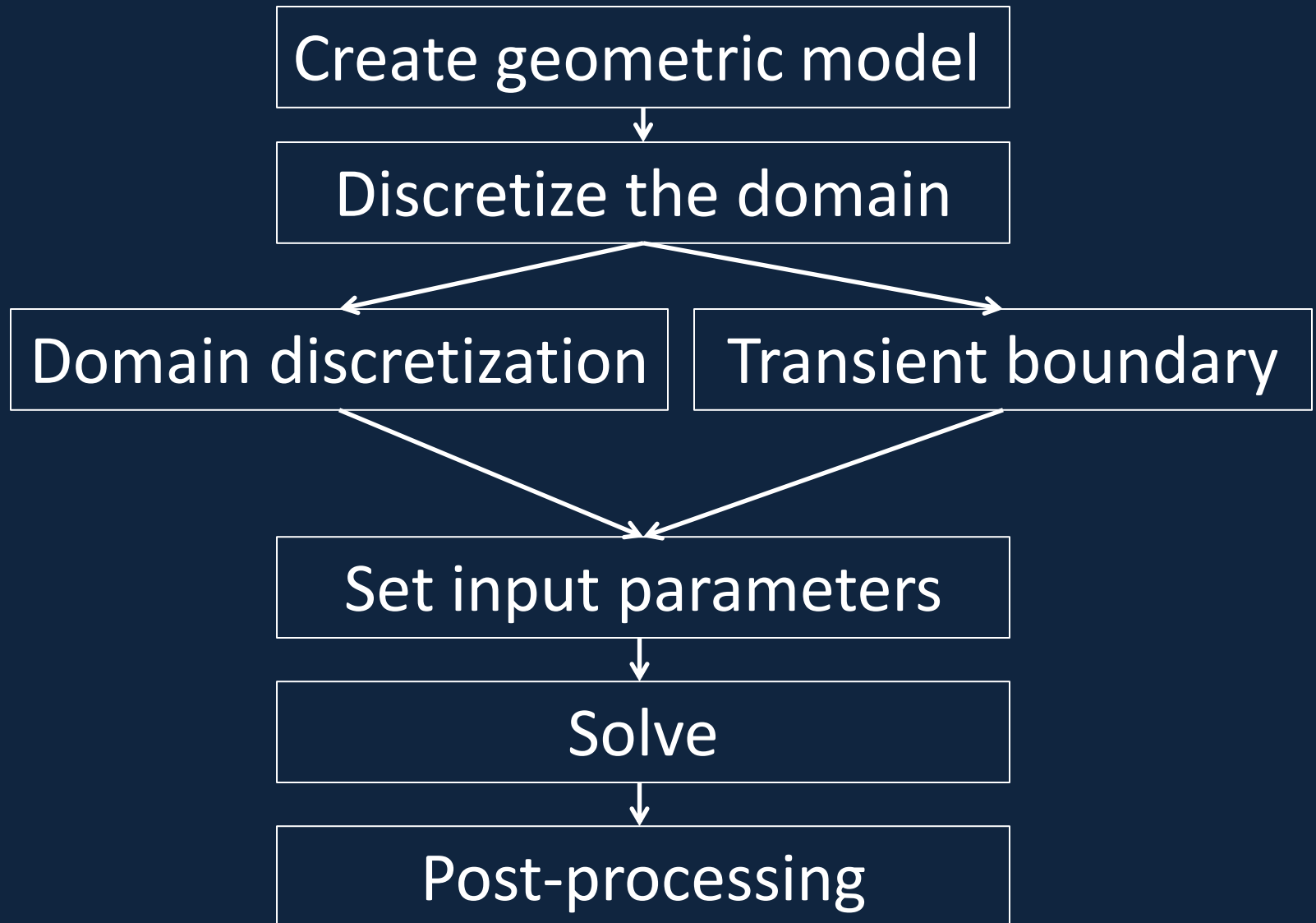
Objective

- Develop a computer model to simulate the interaction of food with an active package.

Specific objectives

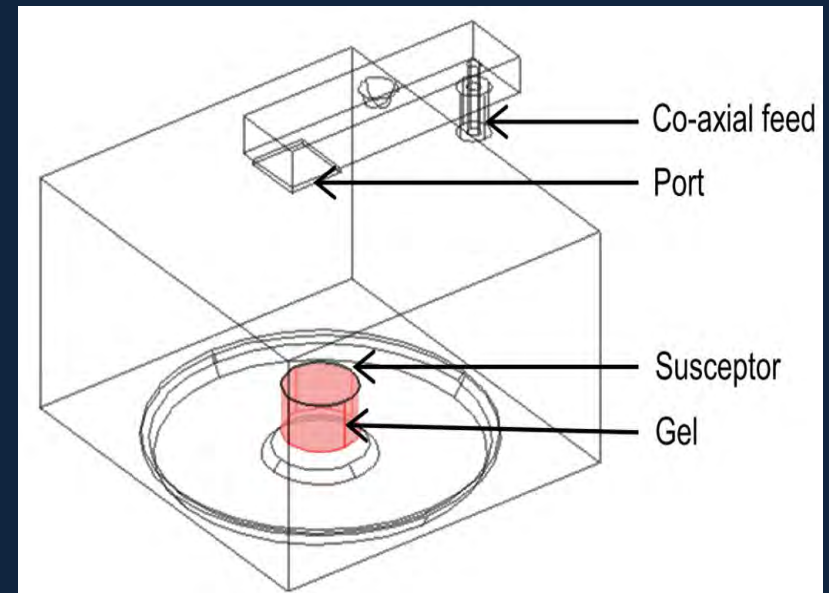
- Discretize the active package domain using two different methods and choose the best method based on accuracy and computational time.
- Validate the numerical model with an experimental condition.
- Explore the possibility of modeling shielding package.

Model development

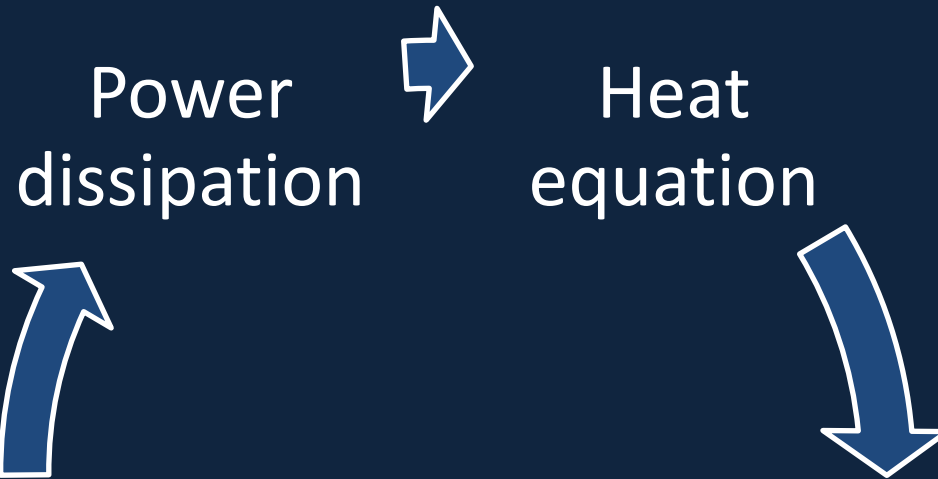


Geometric model

- 700 W microwave oven
- Cylindrical model food
- Susceptor on top of gel
- Co-axial feed



Solving coupled equation



Maxwell's equation

Temperature field

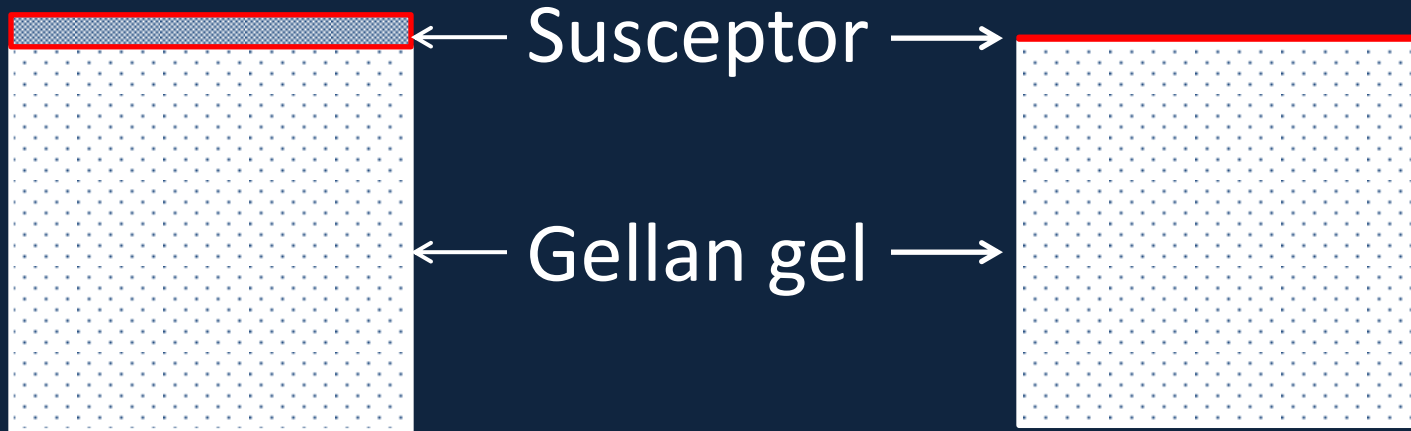
EM properties

$$\begin{aligned}\oint \mathbf{E} \cdot d\mathbf{A} &= \frac{q_{enc}}{\epsilon_0} \\ \oint \mathbf{B} \cdot d\mathbf{A} &= 0 \\ \oint \mathbf{E} \cdot d\mathbf{s} &= -\frac{d\Phi_B}{dt} \\ \oint \mathbf{B} \cdot d\mathbf{s} &= \mu_0 \epsilon_0 \frac{d\Phi_E}{dt} + \mu_0 i_{enc}\end{aligned}$$

$$\rho c_p \frac{\partial T}{\partial t} = \nabla \cdot (k \nabla T) + \mathcal{Q}$$

Discretization approach

- Domain discretization
- Transient boundary



$$J_S = \frac{(Z_S \mathbf{E}_{t1} - Z_T \mathbf{E}_{t2})}{Z_S^2 - Z_T^2}$$

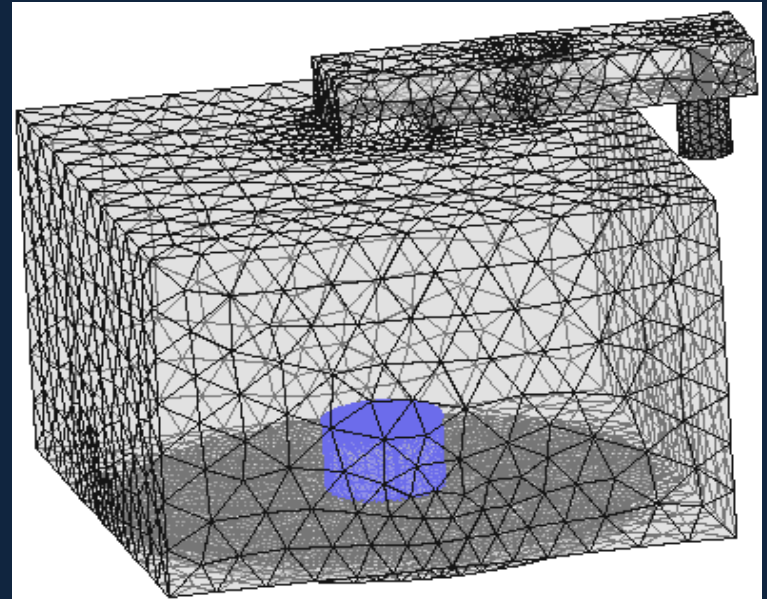
$$Z_S = \frac{-j\omega\mu}{\varphi} \frac{1}{\tan(\varphi d)}$$

$$Z_T = \frac{-j\omega\mu}{\varphi} \frac{1}{\sin(\varphi d)} \quad (6)$$

$$\text{where } \varphi = \omega \sqrt{\left(\epsilon + \frac{\sigma}{j\omega}\right)\mu}$$

Meshing scheme

- Domain discretization method
 ~ 366,000 elements
- Transient boundary method
 ~ 210,000 elements



Simulation strategy

- Radio frequency and heat transfer modules of **COMSOL Multiphysics v4.2**
- **Coupled approach** using segregated steps
- Parametric sweep of conductance from **0.001 to 0.1 S**
- Magnetron frequency of **2.45 GHz**

Experimental setup

- A homogeneous gellan gel cylinder was used
- Microwave heating for 30 s
- Turntable was stationary
- A susceptor film laminated with paper and PET was placed on top of gel

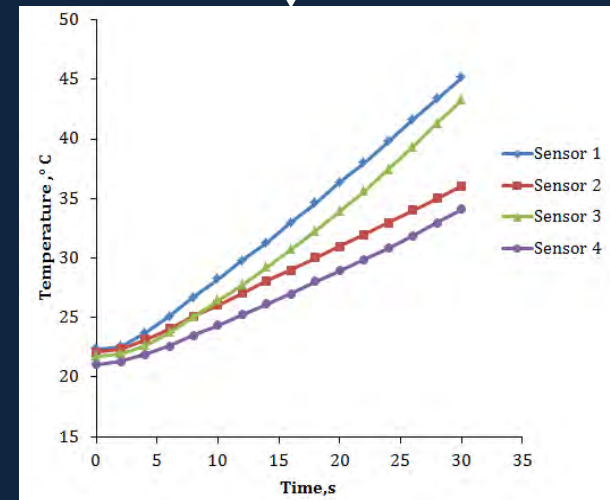
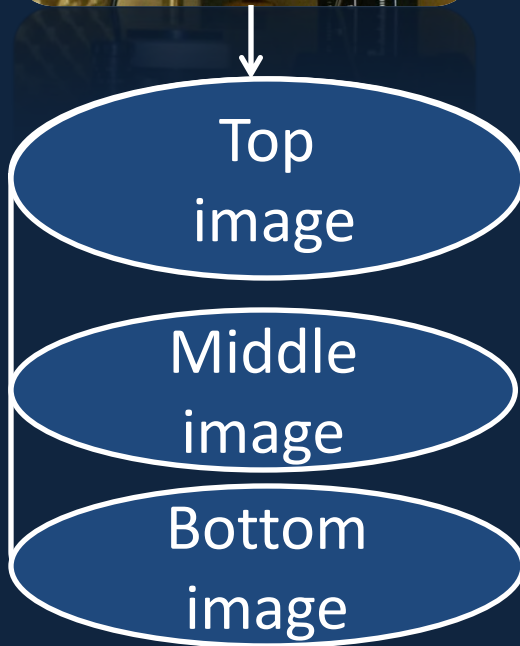


Shielding

- Food grade aluminum foil was used
- Conductance of the material was 0.1 S
- Simulation was performed using transient boundary condition

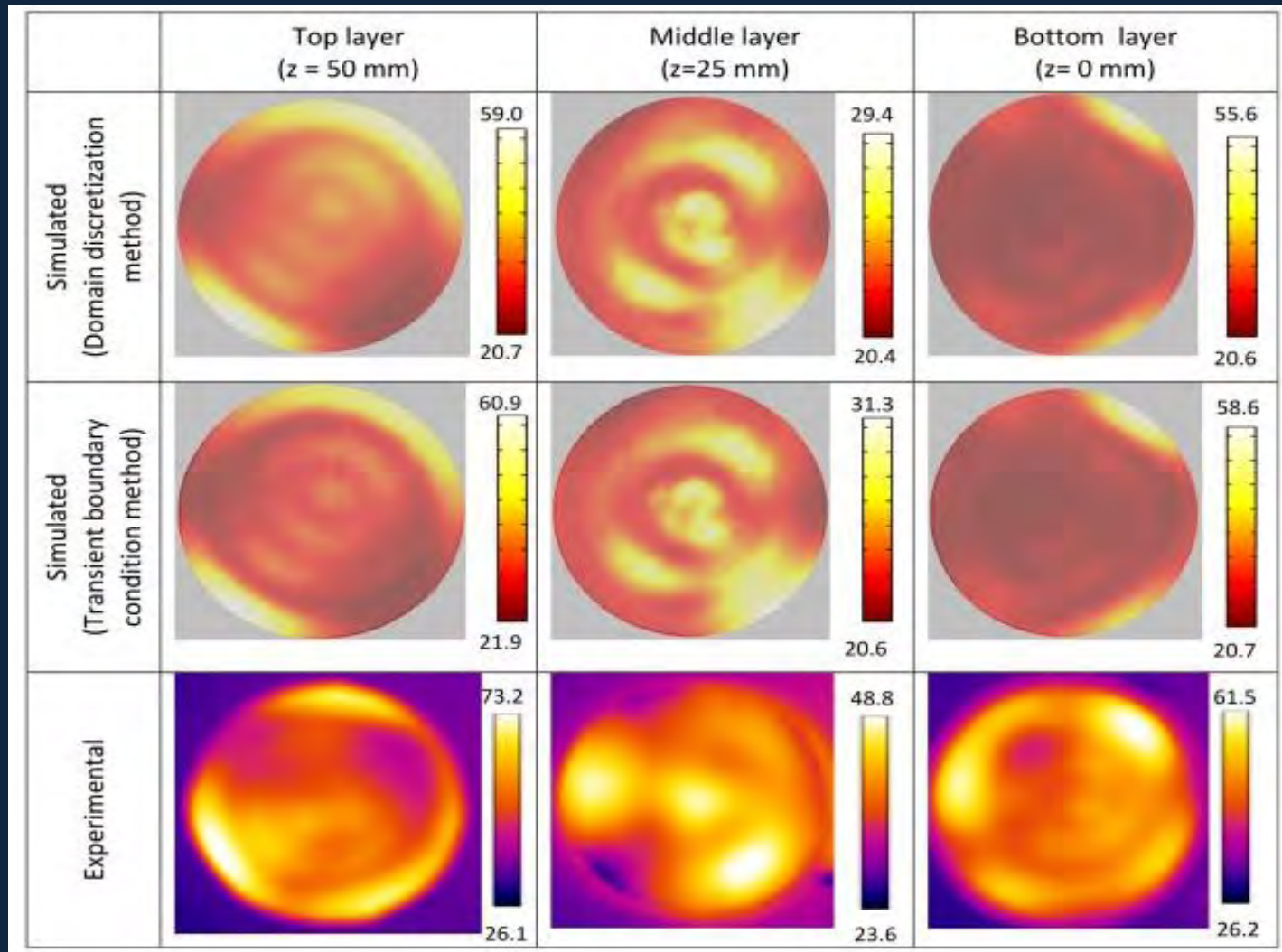


Temperature measurement

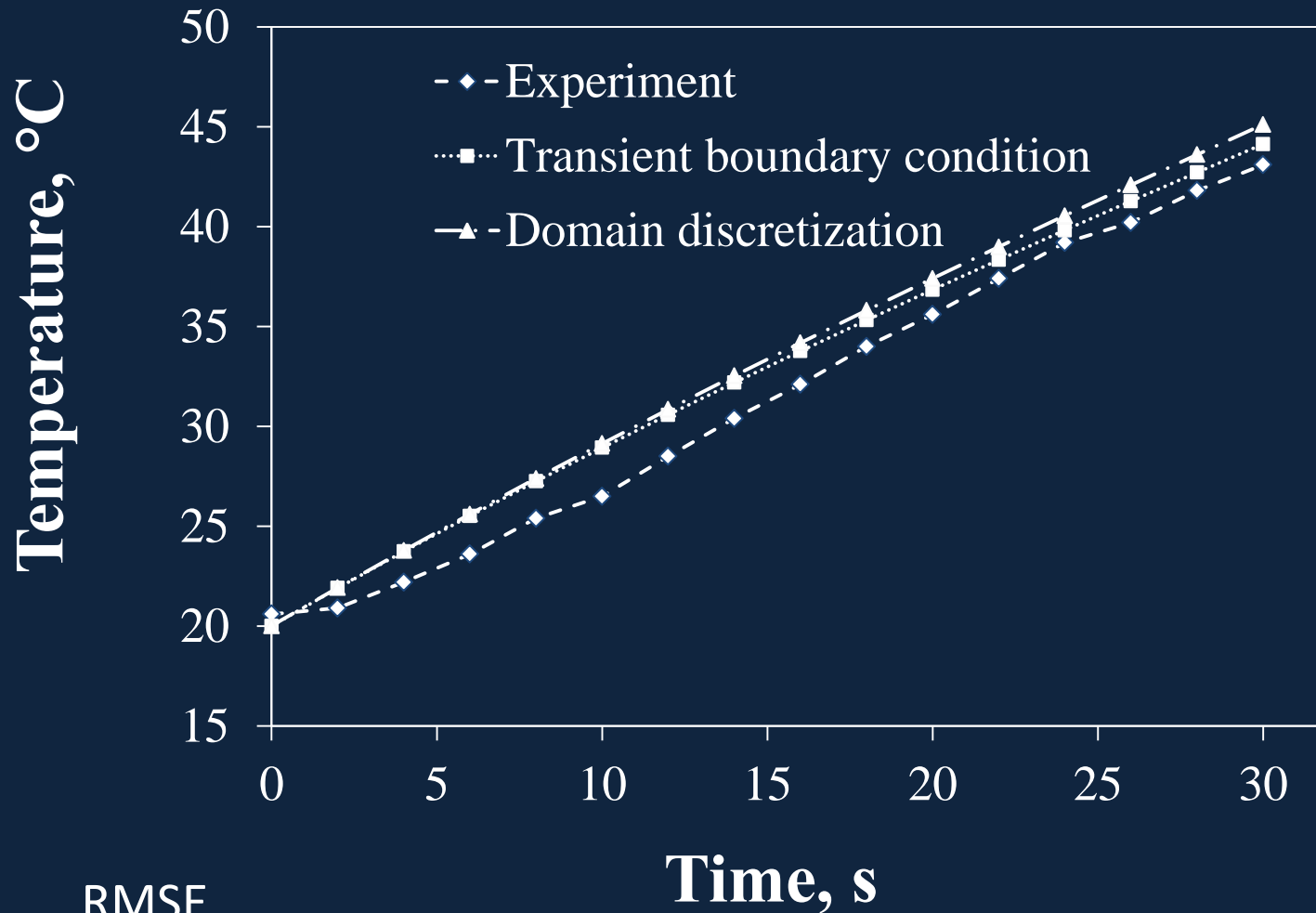


Results

Temperature profiles



Time-temperature profile



RMSE

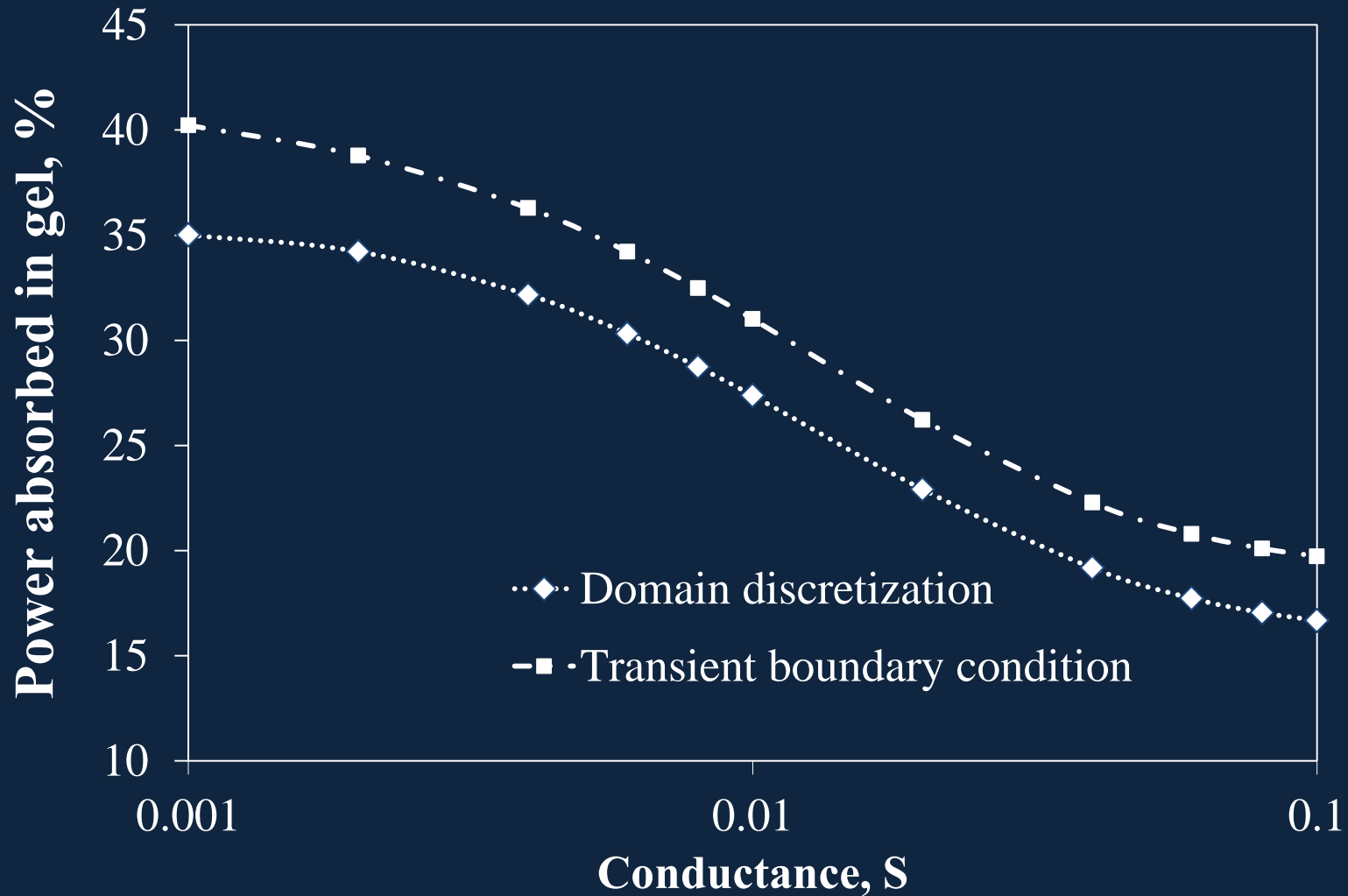
Transient boundary condition 1.51°C

Domain discretization 1.76°C

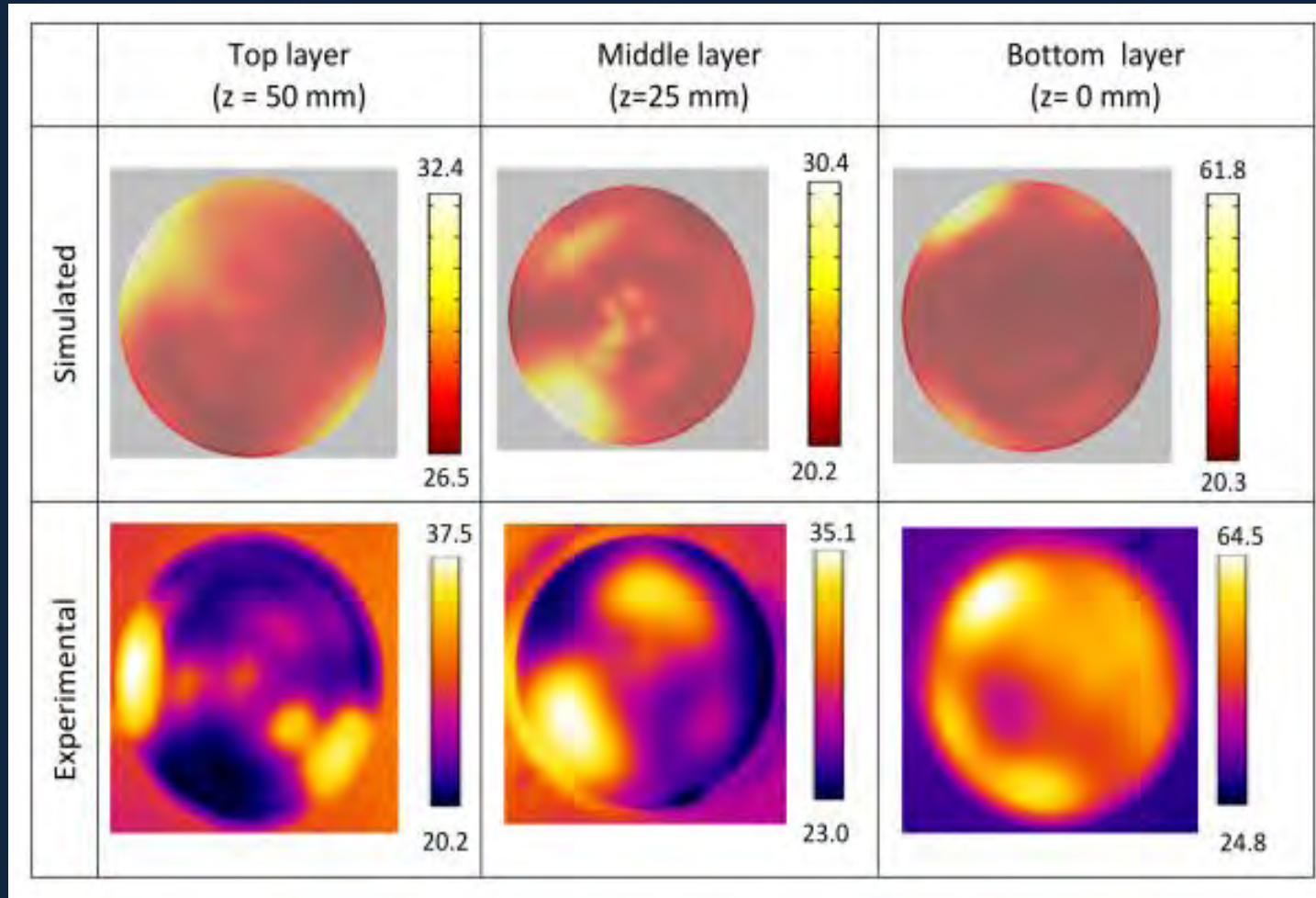
Comparison of approaches

	Transient boundary condition	Domain discretization method
Elements	Less elements	More elements
Computational time	~ 1 h	5 h
RMSE	1.51 °C	1.76 °C

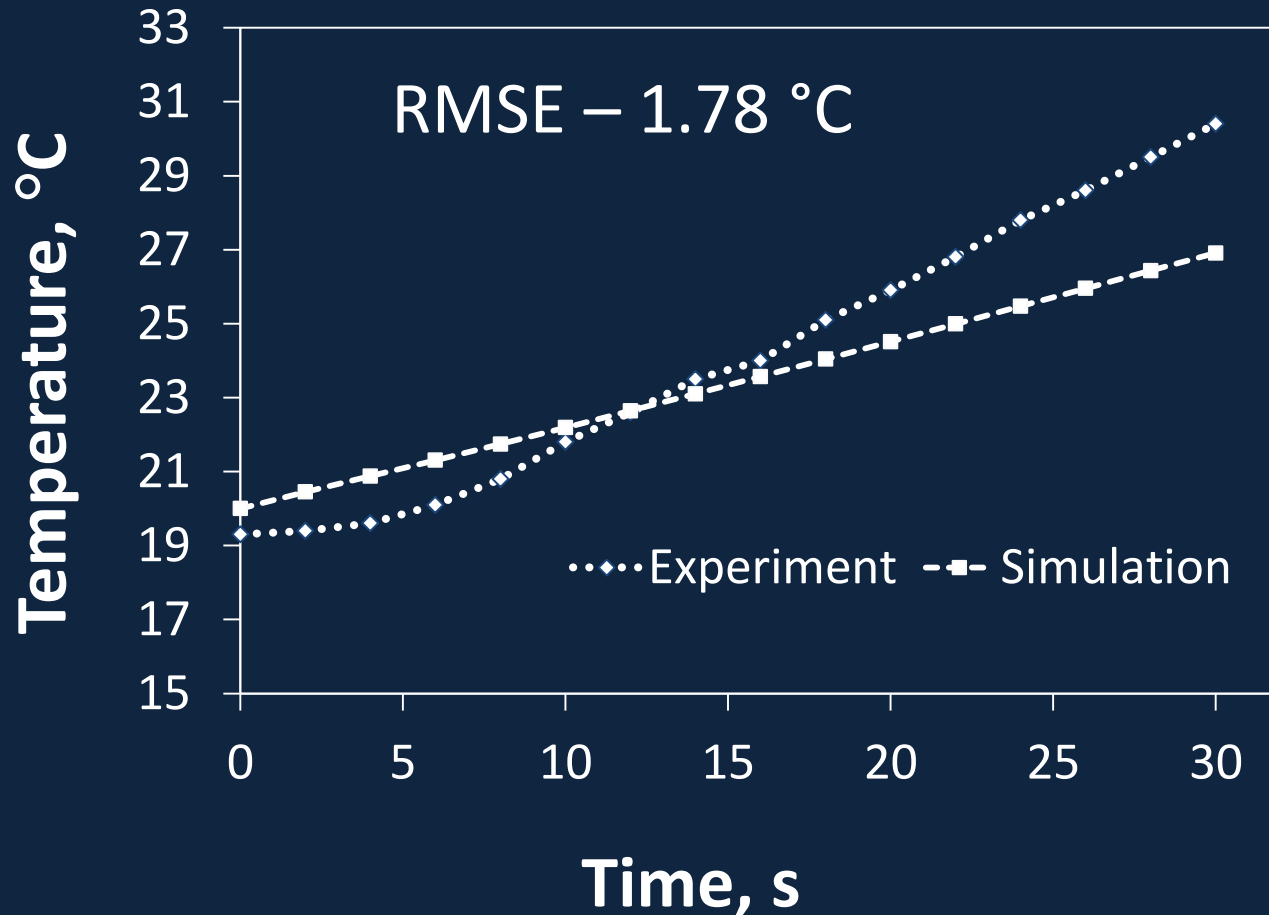
Effect of conductance



Shielding effect



Shielding effect – point temperature



Conclusion

- A simulation model was developed and validated for microwave interaction with model food and an active package
- Transient boundary condition method was best suitable one due to less computational time and better accuracy
- Model was also validated for shielding package

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