

# Numerical Simulation of Forward and Static Smoldering Combustion

Simcha L. Singer, Prof. William H. Green

MIT, Department of Chemical Engineering, 77 Massachusetts Ave., Cambridge, MA, 02139

**Introduction:** Understanding the formation and transport of toxins in cigarette smoke can be aided by numerical simulation. Smoldering combustion in a cigarette is comprised of many physical, chemical and morphological processes, all of which must be included in the model.

- Simulation domain encompasses tobacco rod, filter, paper and surrounding air
- Pyrolysis zone exist ahead of oxidation zone
- Transient problem due to alternation between static and forced smoldering (puffing)
- Most air enters at paper burn line
- Fundamentally a 2-D (or 3-D) problem
- Local thermal equilibrium between gas and solid does not always hold
- System of equations is highly nonlinear and possesses a range of time and length scales

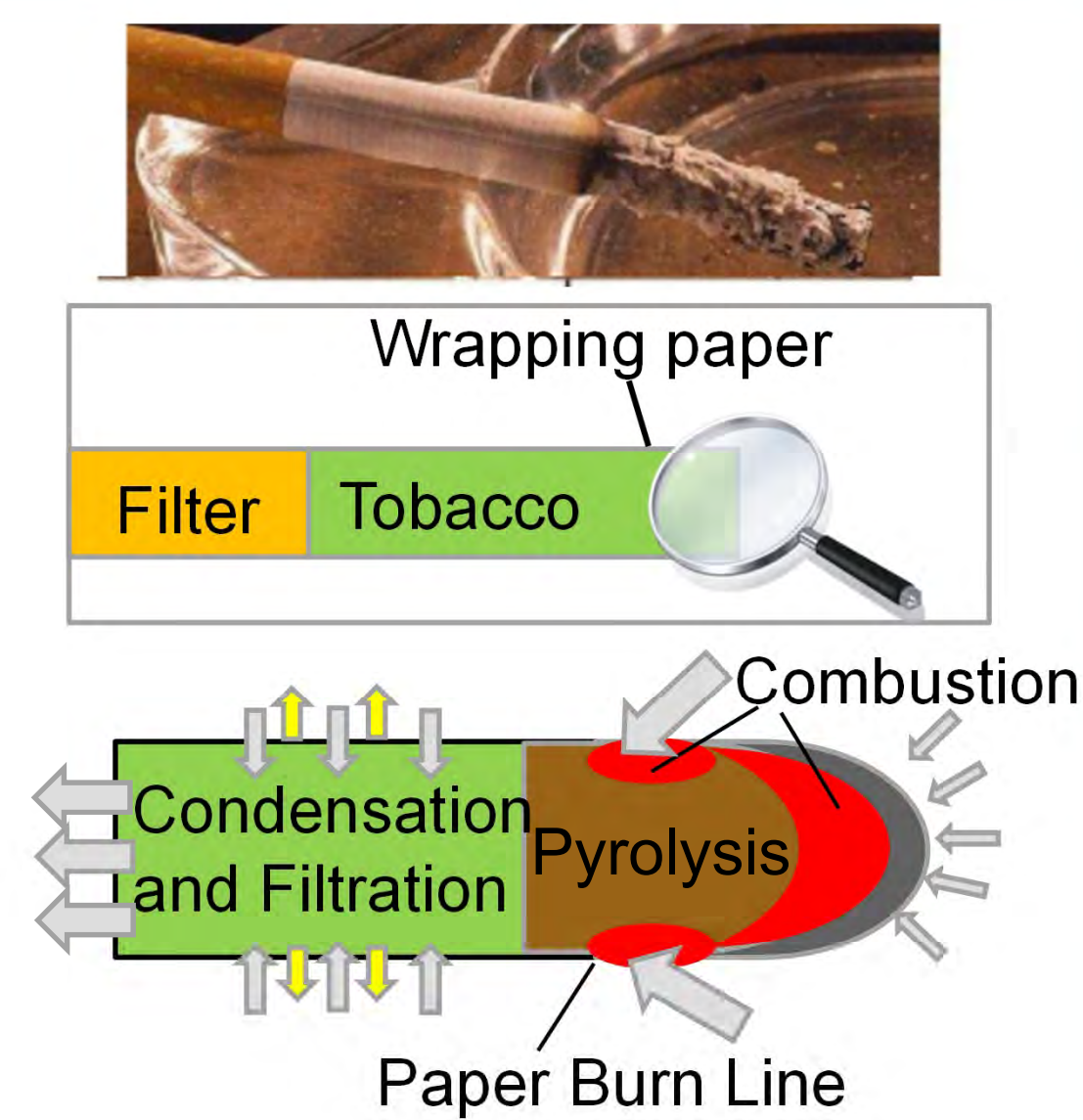


Fig 1. Schematic of burning cigarette showing convective and diffusive fluxes.

**Computational Methods:** A 2-D axisymmetric domain is employed, with conservation equations supplemented by expressions defining transport, thermodynamic and kinetic properties of the gas and the porous solid.

## Conservation Equations

Mass: 
$$\frac{\partial(\phi\rho)}{\partial t} + \nabla \cdot (\phi\rho\mathbf{u}) = \sum_j \sum_k v_{j,k} \mathcal{R}_k \equiv Q$$

Momentum: 
$$\frac{\rho}{\phi} \left( \frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \frac{\mathbf{u}}{\phi} \right) = -\nabla p - \left( \frac{\mu}{\kappa} + \frac{Q}{\phi^2} \right) \mathbf{u} + \nabla \cdot \left[ \frac{1}{\phi} \left\{ \mu (\nabla \mathbf{u} + (\nabla \mathbf{u})^T) - \frac{2}{3} \mu (\nabla \cdot \mathbf{u}) \mathbf{I} \right\} \right] + \mathbf{F}$$
  
For free flow region:  $\phi = 1$ ,  $Q = 0$  and  $\kappa \rightarrow \infty$

Thermal Energy (Gas): 
$$(\rho c_p)_{eff} \frac{\partial T_g}{\partial t} = \nabla \cdot (k_{eff} \nabla T_g) - \sum_j (N_j c_{p,j}) \cdot \nabla T_g + h_{g \rightarrow s} A_{g \rightarrow s} (T_s - T_g)$$

Thermal Energy (Solid): 
$$(\rho c_p)_{eff} \frac{\partial T_s}{\partial t} = \nabla \cdot (k_{eff} \nabla T_s) + \sum_k (-\Delta h_r \mathcal{R}_k) + h_{g \rightarrow s} A_{g \rightarrow s} (T_g - T_s)$$

Gas Species: 
$$\phi \rho \left( \frac{\partial w_j}{\partial t} + \mathbf{u} \cdot \nabla w_j \right) = -\nabla \cdot \mathbf{J}_j + \sum_k v_{j,k} \mathcal{R}_k - w_j Q$$
 Maxwell-Stefan model for diffusion

Solid Species: 
$$\frac{d\rho_{solid,i}}{dt} = \sum_k v_{i,k} \mathcal{R}_k$$

## Physics Interfaces Employed in Each Region

- **Reaction Engineering** synced with:
- **Free and Porous Media Flow:** Regions 1,2,3,4
- **Transport of Concentrated Species:** Regions 1,2,3,4
- **Heat Transfer in Fluids:** Regions 1,2,3,4
- **Heat Transfer in Solids:** Regions 2,3,4
- **Domain ODEs:** Region 2 (four tobacco components, two char components, etc.)
- **Domain ODE:** Region 4 (for paper permeability)

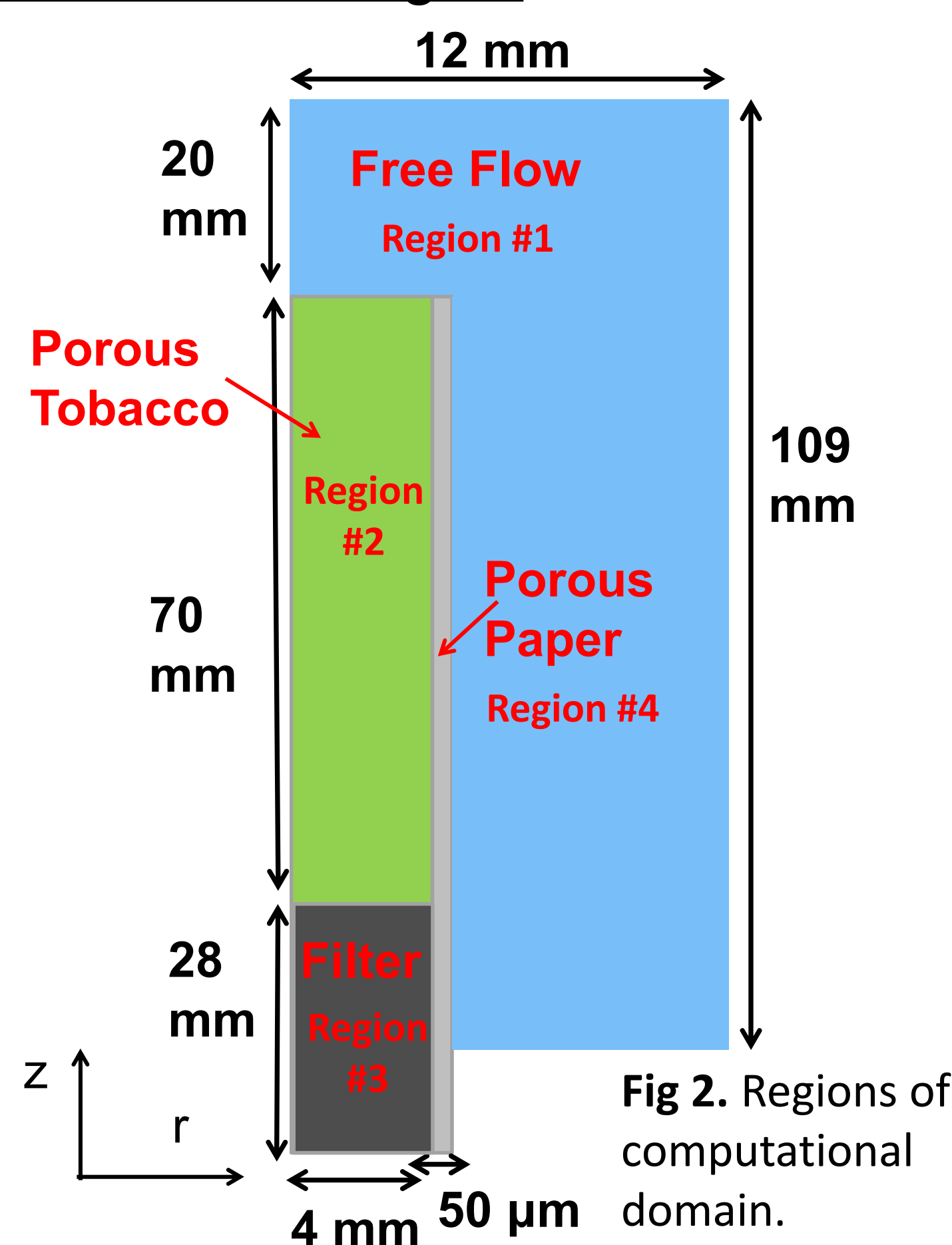


Fig 2. Regions of computational domain.

## Numerical Implementation

Mesh of 8341 elements is sufficiently refined

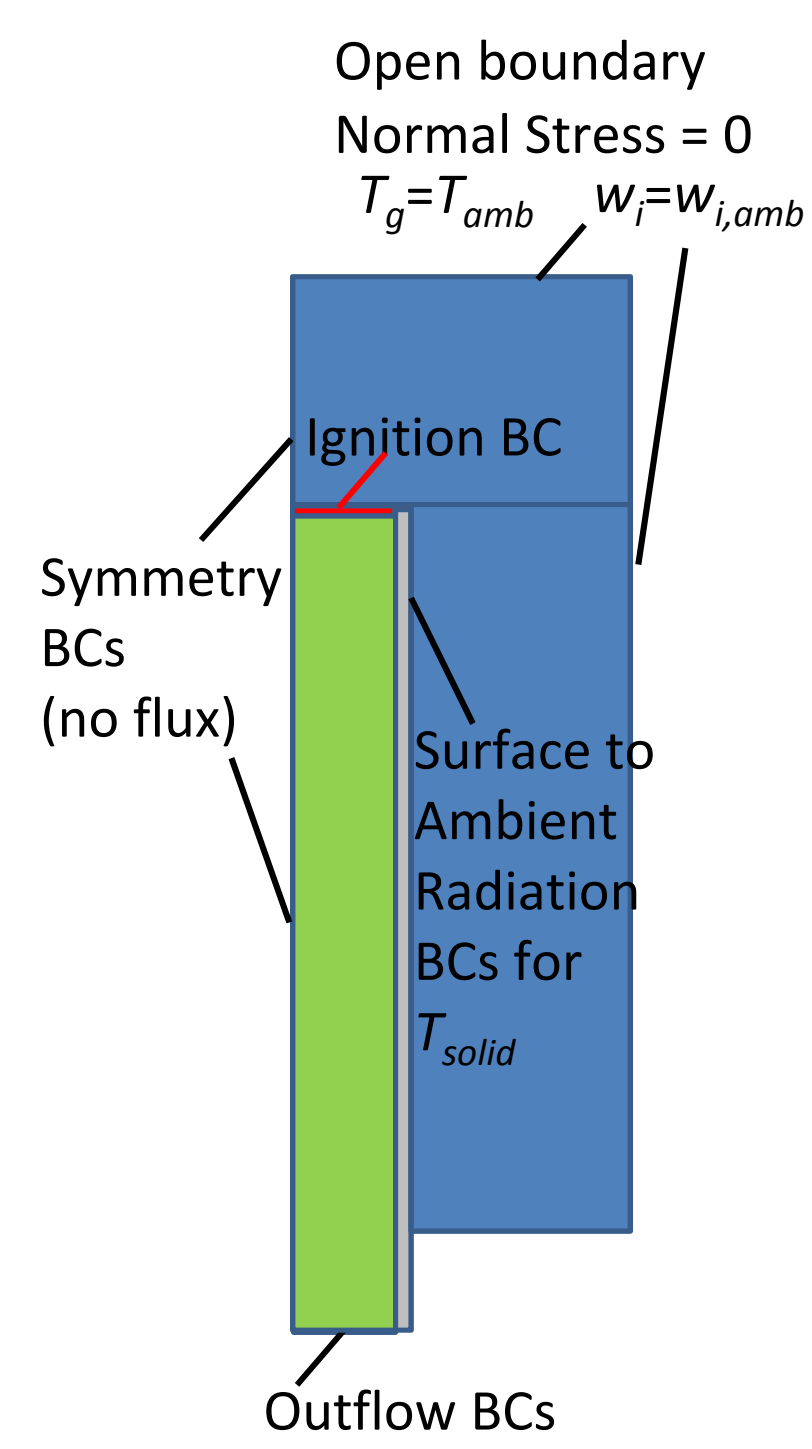
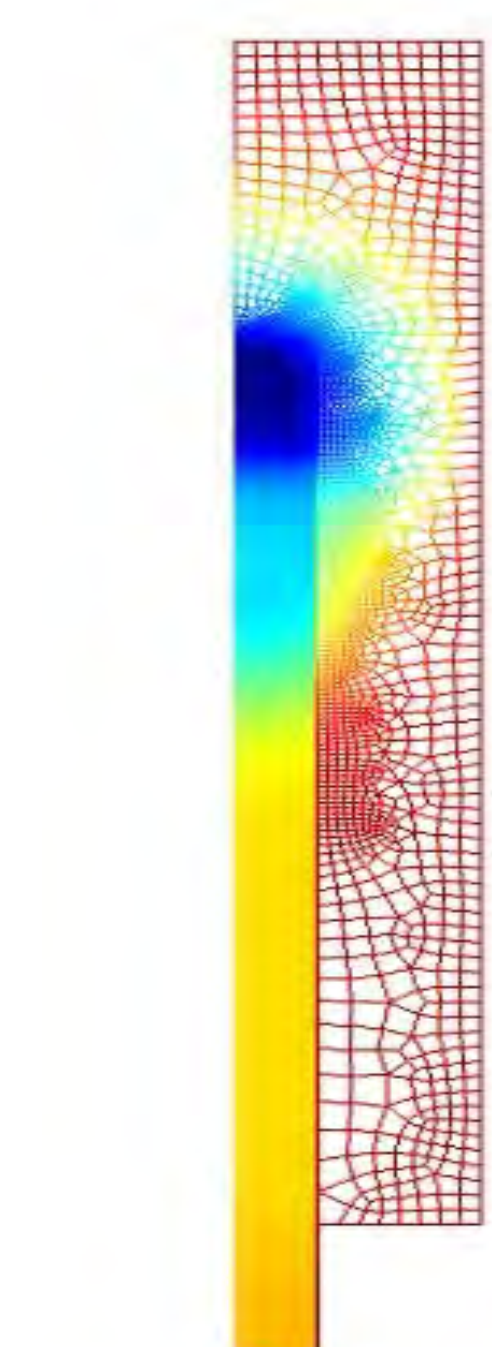


Figure 3. (a) Mesh and (b) Boundary conditions.

### Initial and Boundary Conditions

- Atmospheric ICs with zero velocity
- Puffing/smoldering transition via application of 17.5 cc flow rate at outlet for 2 [s] every 60 [s]

### Mesh and Elements Details:

- Non-uniform **mapped** mesh elements for porous regions (paper is *thin*!)
- Free quad elements in free flow region
- Most elements linear, although 2<sup>nd</sup> order shape functions also used
- **Solver Settings:**
- Time dependent BDF solver
- Newton's Method at each time step
- Direct MUMPS linear solver

**Results:** The agreement between simulation and experiment<sup>1,2</sup> is qualitatively and quantitatively reasonable.

## Solid and Gas Temperatures

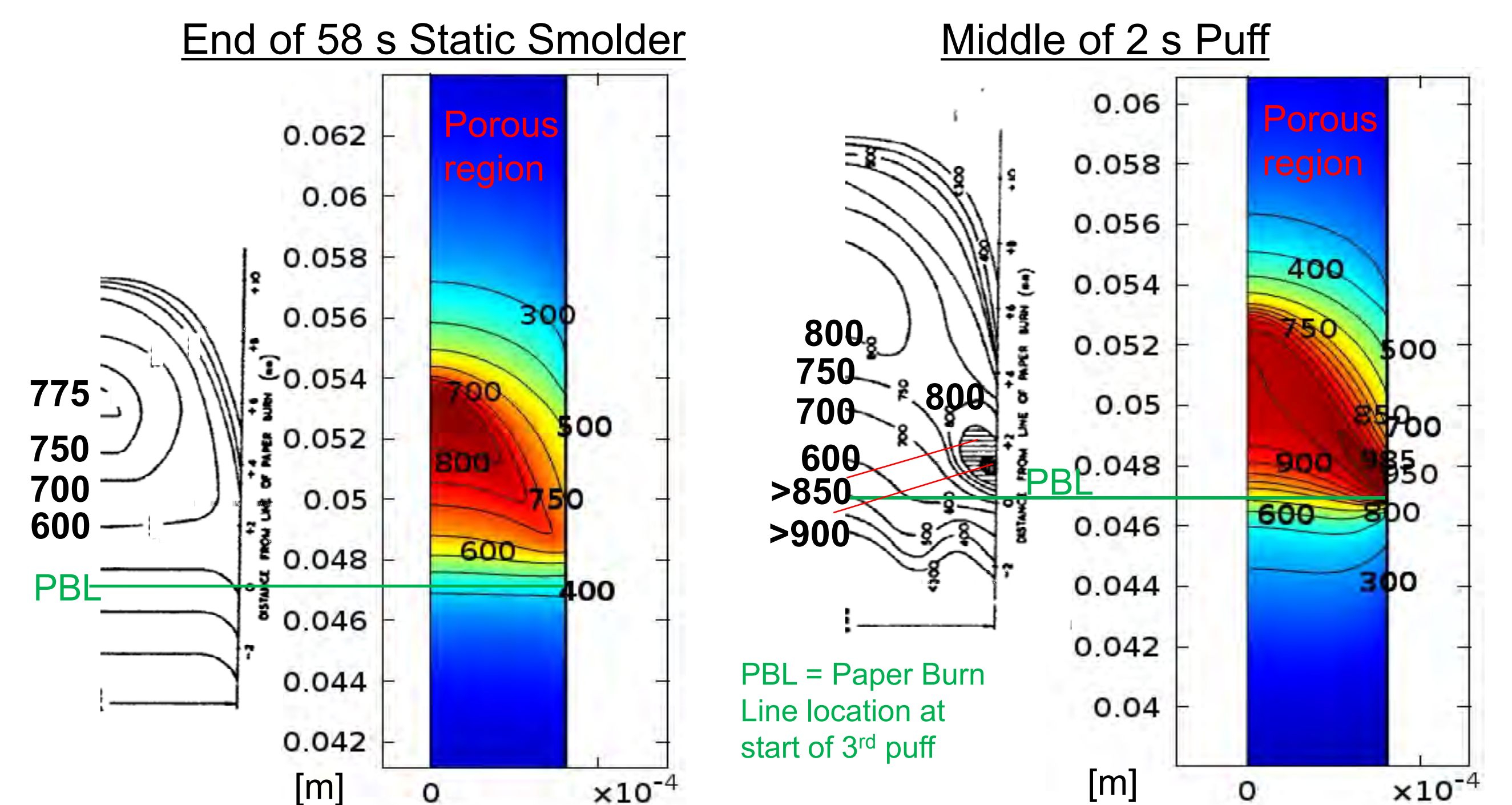


Fig 4. Experimental and Simulated Solid Temperatures (°C) at two times.

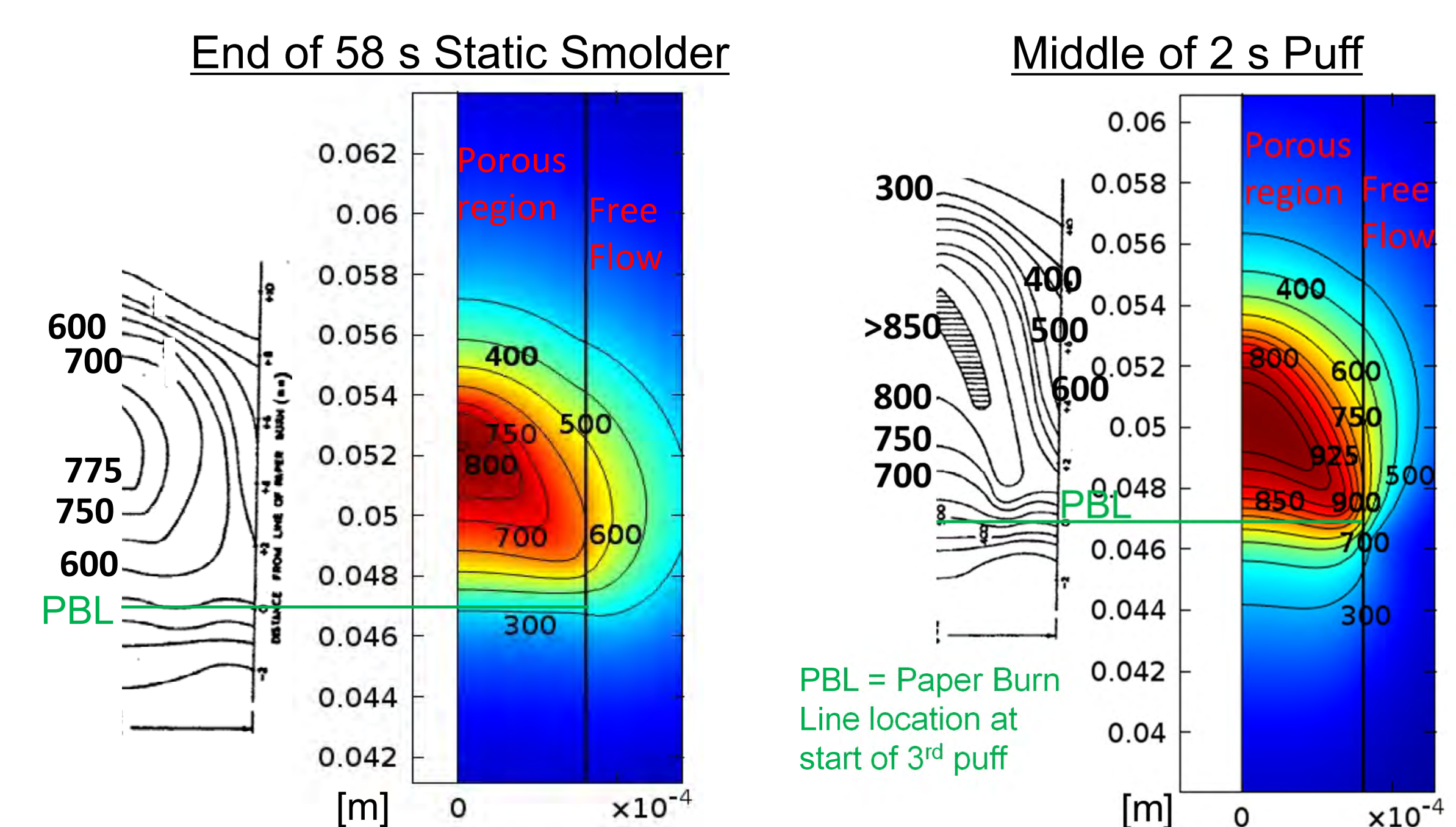


Fig 5. Experimental and Simulated Gas Temperatures (°C) at two times.

- Solid temperatures are highest along axis during the static smolder and highest along periphery, just in front of the burn line, during forward smoldering
- Maximum gas and solid temperatures are within 50-75 (°C) of experimental data<sup>1</sup>
- Deviations between experiments and simulations mostly due to shape of char coal

## Char Oxidation Rate

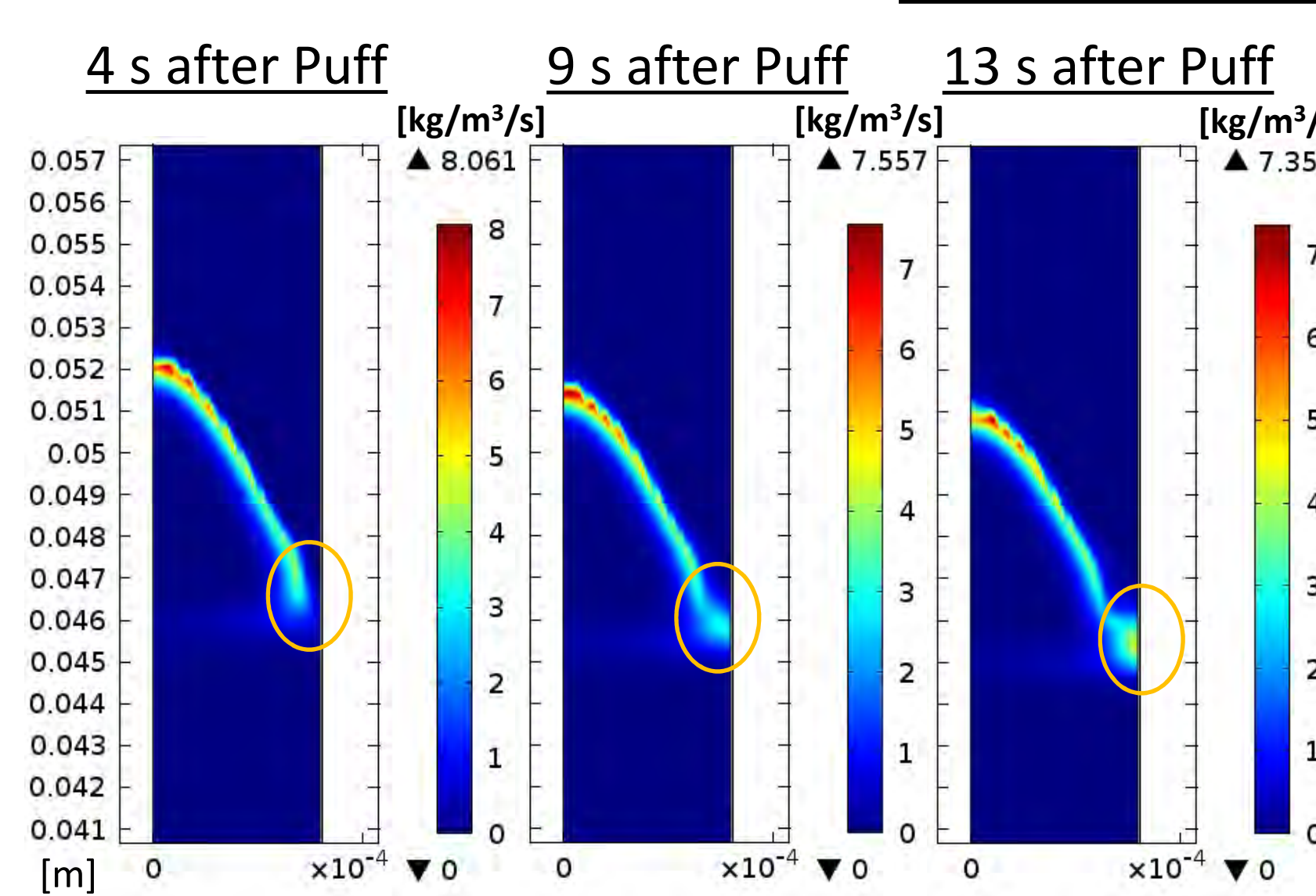


Fig 6. Char oxidation rate profiles during static smolder period.

- Char oxidation along periphery pauses for ~10 s after puff, **similar to experimental observation<sup>1</sup>** that paper burn line does not advance for ~15 s after puff!
- "Pause" is due to build-up of products at expense of O<sub>2</sub> as puff ends and lasts until diffusion can replenish O<sub>2</sub> concentrations

## Oxygen Mass Fraction

- O<sub>2</sub> depletion zone during static smolder is roughly 6 mm in length for both the simulations and experiments<sup>2</sup>
- During forward smoldering, predicted O<sub>2</sub>-starved region extends further downstream than experiment...
- Assumption of a *homogeneous porous medium* is questionable

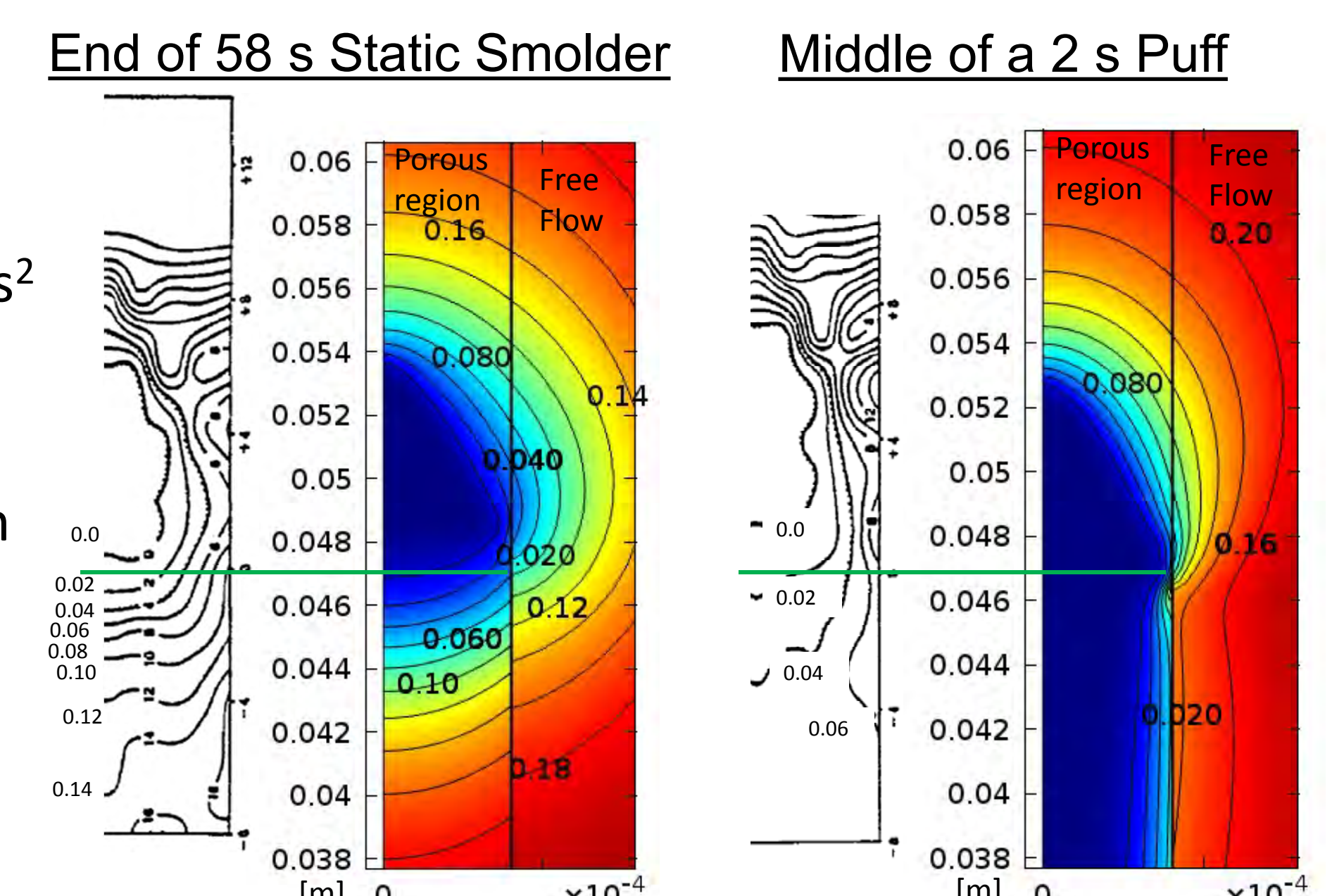


Fig 7. Experimental and Simulated Oxygen mass fractions.

**Conclusions:** A simulation of a static and forward smoking cycle in and around a burning cigarette has been validated. Ongoing work is focused on incorporating more detailed pyrolysis models. Future work may attempt to resolve smaller scales, since scale separation is weak.

## References:

1. Baker, R R, *High Temp. Science*, 7 (1975) 236-247
2. Baker, R R, *Beitr. Tabakforsch.*, 11, (1981), 1-17

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