

# Miscible viscous fingering of pushed versus pulled interface

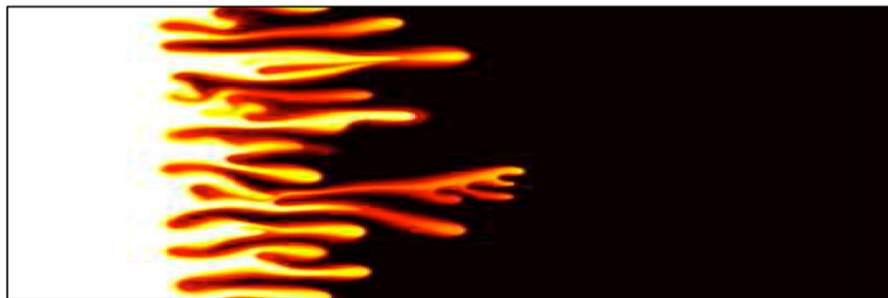
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# Viscous fingering (VF) instability

- Viscous fingering instability is special class of **hydrodynamic instability** which leads to the **dispossession** of the initial interfacial shape between the fluids with different viscosity.
- Less mobile fluid lag behind the high mobile fluid which penetrates through the former in a **porous media**.



Rectilinear displacement



Radial displacement

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# Viscous fingering (VF) instability

Viscous fingering can be observed in

- ❖ **immiscible fluids** where **surface tension** acts as the most important factor
- ❖ **miscible fluids** where the **diffusion** plays the key role

## AIM

Here we focus on the **rectilinear displacement of miscible solutions**.

Two most important applications of viscous fingering instability are

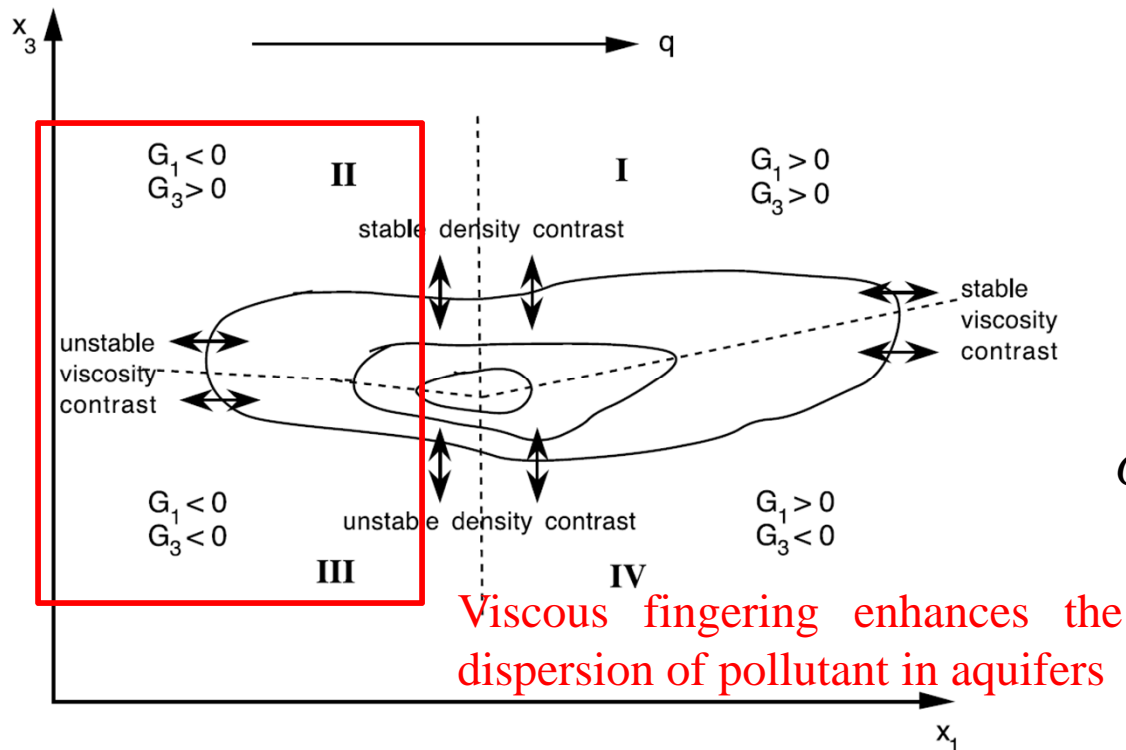
- 1. Chromatographic separation and**
- 2. Pollutants dispersion of in aquifers.**

➤ In both the cases one *fluid is localized within a finite region* and is displaced by another carrying fluid.

➤ Sometimes, the finite fluid can be confined within a *circular region* and hence **single interface model** is not appropriate for these cases.



# Dispersion pollutant in aquifers



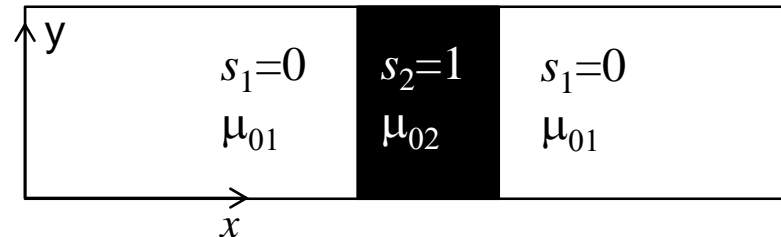
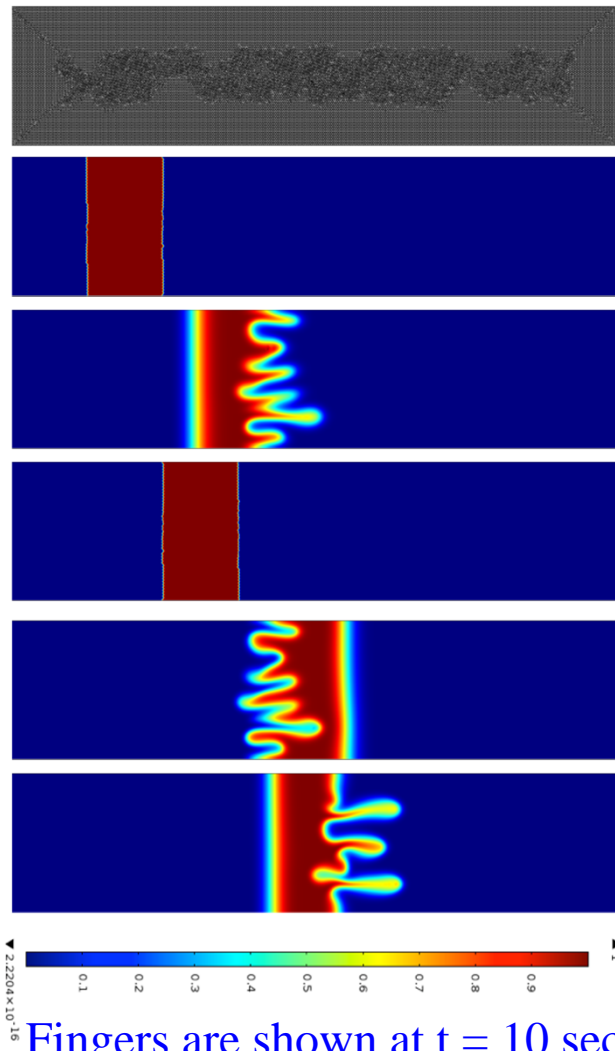
Heavy sample of higher viscosity is displaced by water in a porous media

$$G_i = -\frac{\partial c}{\partial x_i}, i = 1, 2$$

Viscous fingering enhances the dispersion of pollutant in aquifers

Fig. Schematic of hypothetical solute body with signs of concentration gradients indicated in each quadrant.

Welty et al., Water Resour. Res. 39(6), 2003

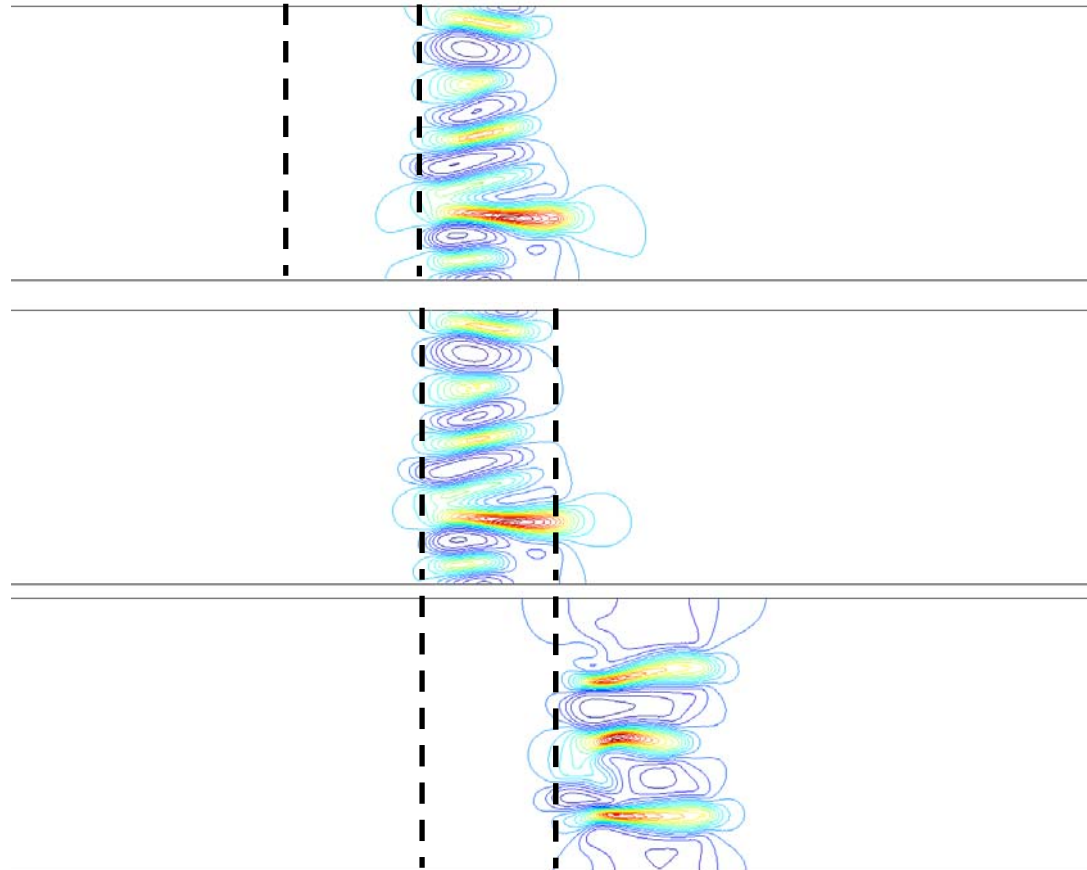


Pramanik *et al.* “Miscible viscous fingering: Application in chromatographic columns and aquifers”, *Proceedings of the COMSOL conference 2012 Bangalore*.

In version 4.2a:

- Two-phase Darcy’s law
- Free triangular meshing
- Reproduce the work of Mishra *et al.* by keeping the unstable interface at same position for both  $R > 0$  and  $R < 0$ .

# Velocity contours



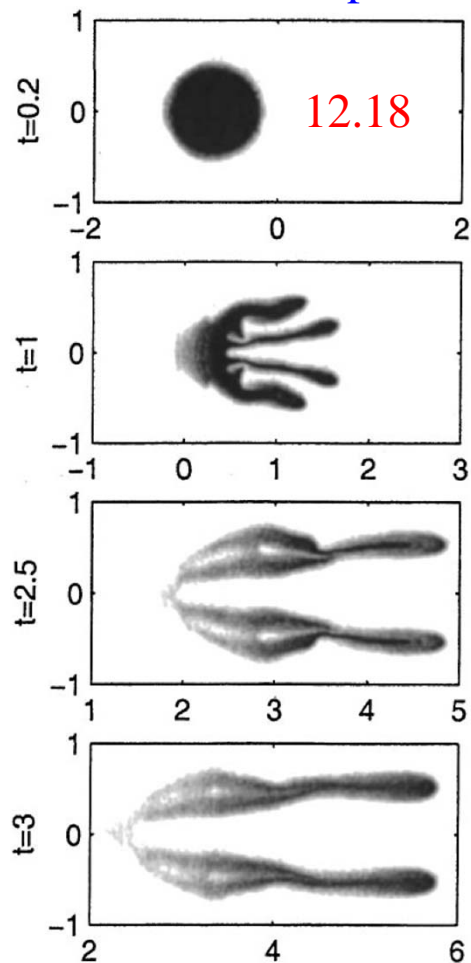
Axial velocity contours at time  $t = 10$  sec

Pramanik *et al.* Proceeding of the COMSOL conference 2012, Bangalore

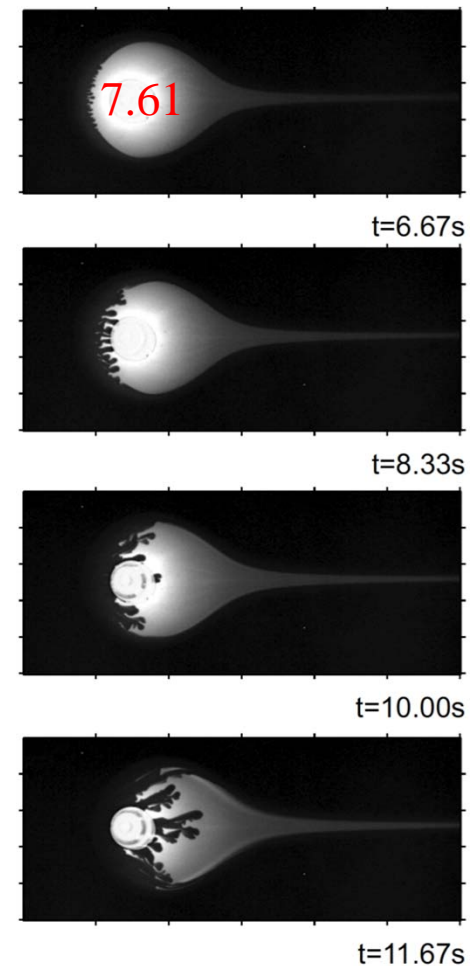
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# VF with circular sample

Theoretical modeling, less  
viscous sample



Experimental investigation, more  
viscous sample

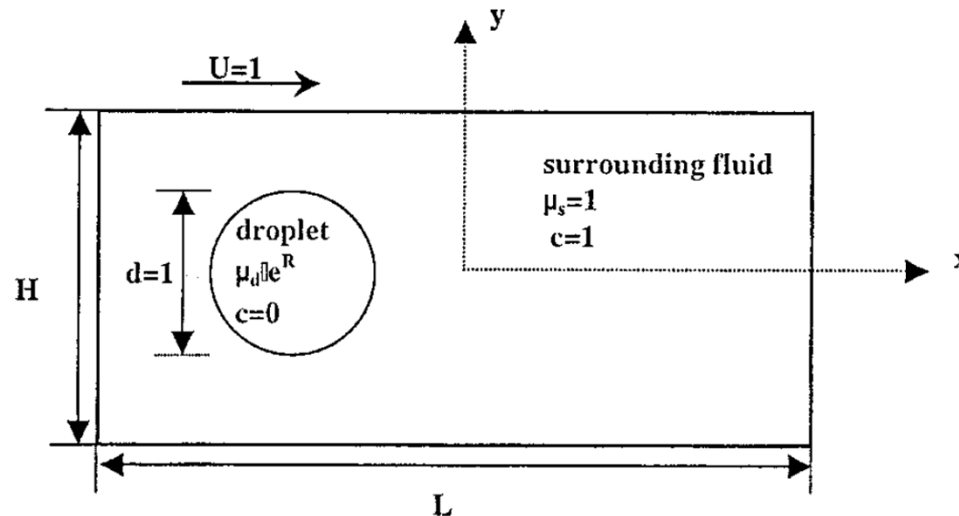


Chen *et al.* Phys. Fluids 13, 2001

Maes *et al.* Phys. Fluids 22, 2010

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# Theoretical model



## Governing equations

$$\nabla \cdot \vec{u} = 0,$$

$$\nabla p = -\frac{\mu(c)}{k} \vec{u},$$

$$\frac{\partial c}{\partial t} + \vec{u} \cdot \nabla c = \nabla \cdot (D \nabla c),$$

$$\mu(c) = e^{R(1-c)}.$$

$\vec{u}$ : 2D velocity field

$k$ : permeability

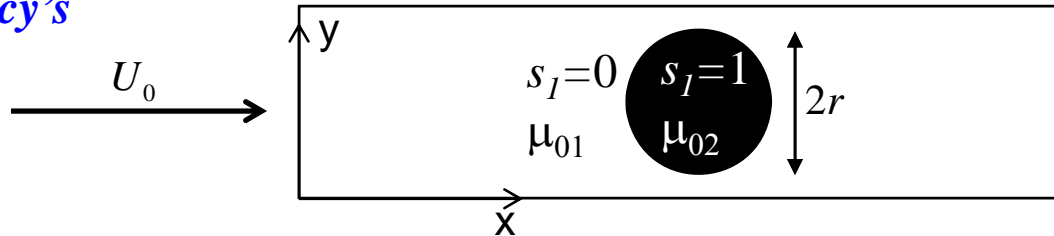
$p$ : pressure

$c$ : concentration of the solute  
driving viscosity

$D$ : dispersion coefficient



*Two-phase Darcy's law*



*Governing equations*

$$\frac{\partial \varepsilon_p \rho}{\partial t} + \nabla \cdot \rho \vec{u} = 0, \quad \vec{u} = -\frac{\kappa}{\mu} \nabla p$$

$$\rho = \rho_1 s_1 + \rho_2 s_2, \quad \frac{1}{\mu} = s_1 \frac{\kappa_{r1}}{\mu_1} + s_2 \frac{\kappa_{r2}}{\mu_2},$$

$$\frac{\partial \varepsilon_p \rho}{\partial t} + \nabla \cdot c_1 \vec{u} = \nabla \cdot D_c \nabla c_1, \quad c_1 = \rho_1 s_1$$

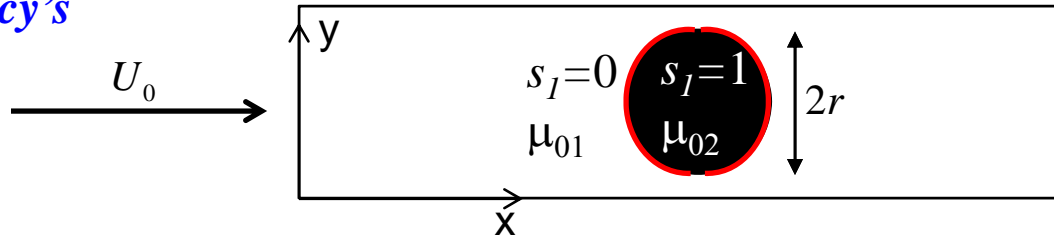
$$\mu_1 = \mu_2 = \mu_{01} e^{Rs_1}$$

$$\rho = \rho_1 = \rho_2 = \text{constant}$$

$$\varepsilon_p, \kappa = \text{constant}$$

$$\kappa_{r1} = \kappa_{r2} = 1$$

## Two-phase Darcy's law



### Boundary conditions

$$-\vec{n} \cdot \rho \vec{u} = 0 \quad \text{No flux}$$

$$-\vec{n} \cdot D_c \nabla c_1 = 0 \quad \text{Outflow}$$

$$-\vec{n} \cdot \rho \vec{u} = (s_1 \rho_1 + s_2 \rho_2) U_0 \quad \text{Inflow}$$

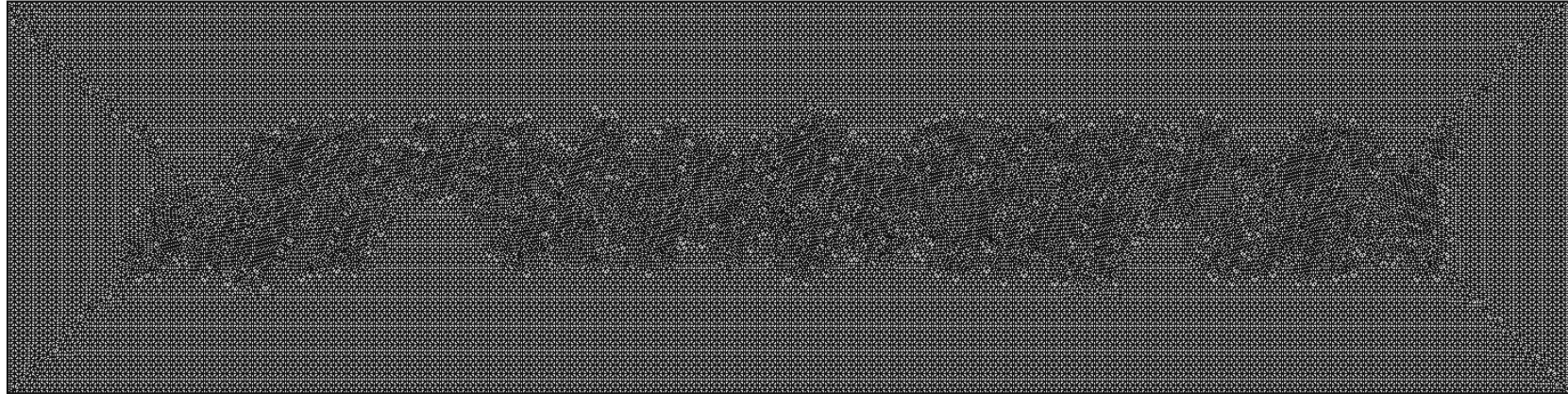
$$s_2 = 1 - s_1$$

### Initial condition

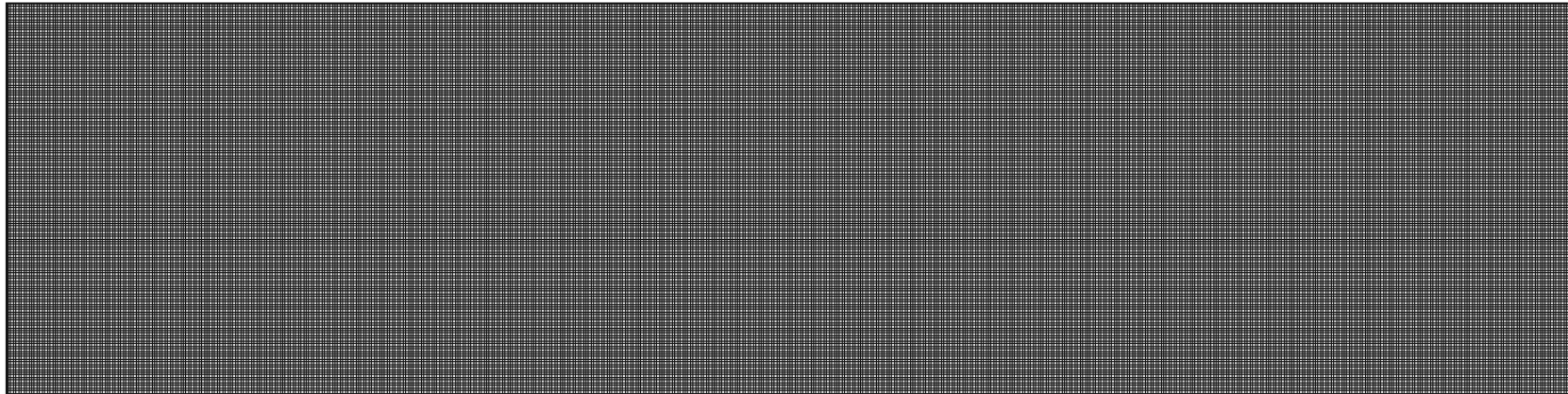
$$s_1 = \begin{cases} 1, & (x - x_0)^2 + (y - y_0)^2 \leq r^2 \\ 0, & (x - x_0)^2 + (y - y_0)^2 > r^2 \end{cases}$$

$(x_0, y_0)$  being the center of the circle

Normal inflow velocity  $U_0$



**Extra fine free triangular mesh (# of elements 64852)**



**Extremely fine mapped mesh (# of elements 91196)**

Parameters	Symbols	Value & Unit
Length of the domain	$L_x$	0.32 mm
Width of the domain	$L_y$	0.08 mm
Log-mobility ratio	$R$	-3, 0, 3
Injection speed	$U_0$	1 mm/s
Viscosity of the displacing fluid	$\mu_{01}$	$10^{-3}$ Pa-s
Aspect ratio	$A$	4
Radius of the circular sample	$r = 0.15 \times L_y$	0.012 mm
	$r = 0.3 \times L_y$	0.024 mm
	$r = 0.45 \times L_y$	0.036 mm
Center of the circle	$x_0 = L_x/9,$ $y_0 = L_y/2$	(0.0356, 0.04) (mm)

## Comparison of two linear solvers MUMPS and PARDISO

Parameter set	Computational time	
	MUMPS	PARDISO
$R = -2, L_y = 0.08$ mm, $r = 0.45 \times L_y, A = 4$	8319 seconds	21345 seconds
$R = 2, L_y = 0.08$ mm, $r = 0.45 \times L_y, A = 4$	2479 seconds	1996 seconds
$R = 0, L_y = 0.08$ mm, $r = 0.3 \times L_y, A = 4$	1912 seconds	466 seconds



# Results

*VF at pushed interface*

$t = 0$



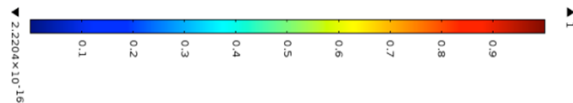
$t = 8$



$t = 10$



$t = 12$



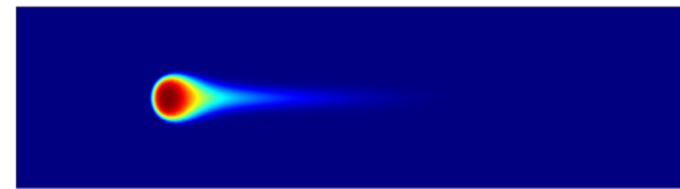
$U_0 = 1 \times 10^{-3} \text{ m/s}$ ,  $R = -3$ ,  $L_y = 0.08 \text{ mm}$ . and  $r = 0.15 \times L_y$ .

*VF at pulled interface*

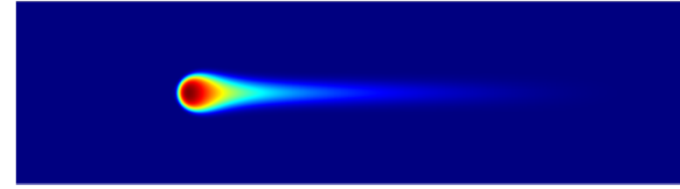
$t = 0$



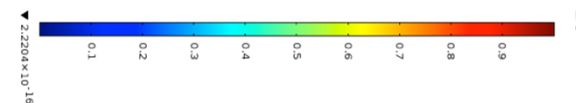
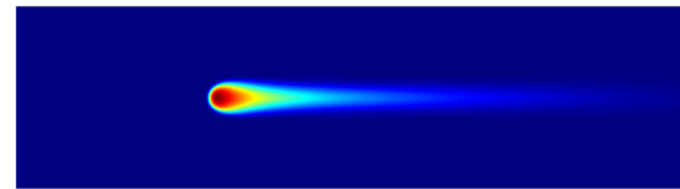
$t = 100$



$t = 150$



$t = 200$



$U_0 = 1 \times 10^{-3} \text{ m/s}$ ,  $R = 3$ ,  $L_y = 0.08 \text{ mm}$ . and  $r = 0.15 \times L_y$ .

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$$U_0 = 1 \times 10^{-3} \text{ m/s}, R = -3, L_y = 0.08 \text{ mm. and } r = 0.15 \times L_y$$



$$U_0 = 1 \times 10^{-3} \text{ m/s}, R = 3, L_y = 0.08 \text{ mm. and } r = 0.15 \times L_y$$





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