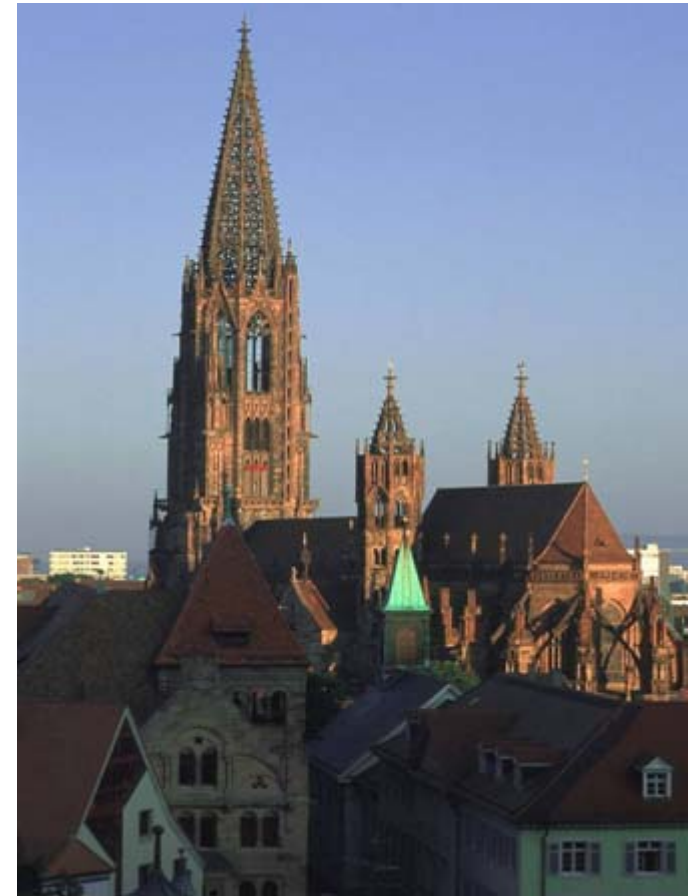


Multiphysics Simulation of Thermoelectric Systems

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Contents

$$-\nabla \cdot ((\sigma \alpha^2 T + \lambda) \nabla T) - \nabla \cdot (\sigma \alpha T \nabla V) = \sigma ((\nabla V)^2 + \alpha \nabla T \nabla V)$$

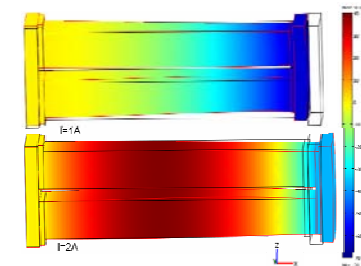
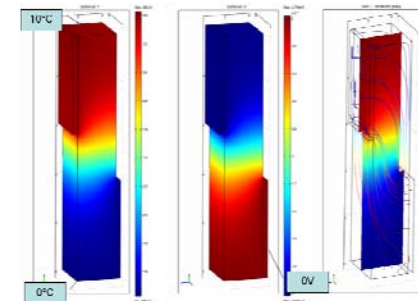
$$\nabla \cdot (\sigma \alpha \nabla T) + \nabla \cdot (\sigma \nabla V) = 0$$

$$c_n \frac{\partial^2 u}{\partial t^2} + d_n \frac{\partial u}{\partial t} + \nabla \cdot (-c \nabla u - \alpha u + \gamma) + \beta \cdot \nabla u + \alpha u = f \quad \text{in } \Omega$$

$$n \cdot (-c \nabla u - \alpha u + \gamma) + q u = g - k^T \mu \quad \text{on } \partial \Omega$$

$$h u = r \quad \text{on } \partial \Omega$$

1. Introduction
2. Equations to solve
3. Implementation in COMSOL
4. Thermoelectric modeling
5. Thermo-electric-mechanic calculations



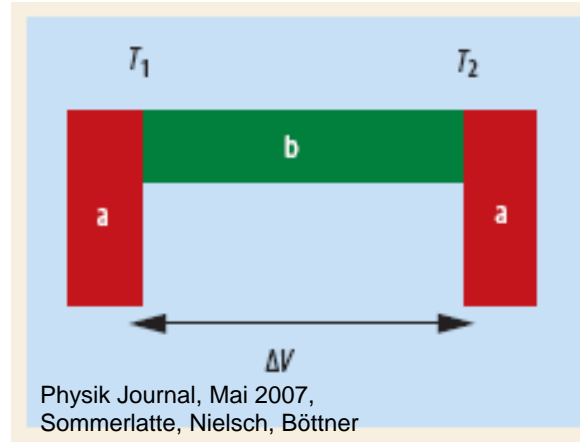
Introduction

Seebeck-Effect



T. Seebeck (1821)

$$\alpha = \Delta V / \Delta T$$



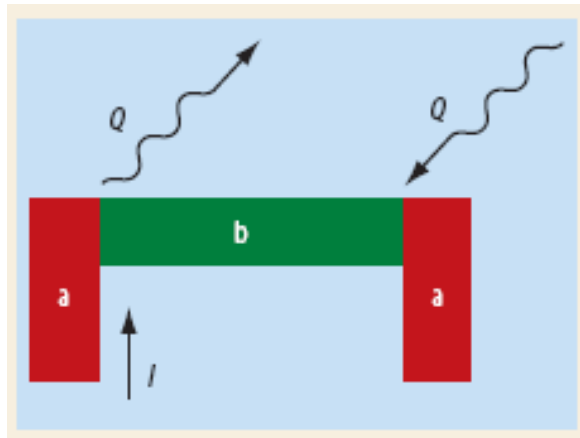
Peltier-Effect



J. C. A. Peltier (1834)

$$Q = \Pi * I$$

$$\Pi = \alpha * T$$



Thermoelectric Figure of Merit Z

$$Z = \frac{\sigma \alpha^2}{\lambda}$$

α : Seebeck Coefficient

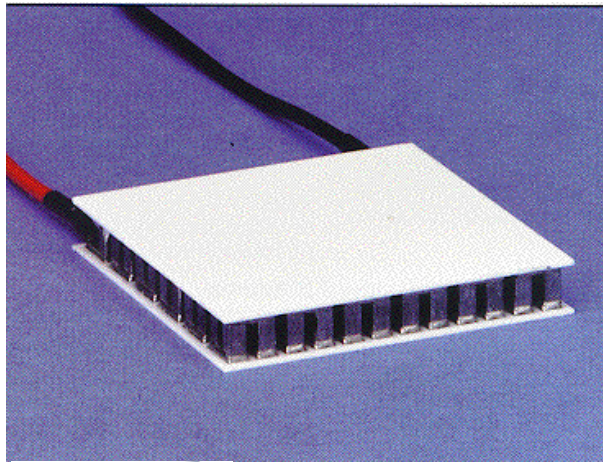
Π : Peltier Coefficient

σ, λ : electrical and thermal conductivities

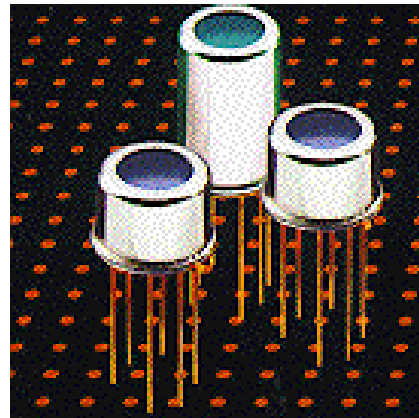
Introduction

Applications of Thermoelectrics

Coolers

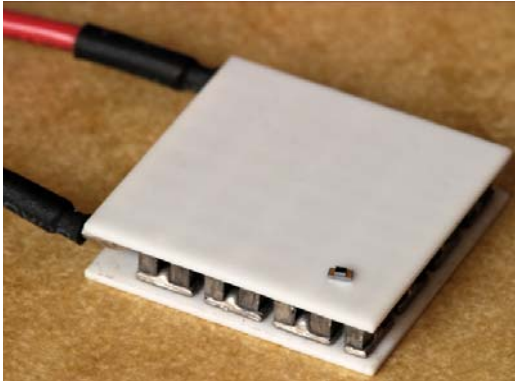


Detectors, Sensors



Generators





Seebeck-Coefficient

α_n and α_p

Electrical Conductivity

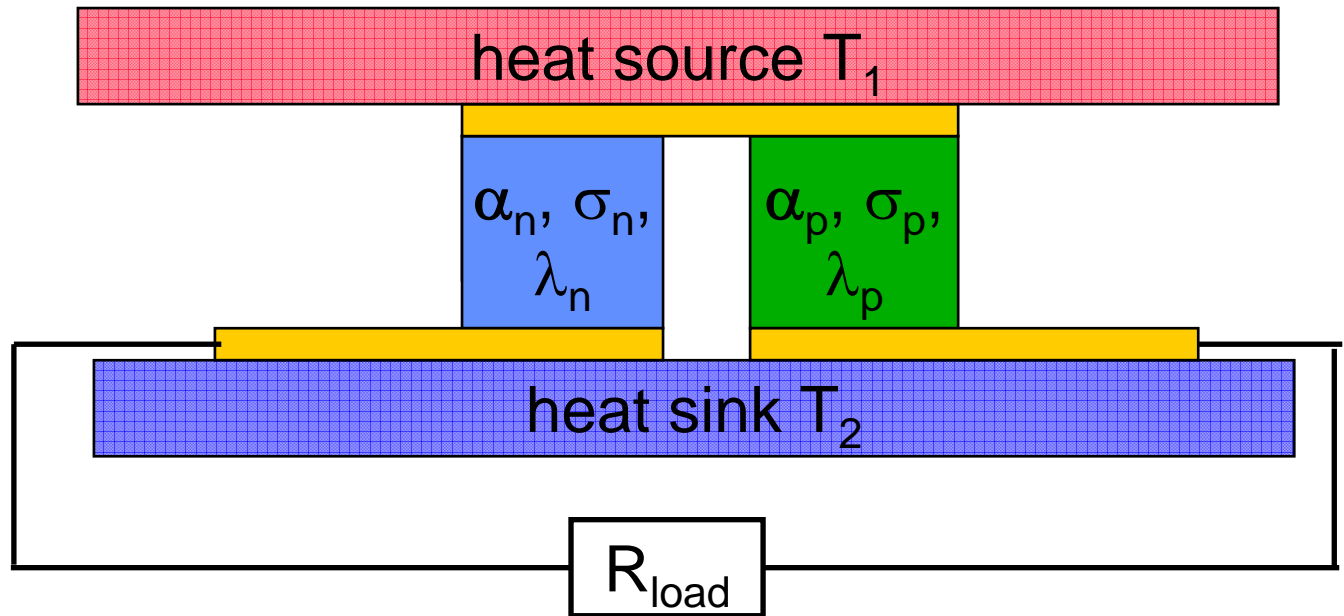
σ_n and σ_p

Thermal Conductivity

λ_n and λ_p

Dimensionless Figure of Merit ZT

Introduction



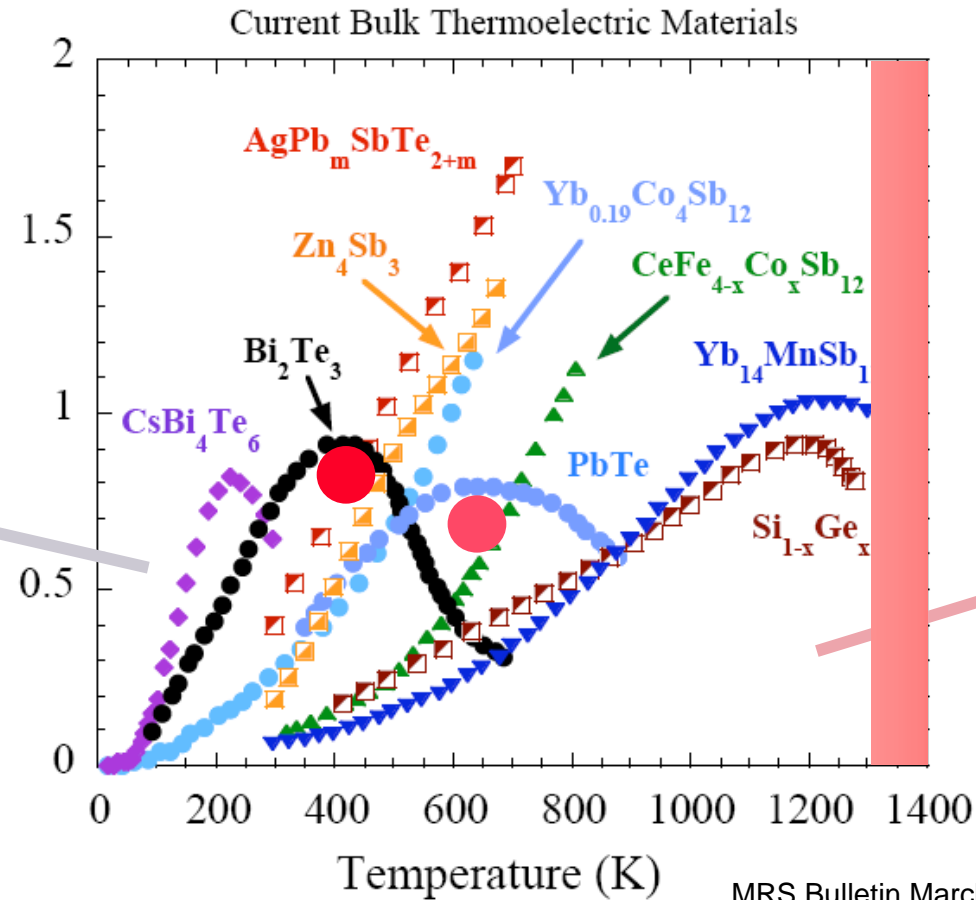
$$ZT = \frac{\sigma \alpha^2}{\lambda} T$$

Introduction



cooling

ZT : Figure of Merit



MRS Bulletin March, 2006



waste heat

Thermoelectric Effects in ANSYS 9 and higher (Antonova et al., ICT 2005)

Example for COMSOL implementation:

Rearrange equations ...

Field equations

$$\rho C \frac{\partial T}{\partial t} + \nabla \cdot \mathbf{q} = \mathcal{Q}$$

$$\nabla \cdot \left(\mathbf{J} + \frac{\partial \mathbf{D}}{\partial t} \right) = 0$$

$$\mathbf{E} = -\nabla \phi.$$

Constitutive equations

$$\mathbf{q} = [\Pi] \cdot \mathbf{J} - [\lambda] \cdot \nabla T$$

$$\mathbf{J} = [\sigma] \cdot (\mathbf{E} - [\alpha] \cdot \nabla T)$$

$$\mathbf{D} = [\varepsilon] \cdot \mathbf{E},$$

Nomenclature :

ρ = density
 C = specific heat capacity
 T = absolute temperature
 \mathcal{Q} = heat generation rate density
 \mathbf{q} = heat flux vector
 \mathbf{J} = electric current density vector
 \mathbf{E} = electric field intensity vector
 \mathbf{D} = electric flux density vector
 $[\lambda]$ = thermal conductivity matrix
 $[\sigma]$ = electrical conductivity matrix
 $[\alpha]$ = Seebeck coefficient matrix,
 $[\Pi] = T[\alpha]$ = Peltier coefficient matrix
 $[\varepsilon]$ = dielectric permittivity matrix

Coupled-Field Equations

~~$$\rho C \frac{\partial T}{\partial t} + \nabla \cdot ([\Pi] \cdot \mathbf{J}) - \nabla \cdot ([\lambda] \cdot \nabla T) = \mathcal{Q}$$~~
~~$$\nabla \cdot ([\varepsilon] \cdot \nabla \frac{\partial \phi}{\partial t}) + \nabla \cdot ([\sigma] \cdot [\alpha] \cdot \nabla T) + \nabla \cdot ([\sigma] \cdot \nabla \phi) = 0$$~~

Antonova, Looman, ICT 2005

5

$$-\vec{\nabla} \cdot ((\sigma \alpha^2 T + \lambda) \vec{\nabla} T) - \vec{\nabla} \cdot (\sigma \alpha T \vec{\nabla} V) = \sigma ((\vec{\nabla} V)^2 + \alpha \vec{\nabla} T \vec{\nabla} V)$$

$$\vec{\nabla} \cdot (\sigma \alpha \vec{\nabla} T) + \vec{\nabla} \cdot (\sigma \vec{\nabla} V) = 0$$

Thermoelectrics in COMSOL:

Rearrange equations ...

$$-\vec{\nabla}((\sigma\alpha^2 T + \lambda)\vec{\nabla}T) - \vec{\nabla}(\sigma\alpha T\vec{\nabla}V) = \sigma((\vec{\nabla}V)^2 + \alpha\vec{\nabla}T\vec{\nabla}V)$$

$$\vec{\nabla}(\sigma\alpha\vec{\nabla}T) + \vec{\nabla}(\sigma\vec{\nabla}V) = 0$$

... to match with PDE-
application modes
(coefficient form,
different notation!)

$$c_a \frac{\partial^2 u}{\partial t^2} + d_a \frac{\partial u}{\partial t} + \nabla \cdot (-c\nabla u - \alpha u + \gamma) + \beta \cdot \nabla u + \alpha u = f \quad \text{in } \Omega$$

$$n \cdot (-c\nabla u - \alpha u + \gamma) + qu = g - h^T \mu \quad \text{on } \partial\Omega$$

$$hu = r \quad \text{on } \partial\Omega$$

Thermoelectrics in COMSOL:

Thermoelectric coupled field equations

$$-\vec{\nabla}((\sigma\alpha^2 T + \lambda)\vec{\nabla}T) - \vec{\nabla}(\sigma\alpha T\vec{\nabla}V) = \sigma((\vec{\nabla}V)^2 + \alpha\vec{\nabla}T\vec{\nabla}V)$$

$$\vec{\nabla}(\sigma\alpha\vec{\nabla}T) + \vec{\nabla}(\sigma\vec{\nabla}V) = 0$$

... example: static thermoelectrics

$$\cancel{c_u} \frac{\partial^2 u}{\partial t^2} + \cancel{d_u} \frac{\partial u}{\partial t} + \nabla \cdot (-c\nabla u - \cancel{\alpha u} + \cancel{\gamma}) + \cancel{\beta} \cdot \nabla u + \cancel{\alpha u} = f \quad \text{in } \Omega$$

$$n \cdot (-c\nabla u - \cancel{\alpha u} + \cancel{\gamma}) + \cancel{qu} = g - h^T \mu \quad \text{on } \partial\Omega$$

$$hu = r \quad \text{on } \partial\Omega$$

Thermoelectrics in COMSOL:

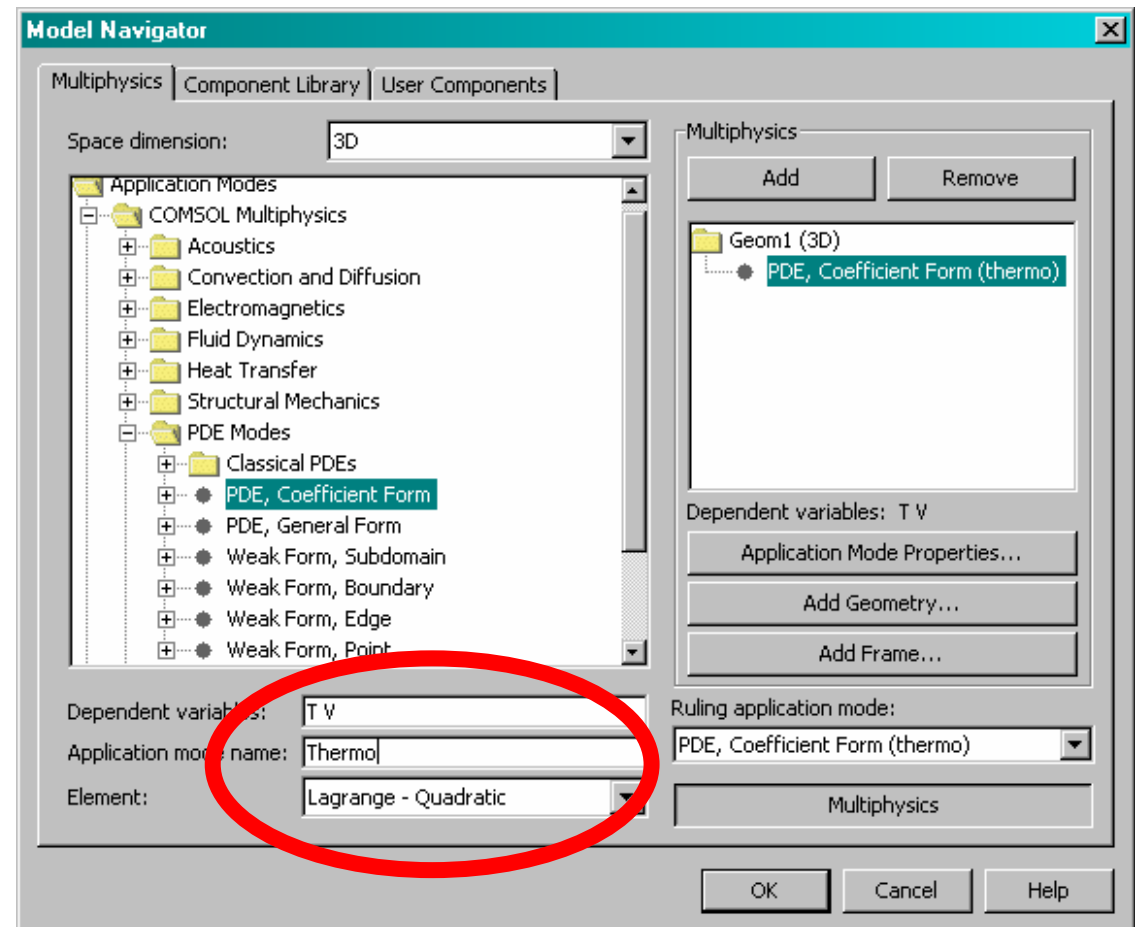
Defining

-Application mode

PDE-Mode, coefficient Form

- Field Variable

$$\vec{u} = \begin{pmatrix} T \\ V \end{pmatrix}$$

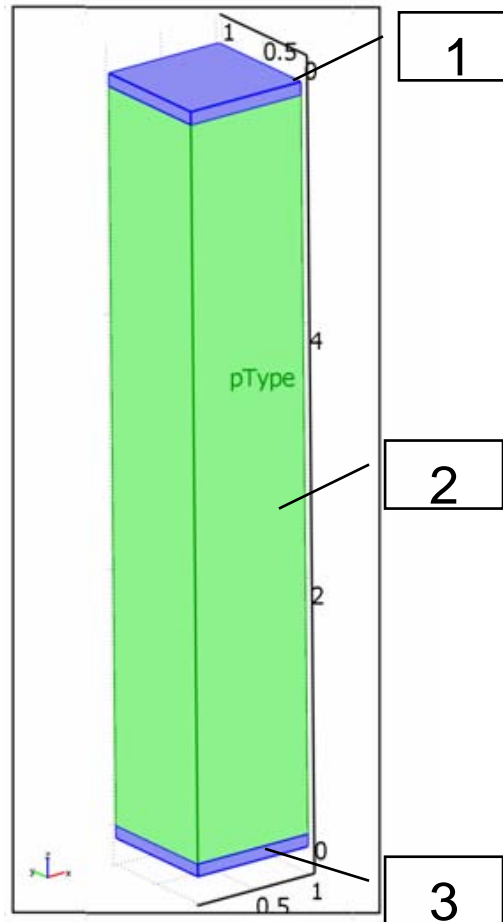


Thermoelectrics in COMSOL:

Defining model geometry, example: P-Type thermoelectric leg

1, 3: Copper electrodes
w_xl_xh: 1x1x0.1mm³

2: p-type thermoelectric leg
w_xl_xh: 1x1x5.8mm³



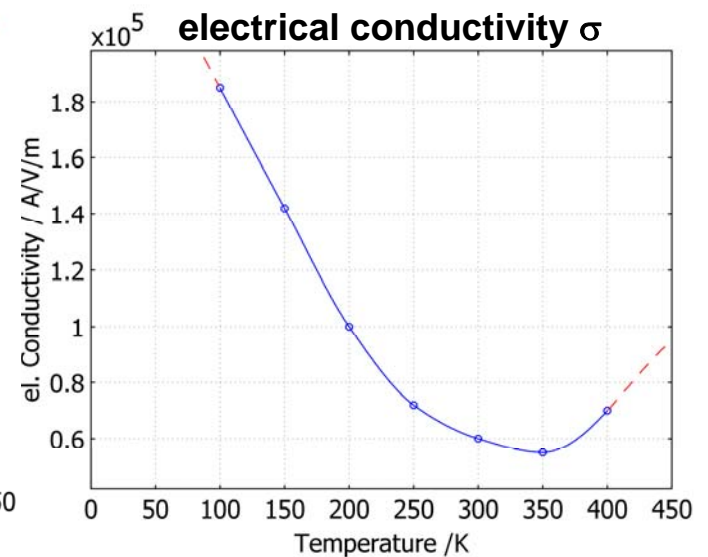
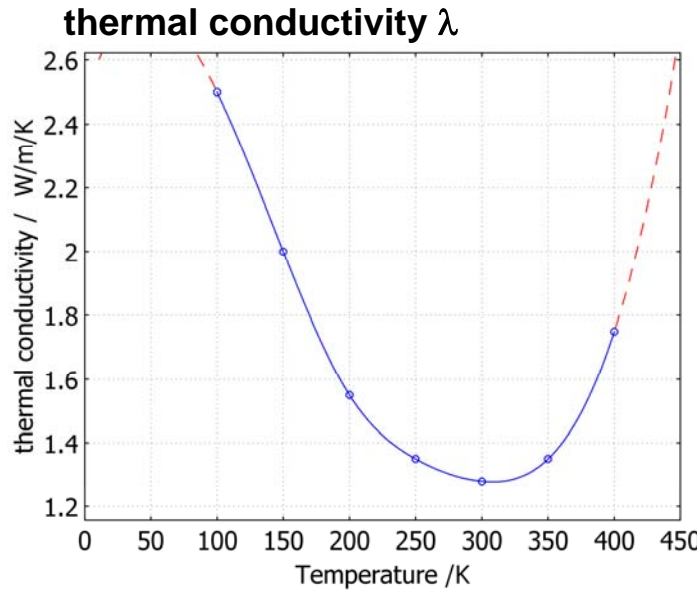
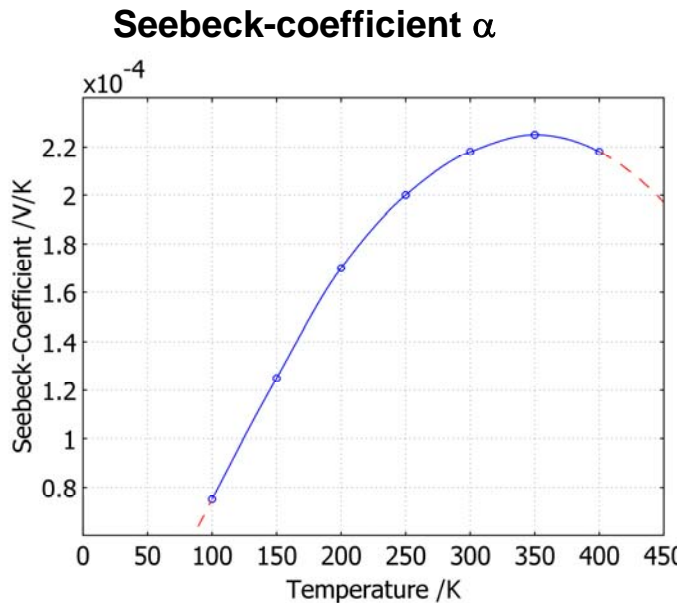
| | | Thermoelectric Material, 2 | Electrode (Copper), 1, 3 |
|-----------------------|----------------------------|----------------------------|--------------------------|
| Seebeck Coefficient | α , V/K | p: 200e-6 n: -200e-6 | 6.5e-6 |
| Electric conductivity | σ , S/m | 1.1e5 | 5.9e8 |
| Thermal conductivity | λ , W/m/K | 1.6 | 350 |
| Density | ρ , kg/m ³ | 7740 | 8920 |
| Heat capacity | C, J/kg/K | 154.4 | 385 |

Antonova, Looman, ICT 2005

Thermoelectrics in COMSOL:

Temperature dependent material properties for p-Bismuth Telluride

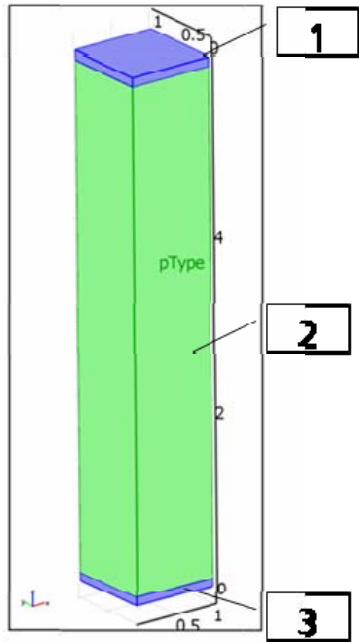
| T /K | α / $10^{-6}V/K$ | λ / W/m/K | σ / $10^3 A/V/m$ |
|------|-------------------------|-------------------|-------------------------|
| 100 | 75 | 2.5 | 185 |
| 150 | 125 | 2 | 142 |
| 200 | 170 | 1.55 | 100 |
| 250 | 200 | 1.35 | 72 |
| 300 | 218 | 1.28 | 60 |
| 350 | 225 | 1.35 | 55 |
| 400 | 218 | 1.75 | 70 |



Seifert, W., Ueltzen, M., Müller, E.; One Dimensional Modelling of Thermoelectric Cooling; phys.stat.sol. (a) 194, No.1, pp 277 – 290; 2002

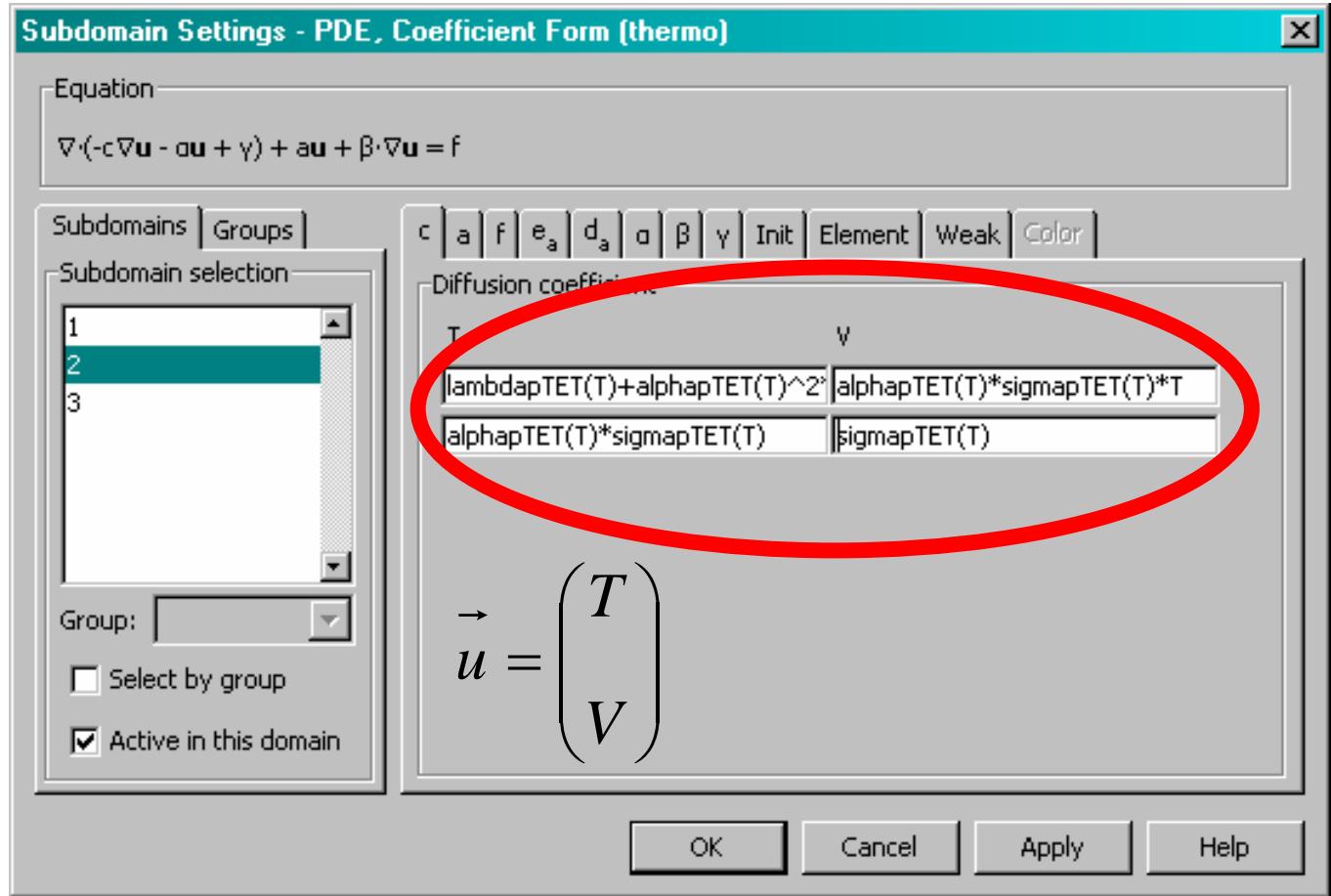


Thermoelectrics in COMSOL:

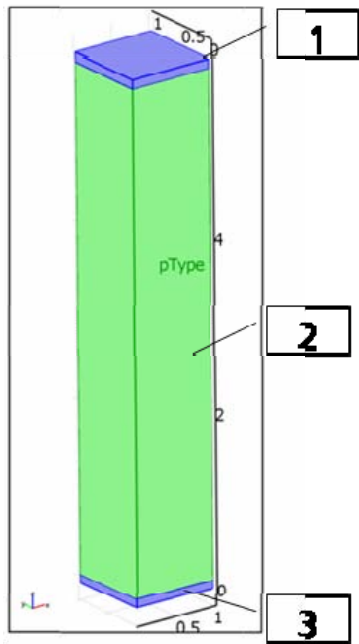


Defining coefficient c:

$$c = \begin{pmatrix} \lambda + \sigma\alpha^2 T & \sigma\alpha T \\ \sigma\alpha & \sigma \end{pmatrix}$$

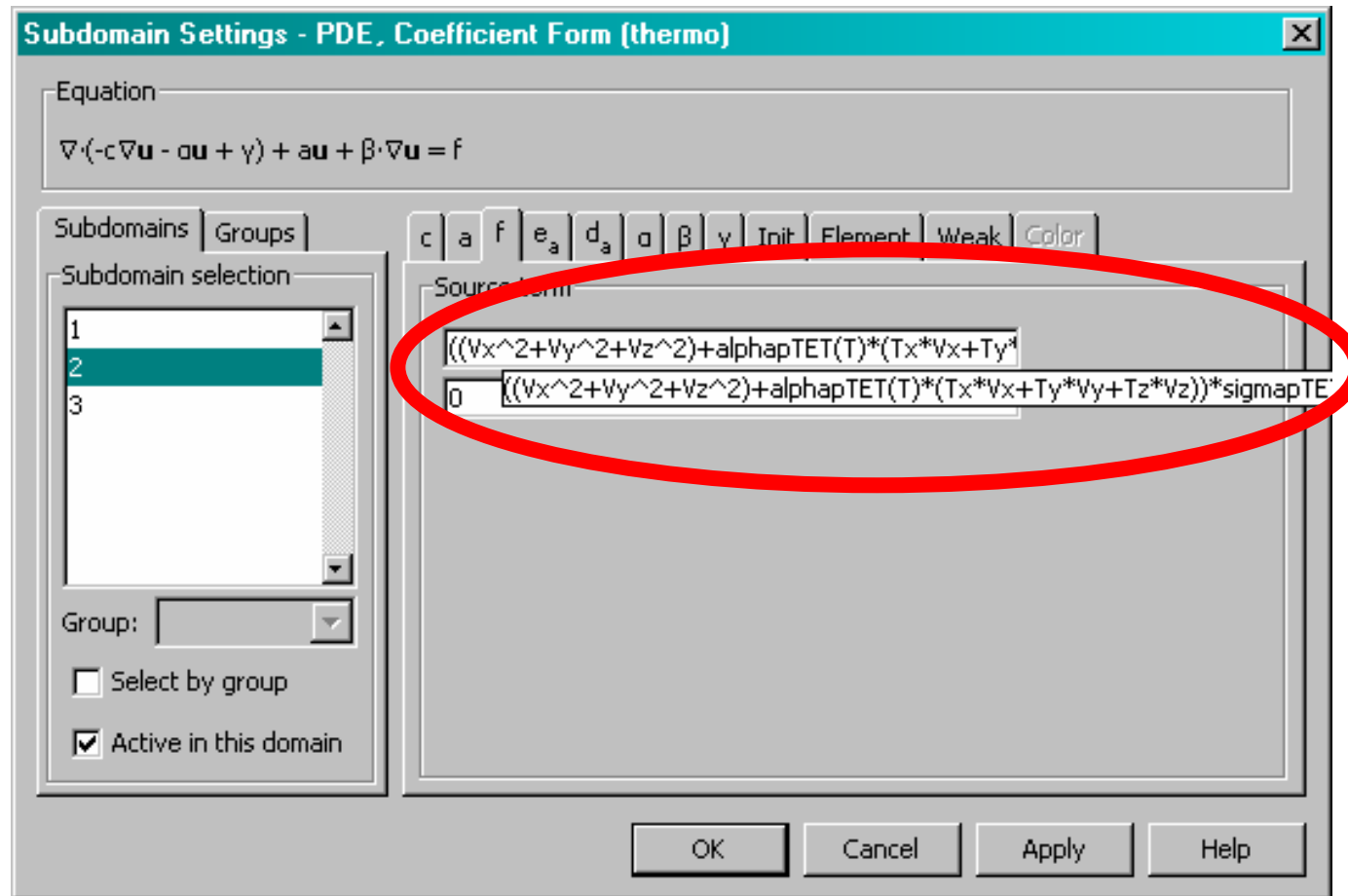


Thermoelectrics in COMSOL:

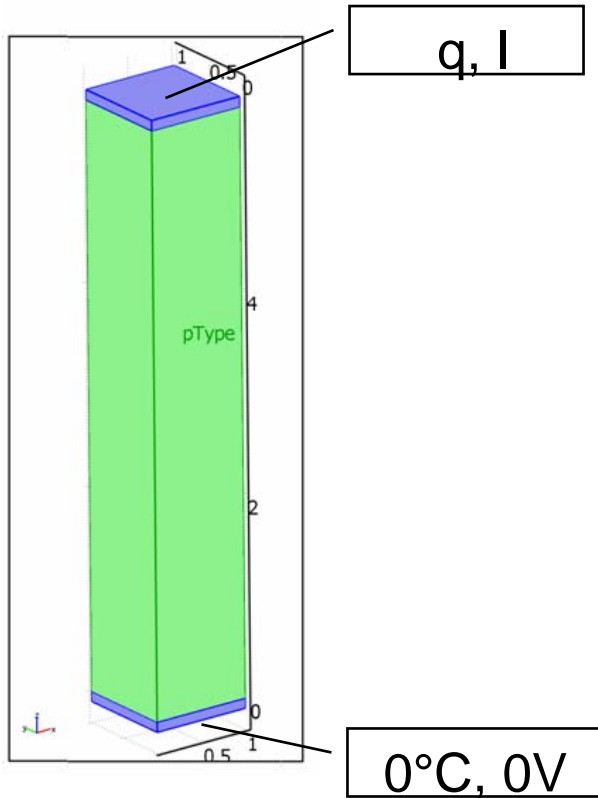


Defining coefficient f

$$f = \begin{pmatrix} \sigma \left(\left(\vec{\nabla} V \right)^2 + \alpha \vec{\nabla} T \vec{\nabla} V \right) \\ 0 \end{pmatrix}$$

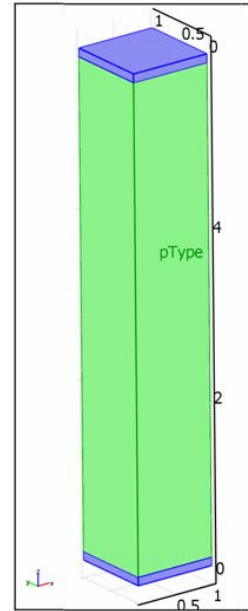


Thermoelectrics in COMSOL:

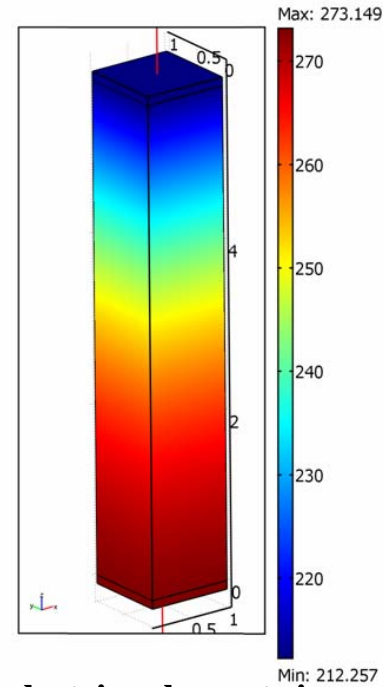


solve →

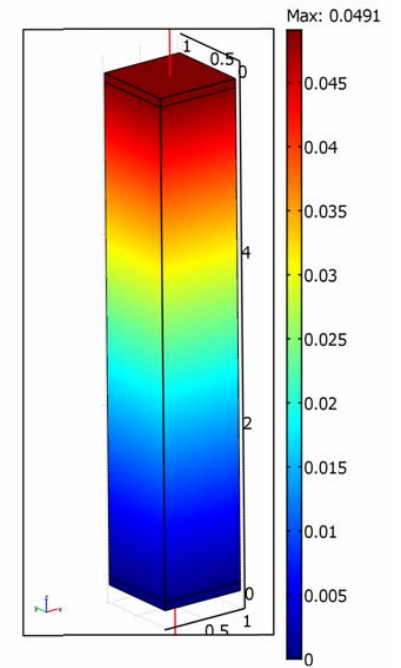
Geometry



Temperature



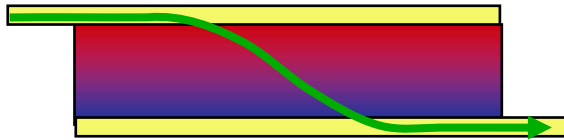
Voltage



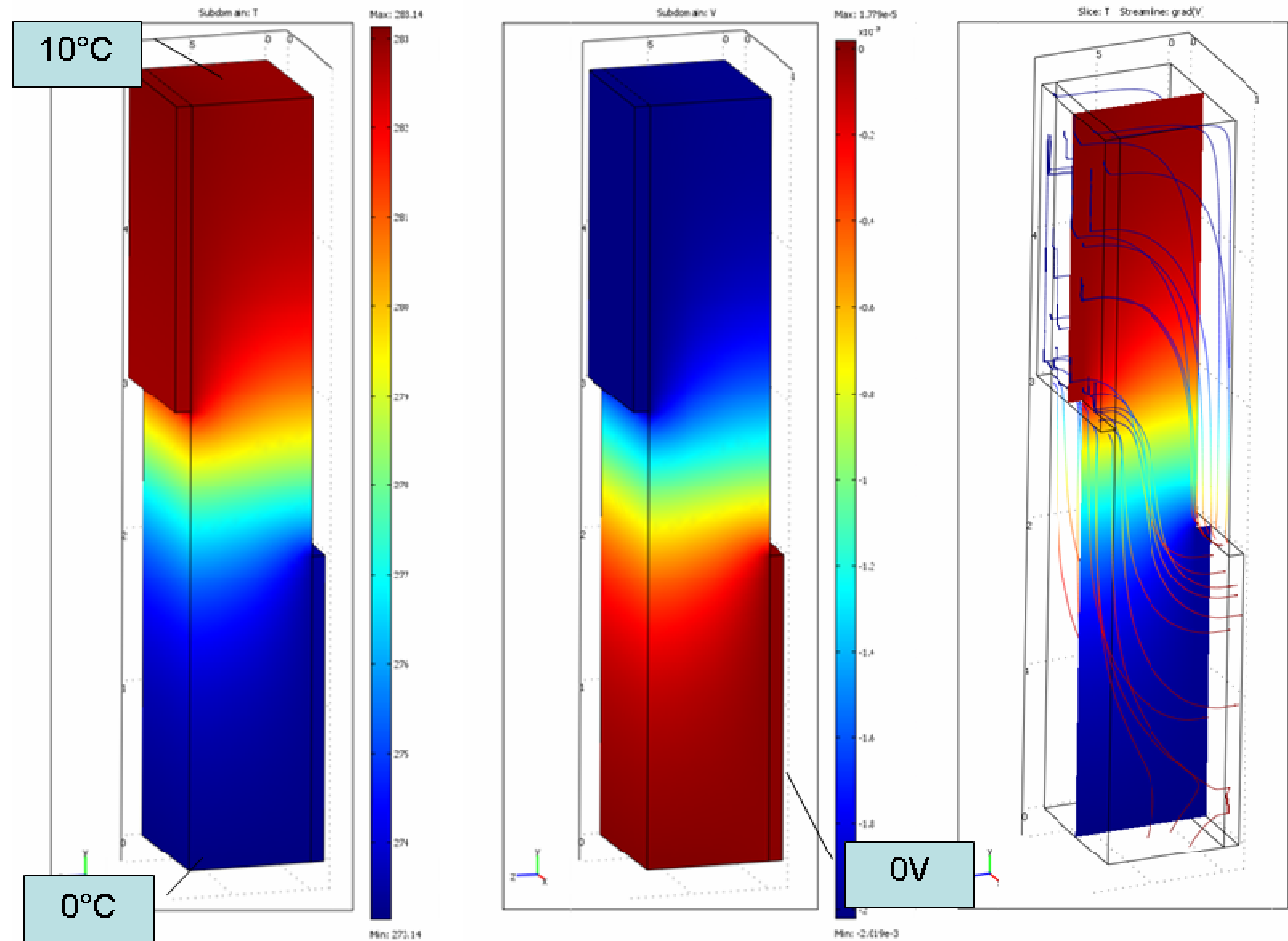
A p-type thermoelectric element is contacted by copper electrodes (left). The base is kept at 0°C and 0V. At the top 0.7A current was applied. Adiabatic boundary conditions were used. The resulting temperature distribution is shown in the center, the voltage is shown right. A temperature difference of nearly 61 K is achieved. The voltage at the upper electrode is 49 mV.

Boundary conditions:
Heat load q (here 0W), current I

„complex“ geometries



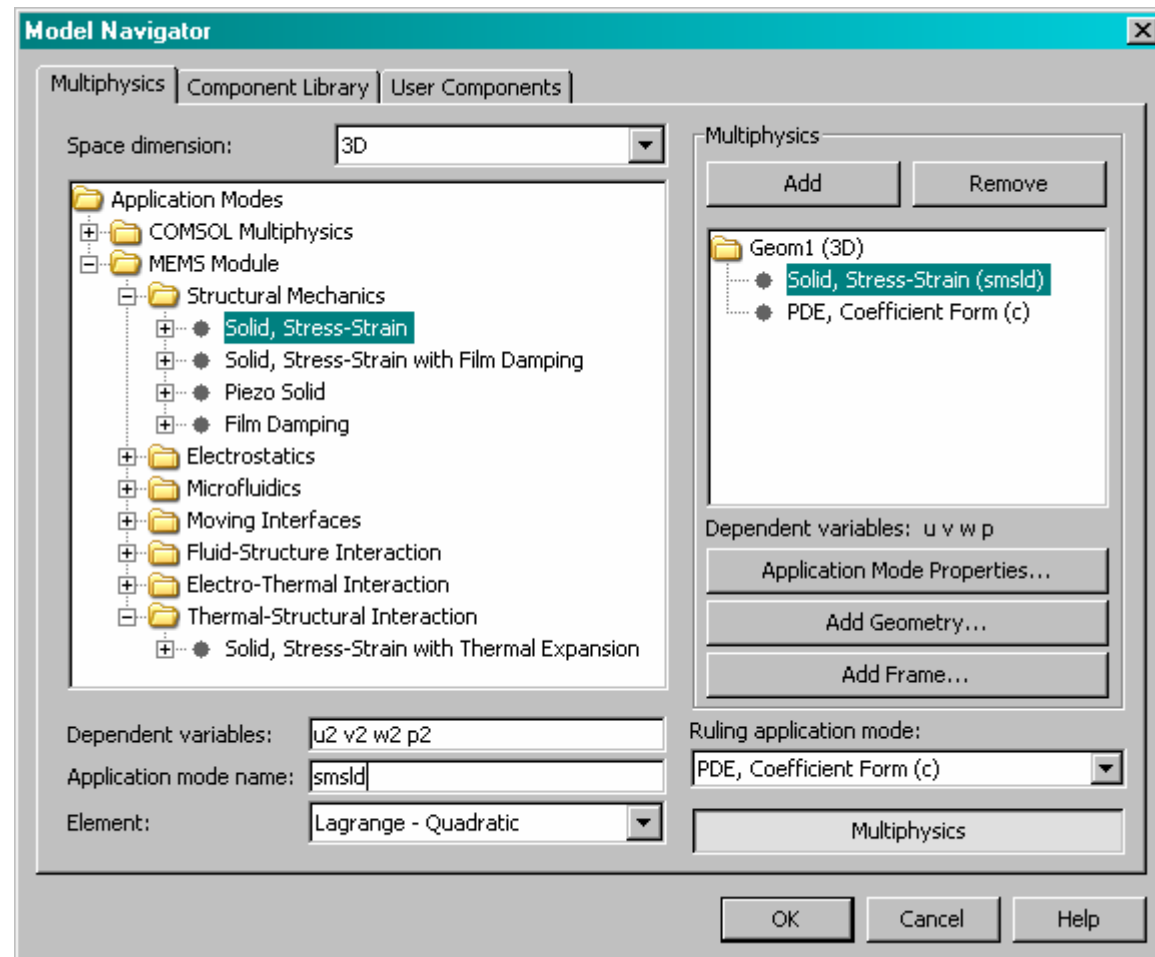
Example for a more “complex” element geometry: The copper electrodes are laterally connected (with respect to the temperature gradient). Left side: Temperature distribution, the top is set to 10°C, the base is at 0°C. The appropriate Voltage is shown in the middle; the left graph shows the voltage color coded electric streamlines and the temperature as a slice plot.



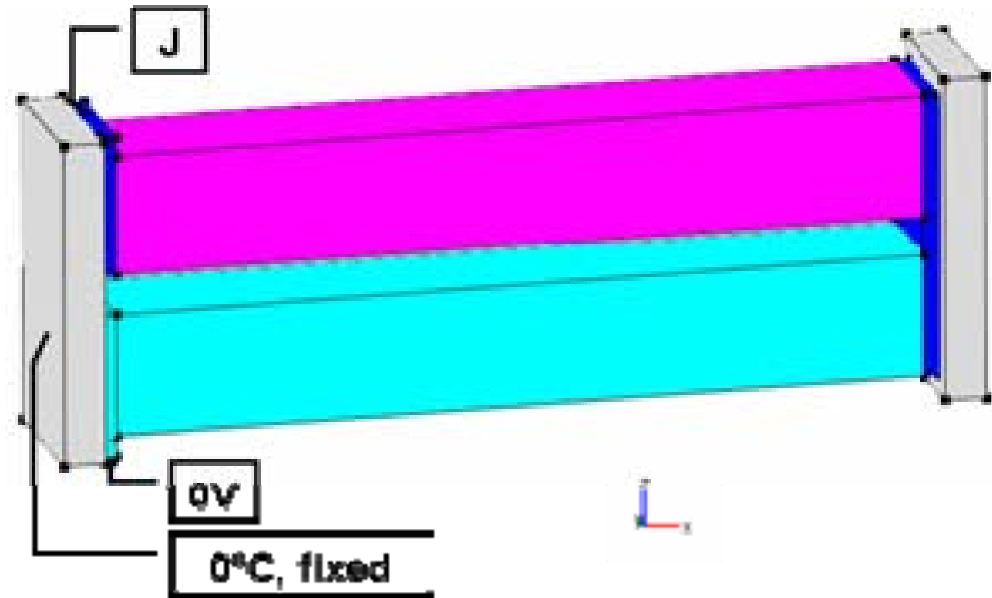
Thermal- electric- mechanic effects

Temperature
Voltage
Displacement
Stress

- thermoelectric effects
- strain
- thermal expansion
- no piezo-effect



Thermoelectric and thermomechanic effects



Elastic material properties of Bi_2Te_3 c_{ij} in 10^{11}dyn/cm^2 at 280K

| | | | | | |
|--|----------|----------|----------|----------|----------|
| c_{11} | c_{66} | c_{33} | c_{44} | c_{13} | c_{14} |
| 6.847 | 2.335 | 4.768 | 2.738 | 2.704 | 1.325 |
| Thermal expansion coefficient $a_i / 10^{-6}/\text{K}$ at 300K of Bi_2Te_3 | | | | | |
| a_x | a_y | a_z | | | |
| 21.3 | 14.4 | 14.4 | | | |

Landolt-Börnstein; Numerical data; ISBN3540121609; Vol 17f, pp.275, 1983

| Thermoelectric material properties | | Thermoelectric Material Bi_2Te_3 based | Electrode (Copper) |
|------------------------------------|-------------------|--|--------------------|
| Seebeck Coefficient | α , V/K | $p: 200e-6$ $n: -200e-6$ | $6.5e-6$ |
| Electric conductivity | σ , S/m | $1.1e5$ | $5.9e8$ |
| Thermal conductivity | λ , W/m/K | 1.6 | 350 |

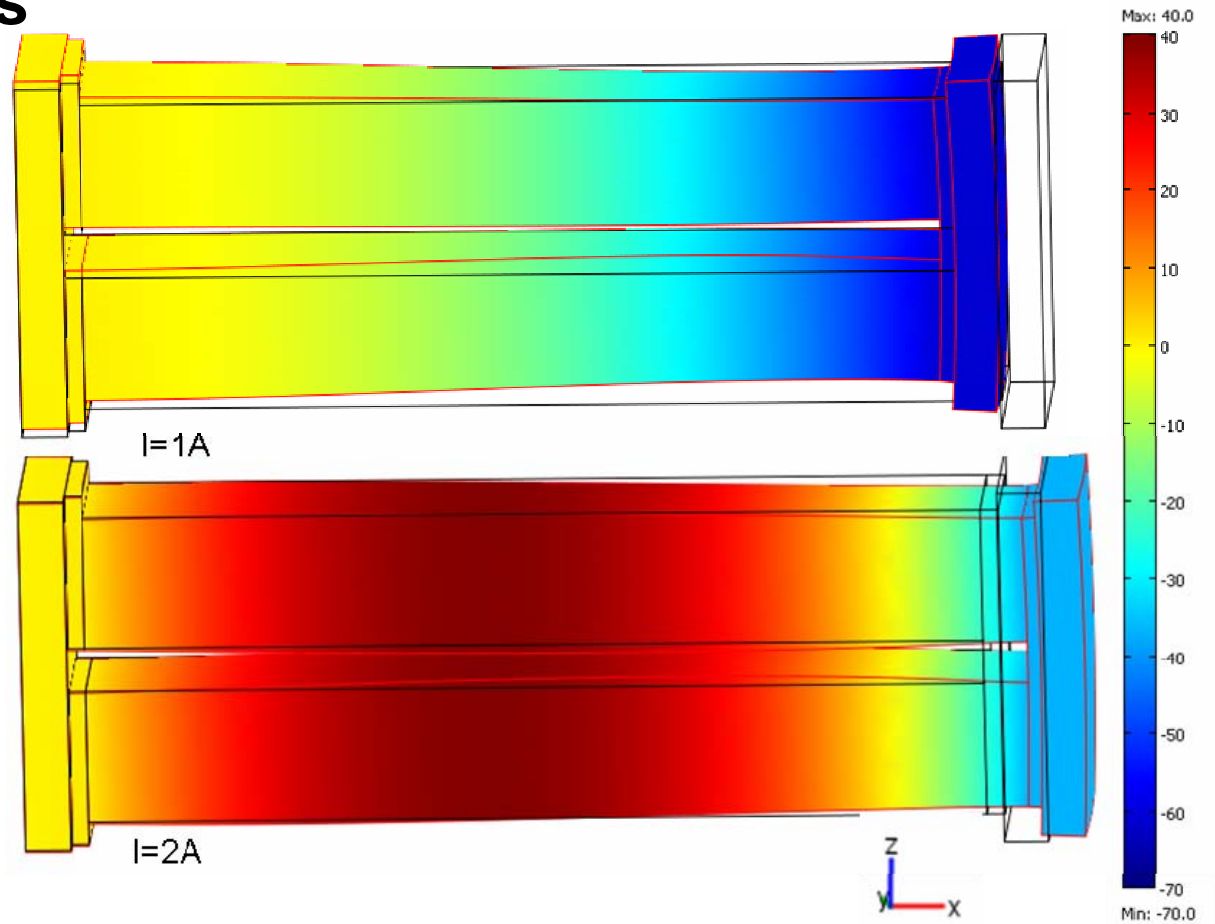
Antonova et al., ICT 2005

Thermoelectric and thermomechanic effects

Example:
Displacement due to thermal expansion

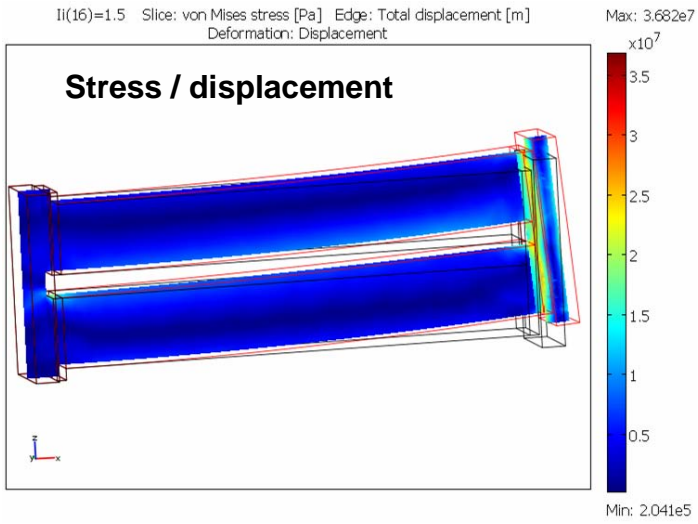
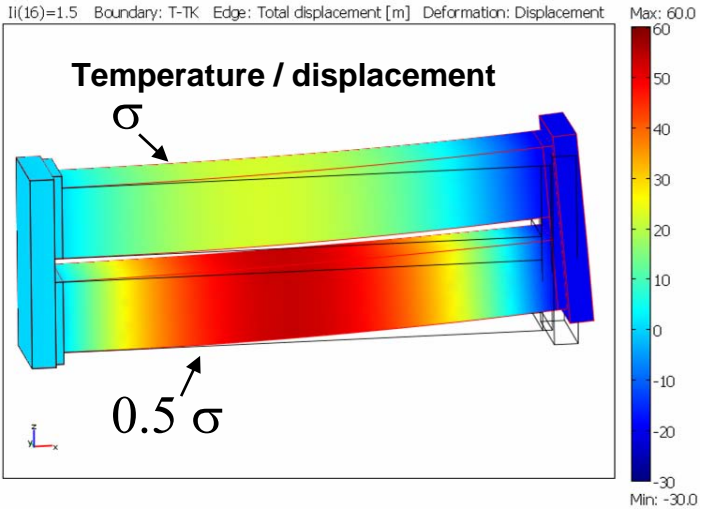
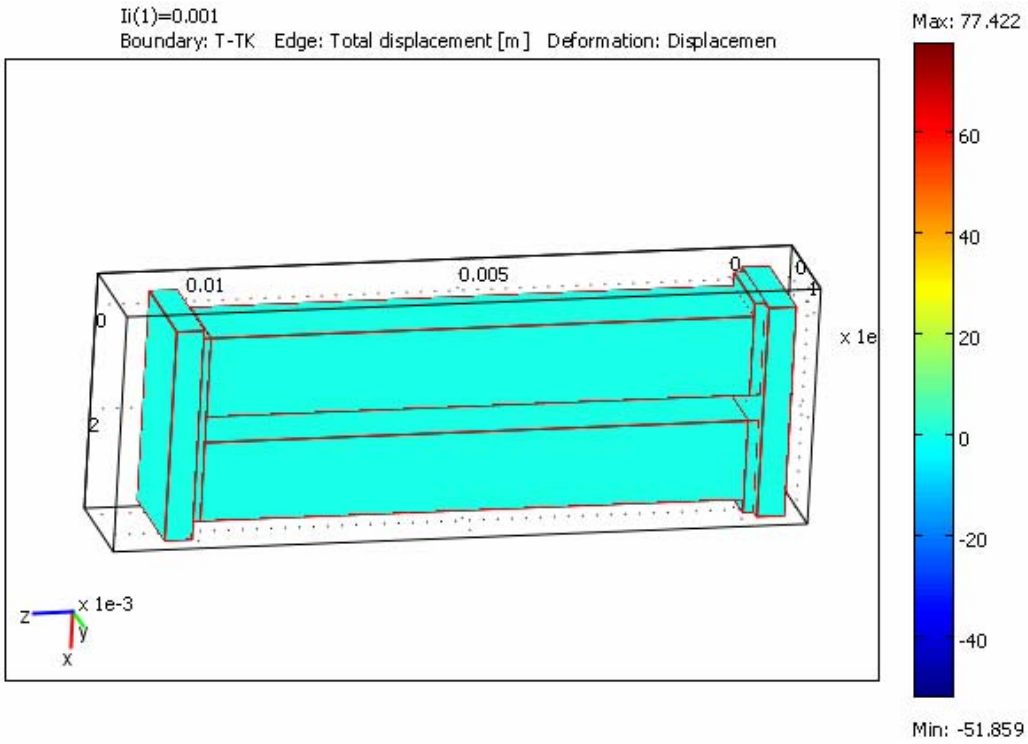
5 microns shrunken at 1A

4 microns expanded at 2A
(still cooling)



Thermoelectric and thermomechanic effects

Example: asymmetric material properties



Summary

Thermoelectric effects in COMSOL for modeling of thermoelectric cooling, generation and sensing

Temperature and position dependent material properties

Anisotropic materials (not shown here for thermoelectrics)

Arbitrary geometries

Graded/ stacked materials

Determination of effective material properties (no quantum effects)

Simultaneous modeling of thermoelectric systems including

-Mechanical effects, strain, stress

-Thermomechanical effects

-Convection (not shown here)

-Radiation (not shown here)

-...

Multiphysics Simulation of Thermoelectric Systems

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