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MultiPhysics Analysis of Trapped Field in Multi-Layer YBCO Plates

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- What are Trapped Flux Magnets (TFM)
- Applications of Trapped Flux Magnets
- Performance of bulk YBCO TFM
- Principle of flux trapping
- Modeling superconducting material
- Definition of the problem
- Implementation in COMSOL
- Simulation results

- Superconductors exhibit a non-measurable electrical resistance when operating below a critical surface (J, B, T)
- Lenz' law states

$$e = -\frac{d\phi}{dt}, e = \rho \cdot j \quad \xrightarrow{\rho = 0} \quad \phi = \iint_S \vec{B} d\vec{S} \quad \text{is constant}$$



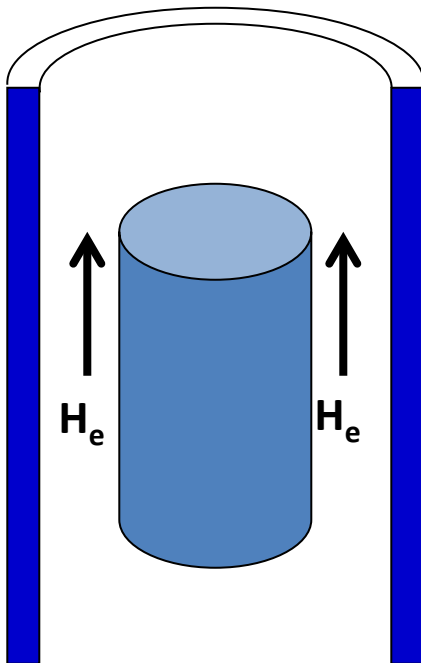
Trapped flux magnets:
 YBCO single grain
 17 T @ 29 K
 Constant magnetic flux

Permanent magnets:
 NdFeB, SmCo...
 < 1 T @ room temperature
 Constant magnetization

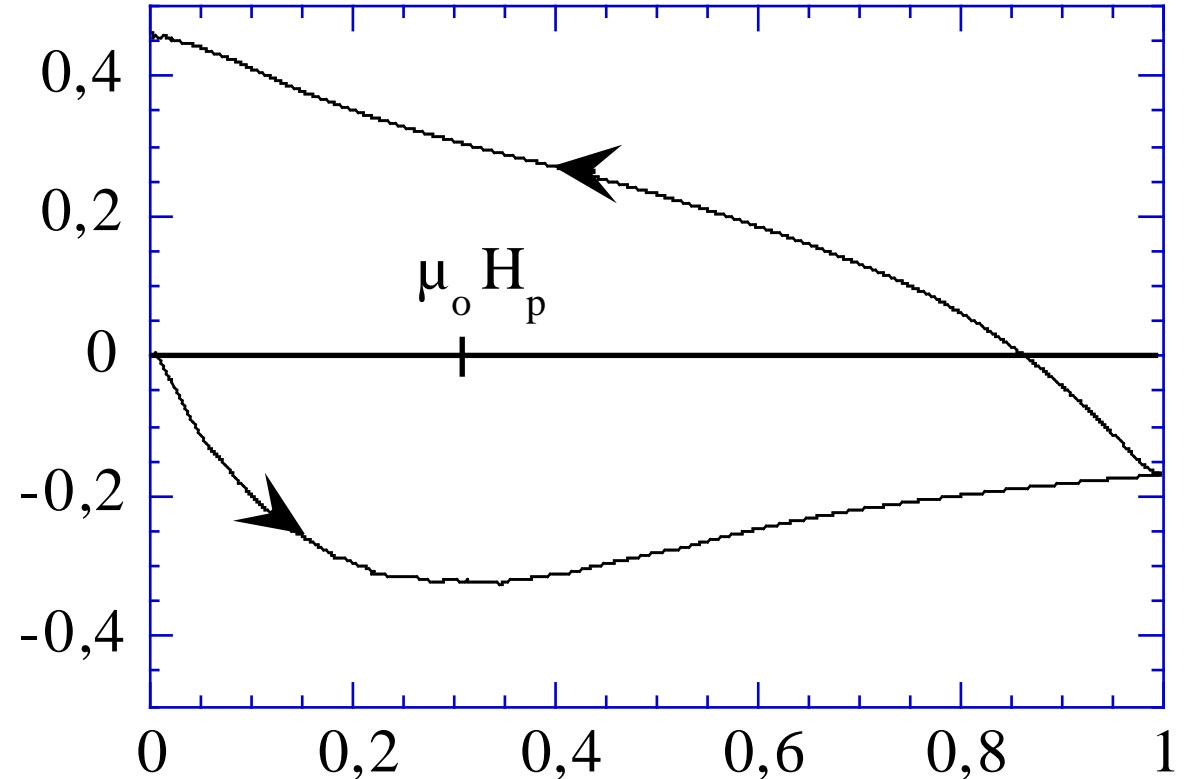
Magnetization of a Superconductor

- Lenz law
- Critical state model

– $J = 0$ or $\pm J_c$

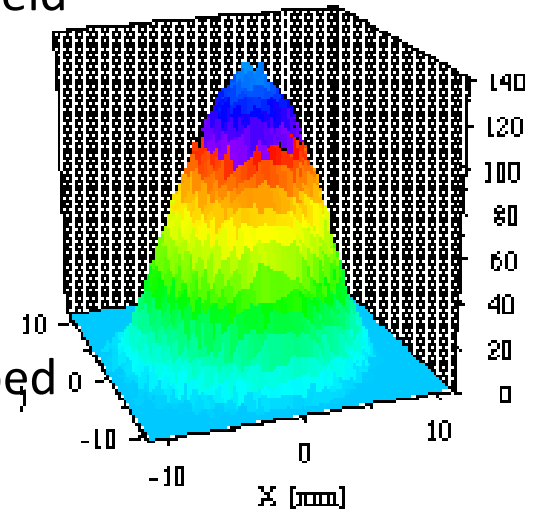


$\mu_0 M$ (T)

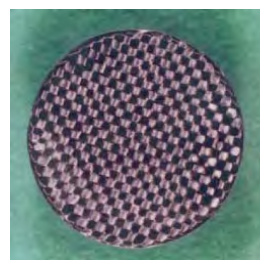
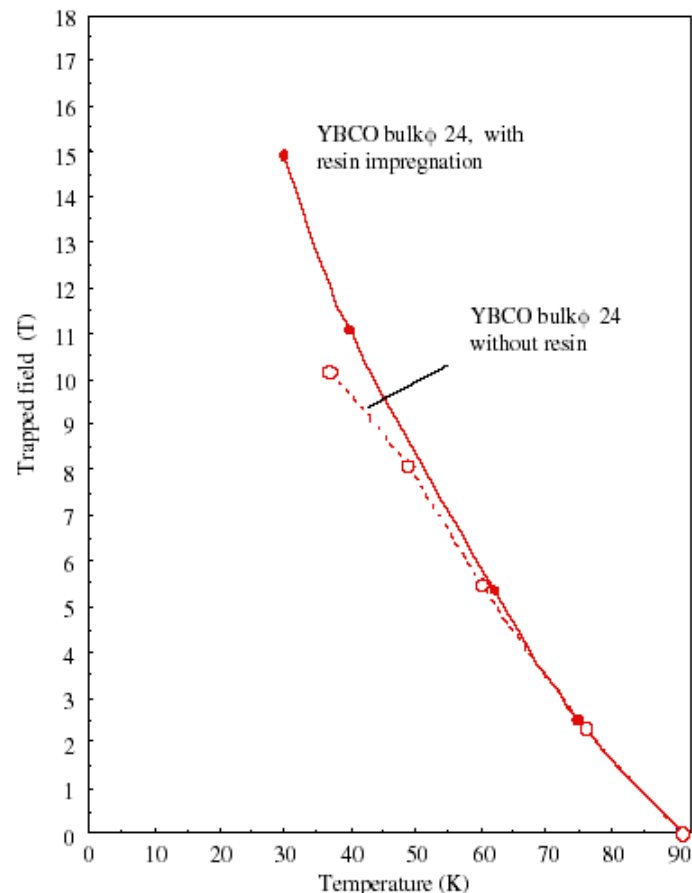


$\mu_0 H_{ext}$ (T)

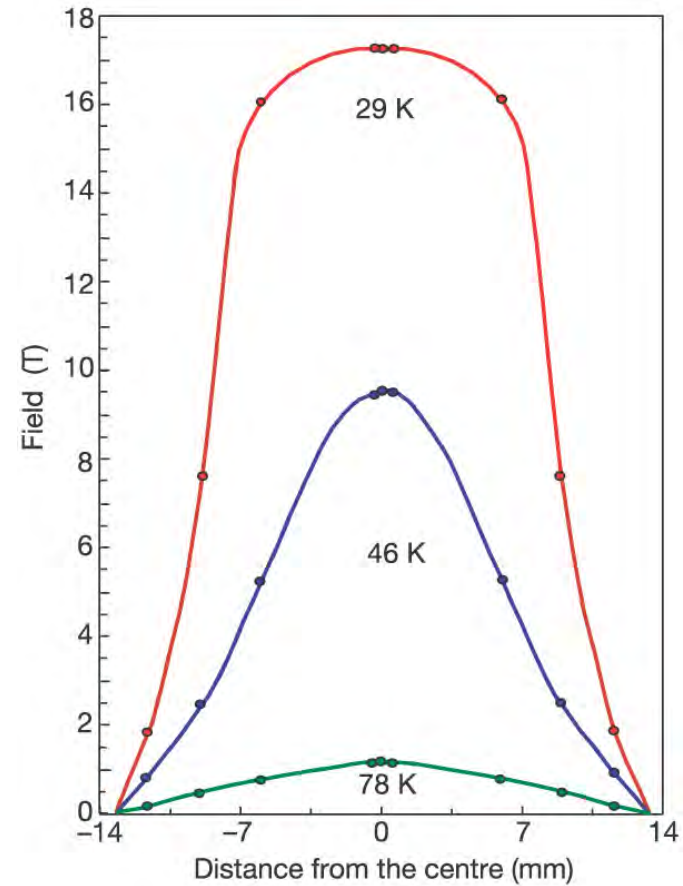
- Field cooling
 - Cool down of the superconductor under applied field
 - Very effective
 - Require large magnets providing $B_{trapped}$
- Zero field cooling
 - Requires full saturation in current
 - Require large magnets providing at least $2 * B_{trapped}$
- Pulsed magnetization
 - Require energy storage for pulse generation
 - Generates losses in the superconductor (flux flow)
- Flux pumping
 - Complex to set up
 - Requires controllable temperature and magnetic gate material



- Flux Trapping up to 17 Tesla at 30K !

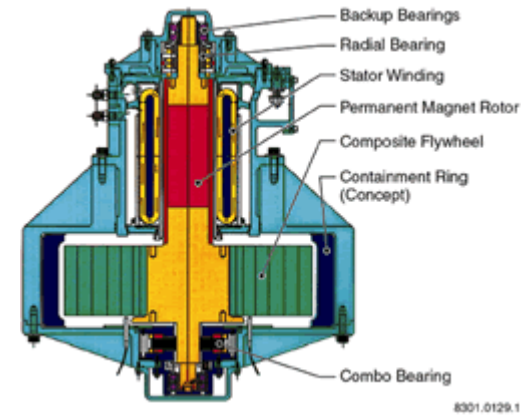


Resin impregnated YBCO pellets

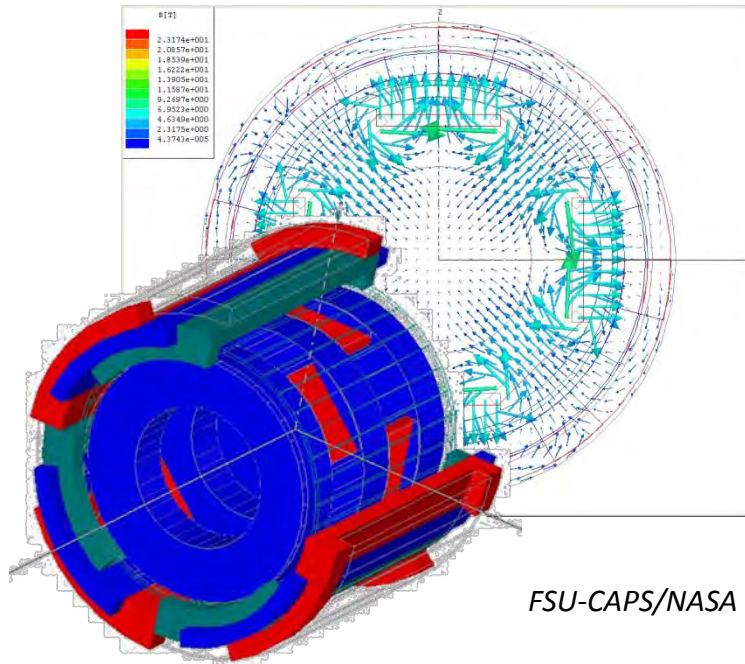


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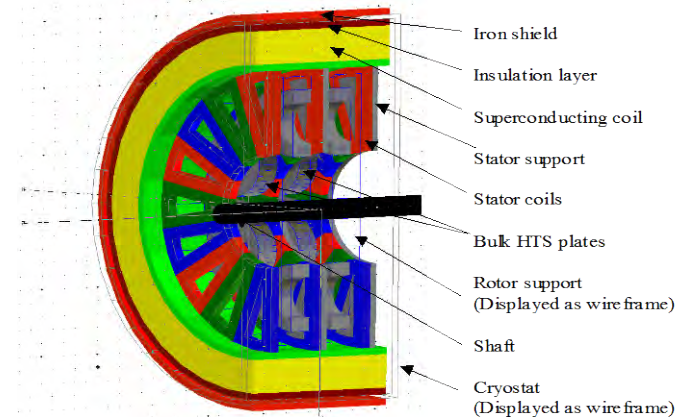
- High power density rotating machines
 - Challenges: trapping the flux
 - Not very scalable
 - Very high excitation field
- Magnetic bearings (Flywheels)
 - Intrinsically stable
 - No control required



Georgia Tech design



FSU-CAPS/NASA



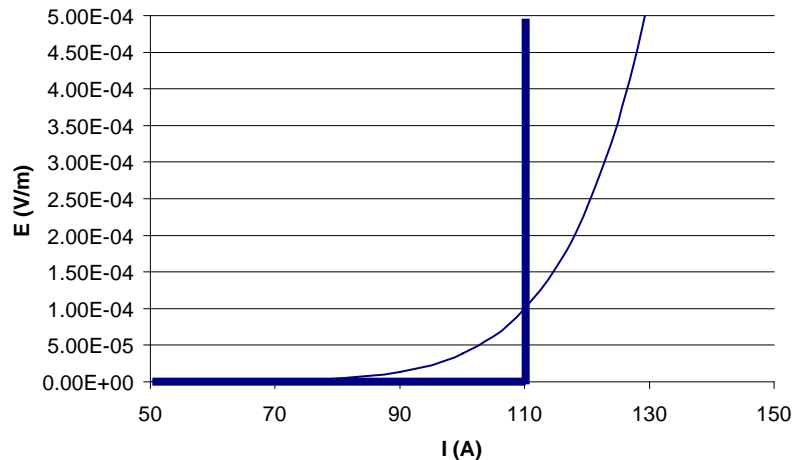
FSU-CAPS/NASA

Equations to solve:

For a given operating temperature:

$$E = E_c \left(\frac{j}{j_c} \right)^n$$

Bean's model



Valid Maxwell's equations:

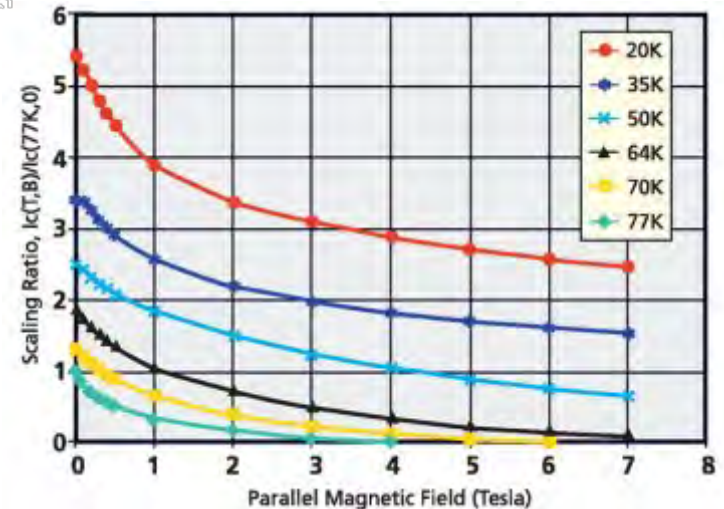
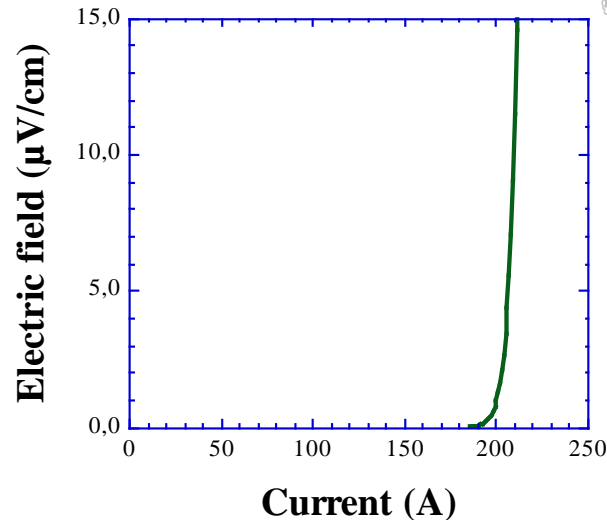
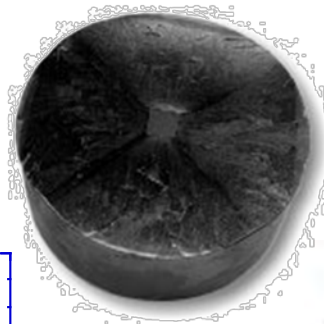
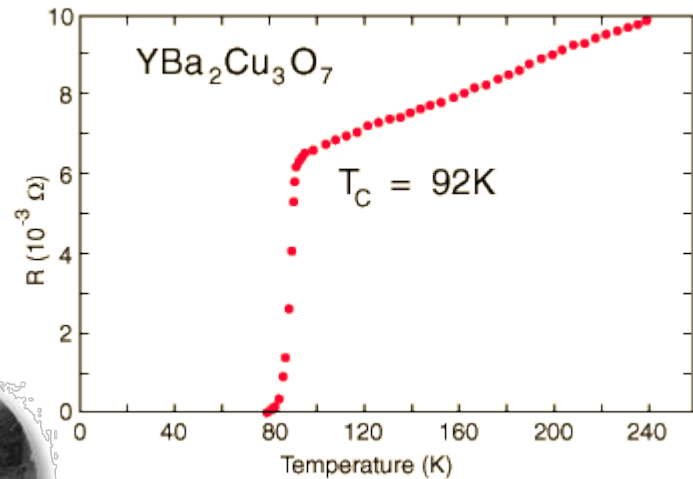
$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\vec{\nabla} \times \vec{B} = \vec{j}$$

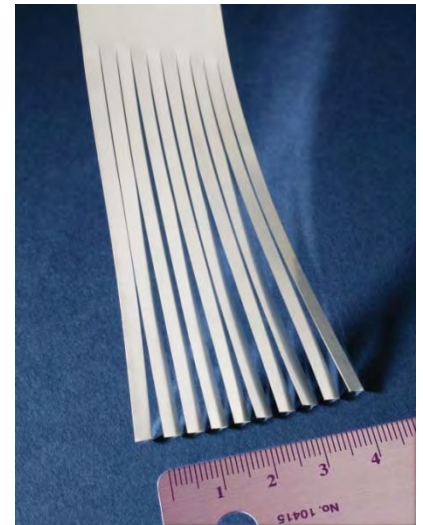
Magnetic behavior:

$$\vec{B} = \mu_0 \vec{H}$$

- $T_c \sim 92\text{ K}$
- J_c depends on B and T
- Non-linear $E(J)$ characteristic (Ohm's law not valid anymore)



- Bulk material
 - Ceramic material
 - Structural limits (forces on vortices)
 - Problem to grow large grains
- Multilayer configuration
 - Deposition of films (proved technology)
 - Stack more stable mechanically (better pinning)
 - Lower packing factor but higher current density
- Need to evaluate the configuration through numerical analysis
 - Flux trapping capability
 - Stability against thermal disturbances

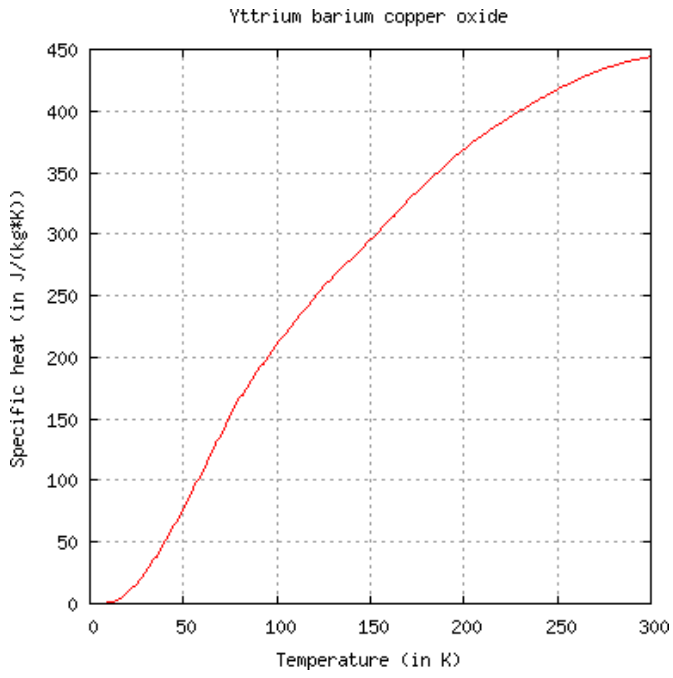


American Superconductor

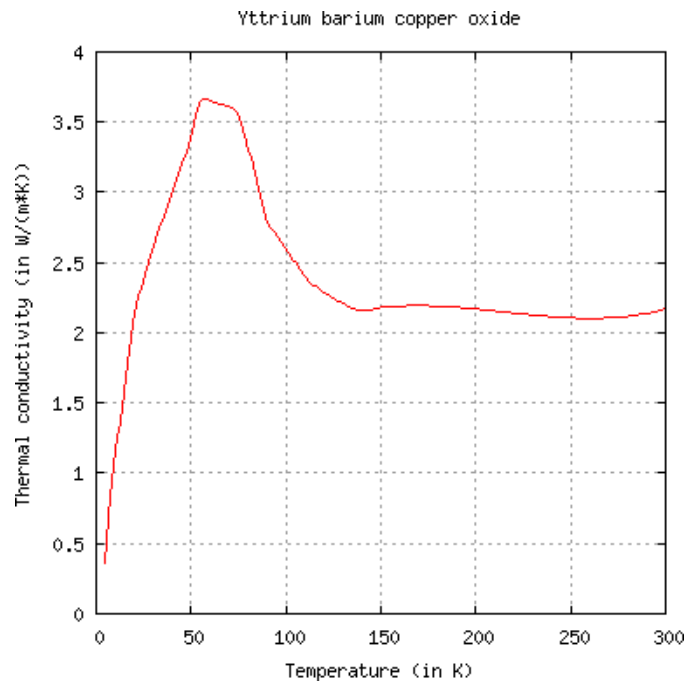
Electrical conductivity model:
Non-linear with strong dependence
upon E, T and B

$$\sigma[S/m] = \frac{J_{c0}}{E_c} \left(1 - \left(\frac{T}{T_c} \right)^2 \right)^{\frac{3}{2}} \left(\frac{1}{1 + \frac{B}{B_0}} \right) \left(\frac{E}{E_c} \right)^{\frac{1}{n}-1}$$

Permeability of vacuum: $\mu_r = 1$

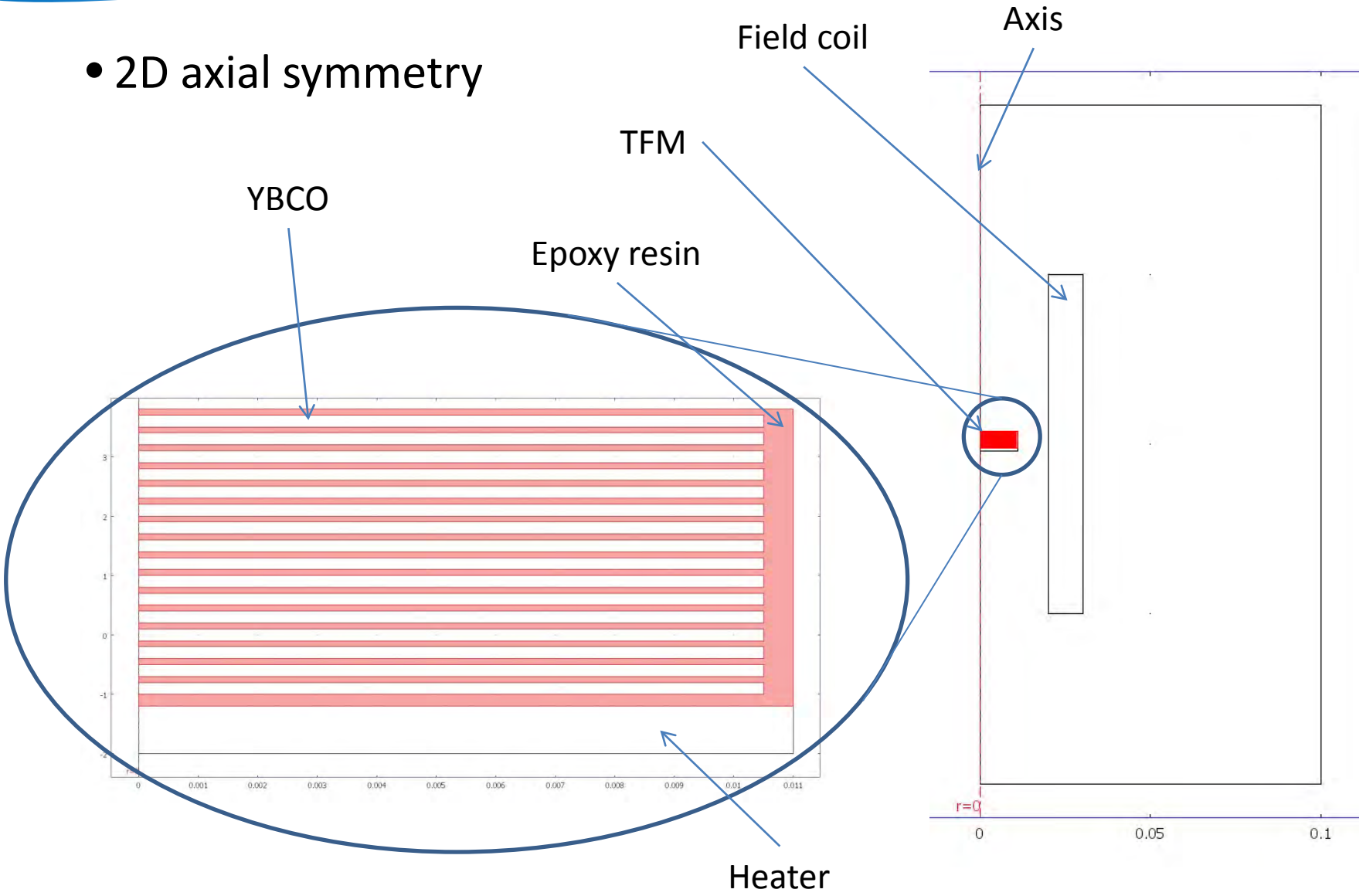


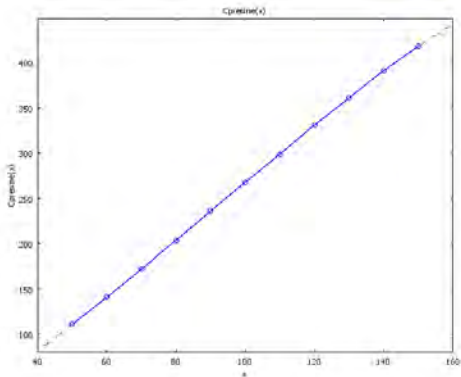
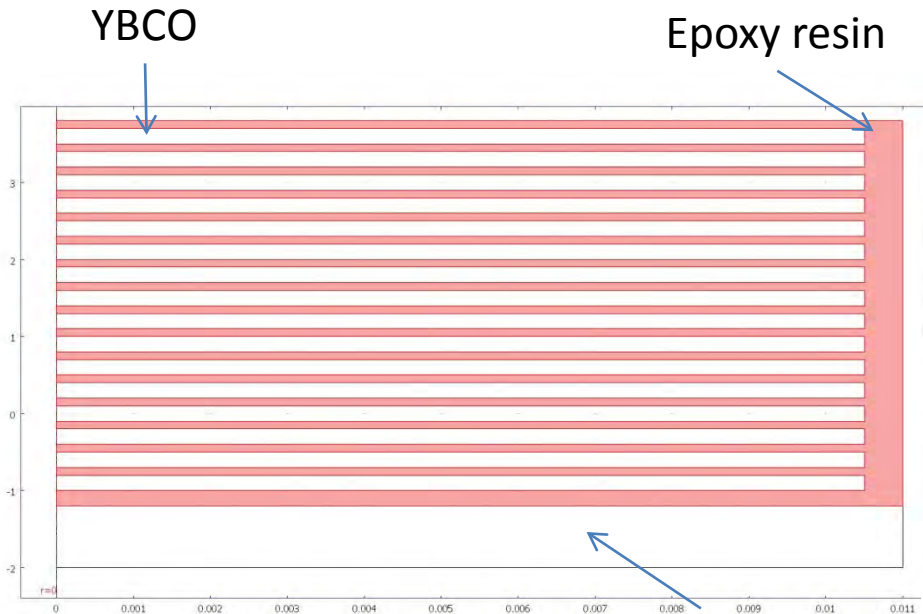
Specific heat of YBCO



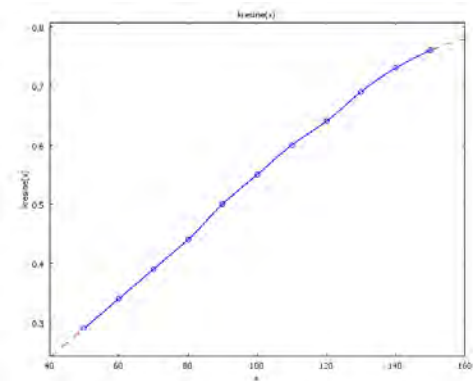
Thermal conductivity of YBCO

- 2D axial symmetry

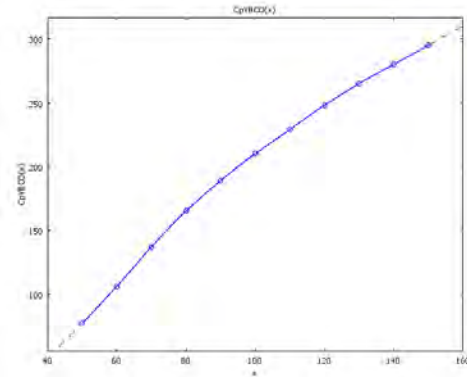




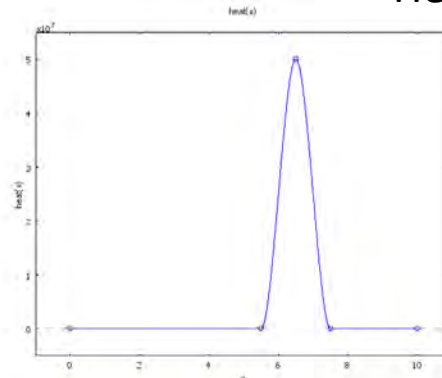
Heat capacity of resin



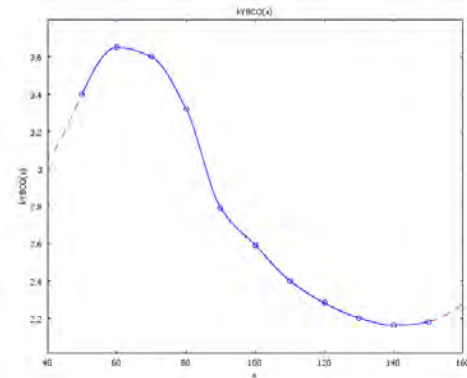
Thermal conductivity of resin



Heat capacity of YBCO

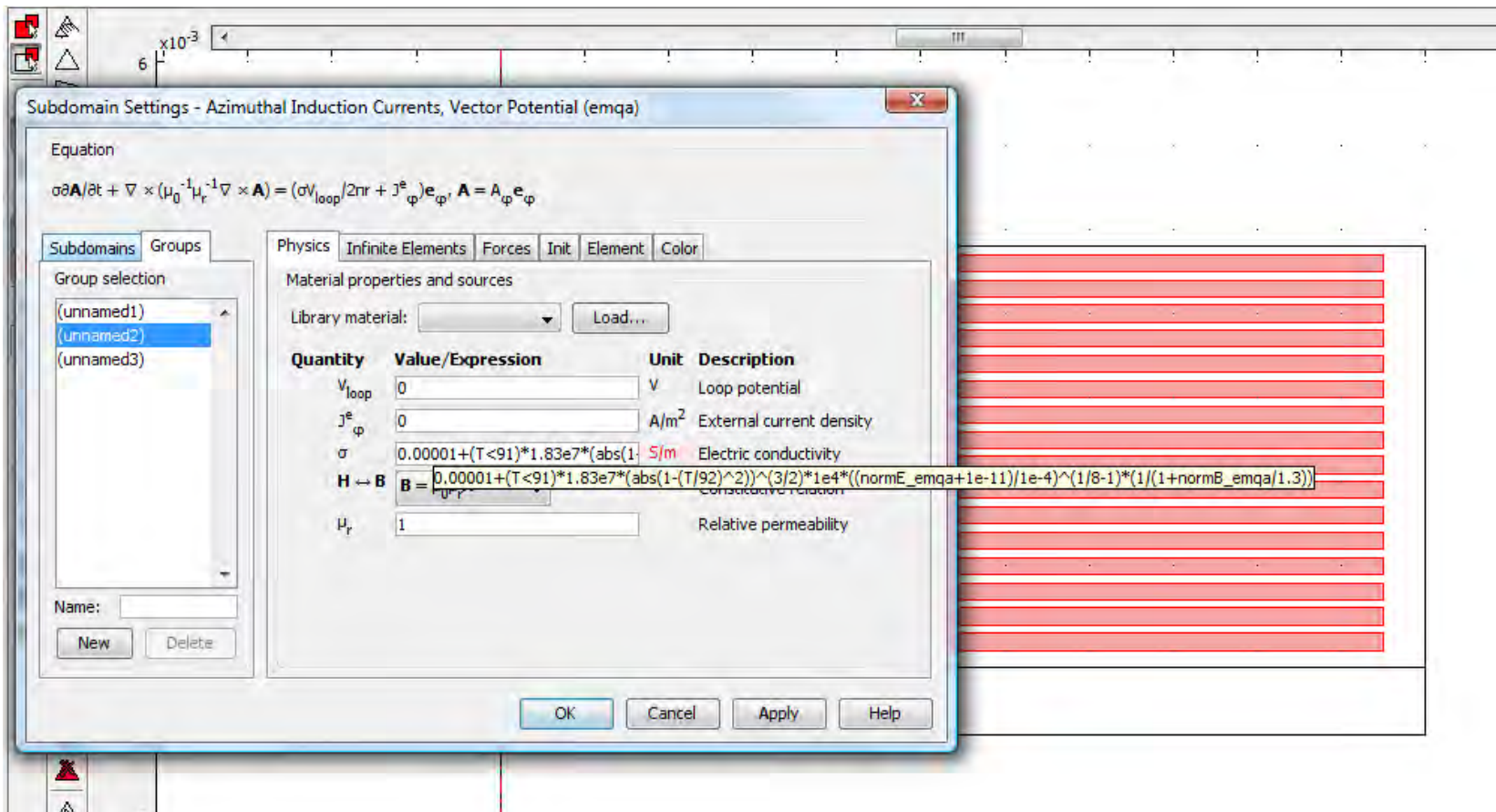


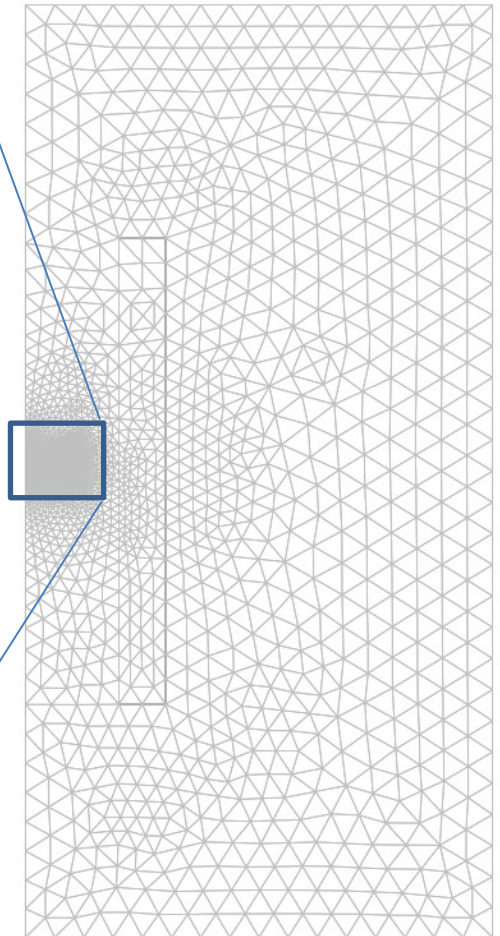
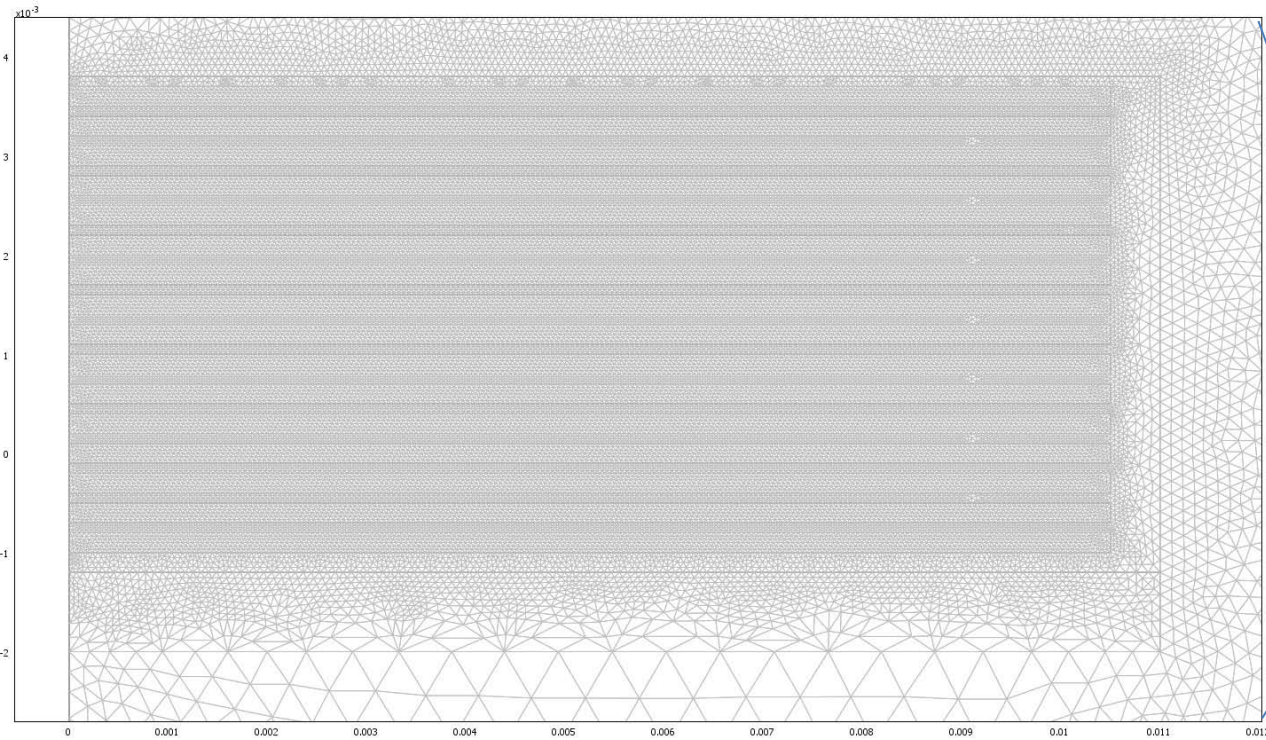
Heat pulse



Thermal conductivity of YBCO

- Linear variation of current density in field coil
- Non linear electrical conductivity in superconductor





- Coarse mesh in air and in the field magnet
- Fine mesh in the multilayer system
- ~ 80,000 elements
- Number of d.o.f. ~305,000

Initial state

Steady state analysis

- Bcoil applied
- $T = 85\text{ K}$



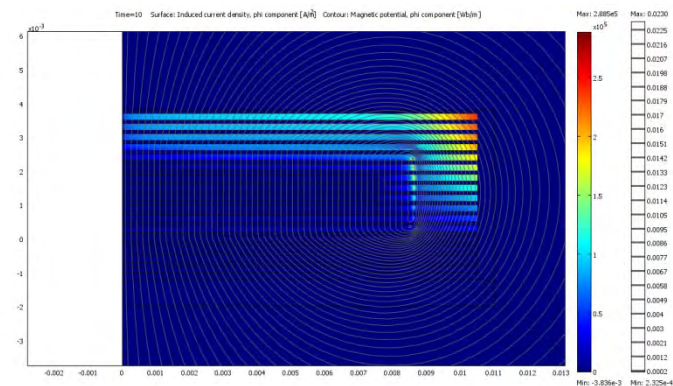
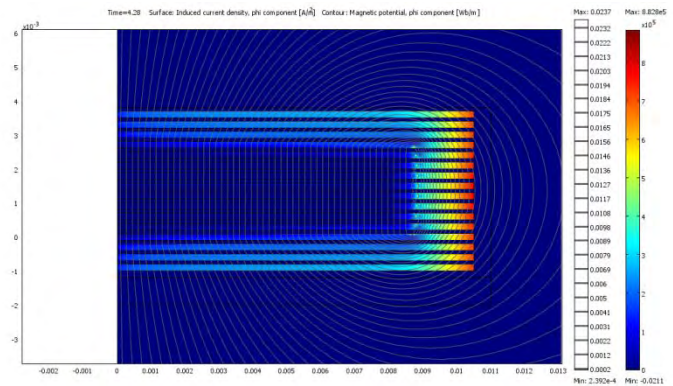
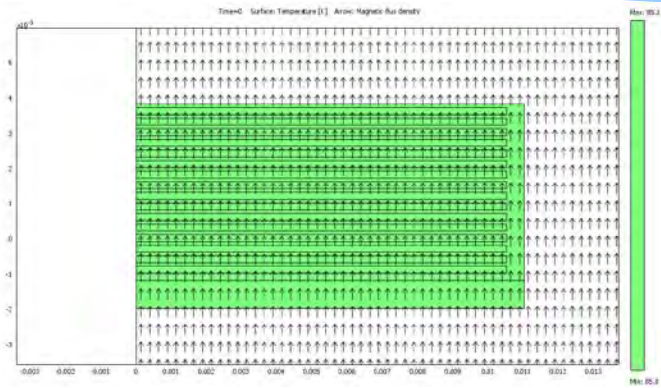
Transient analysis

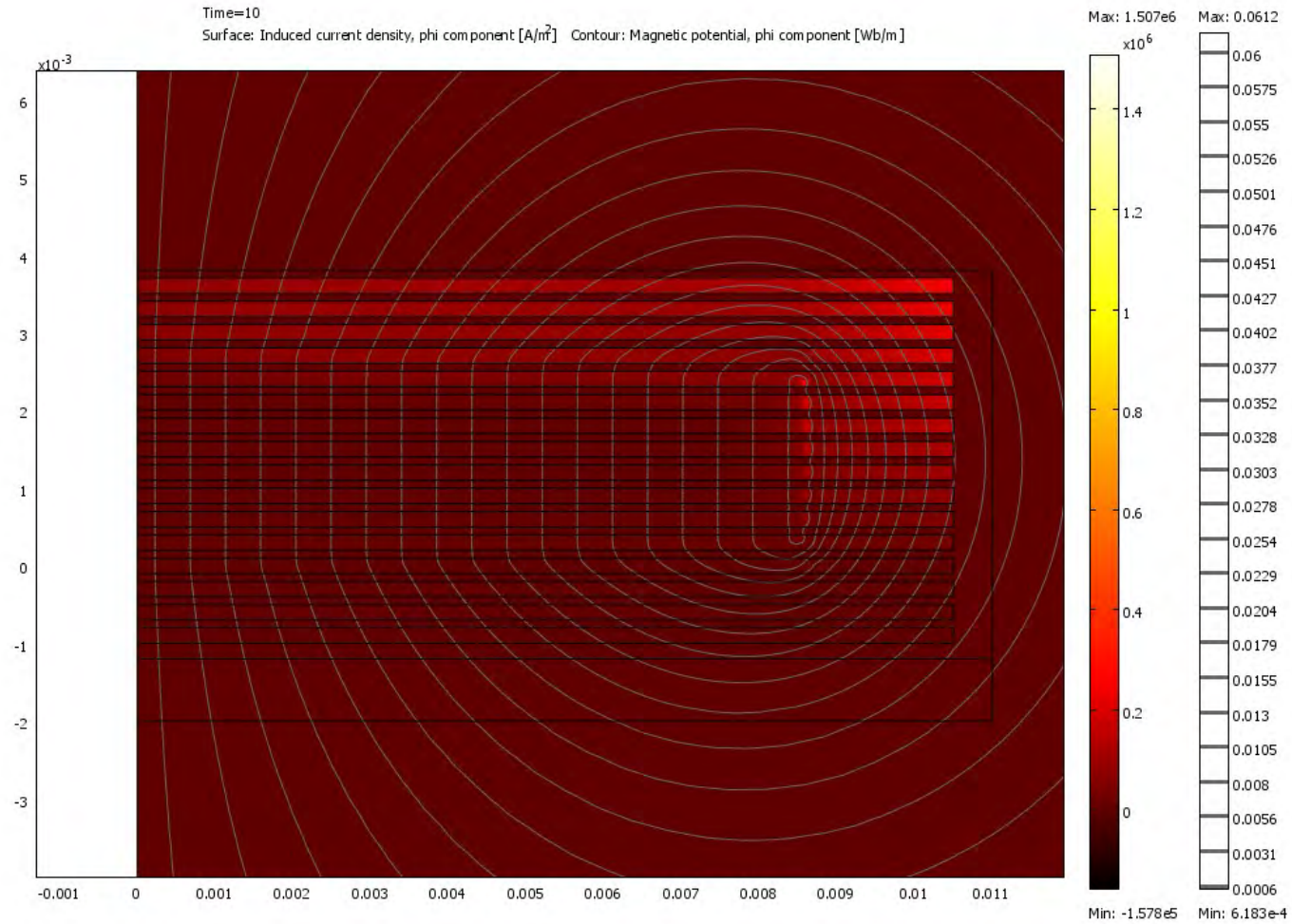
- Jcoil ramped down to 0
- Constant temperature



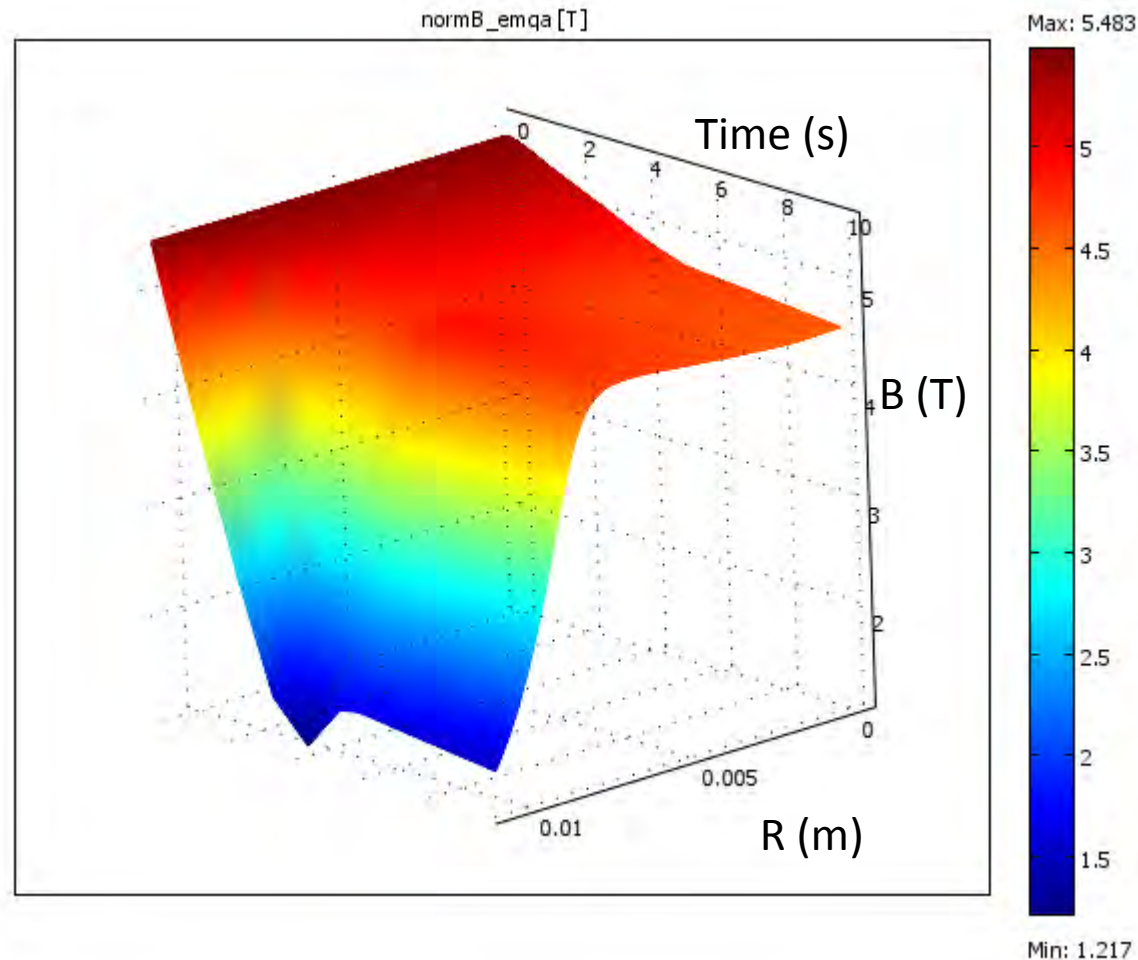
Transient analysis

- Jcoil=0
- pulse of heat applied

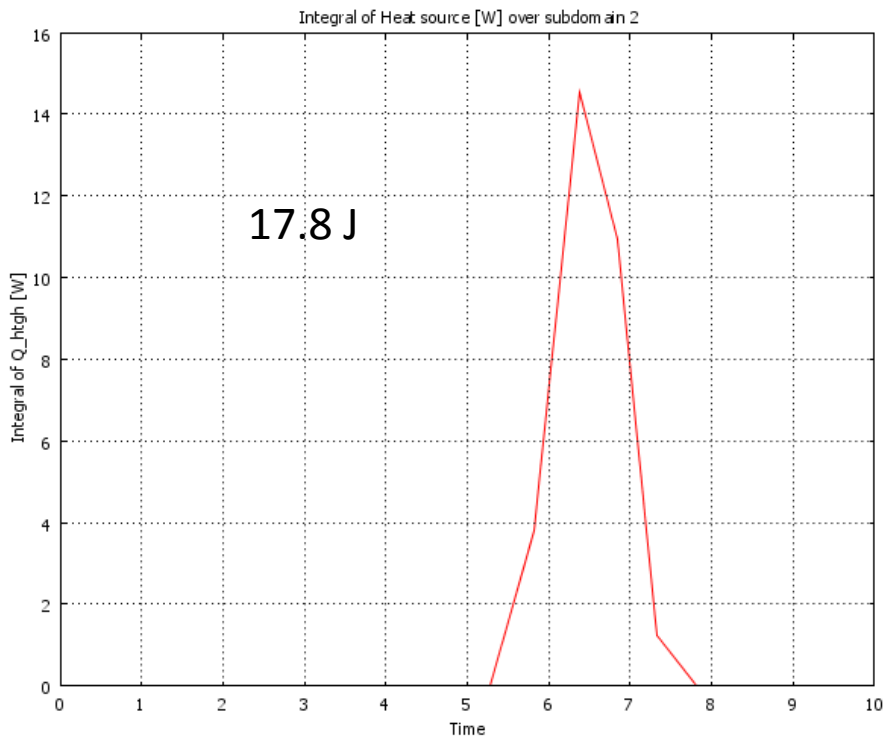




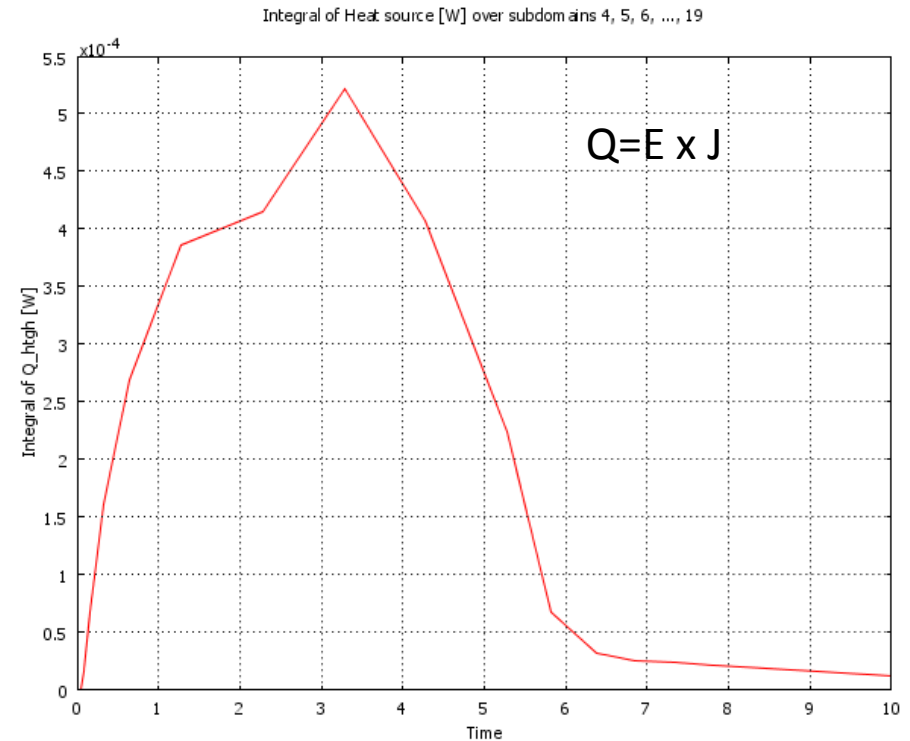
- Field variation of about 7% after heat pulse is applied



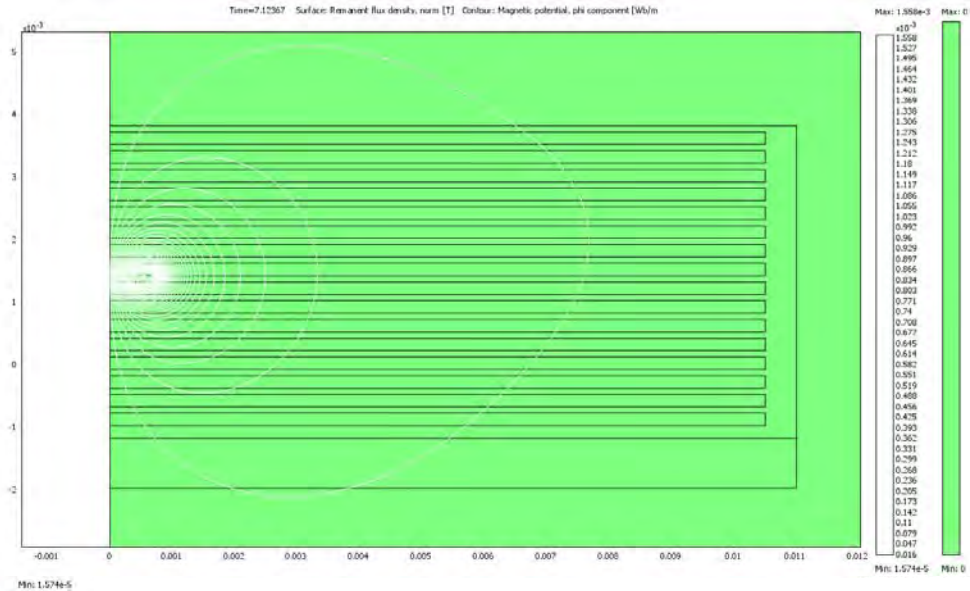
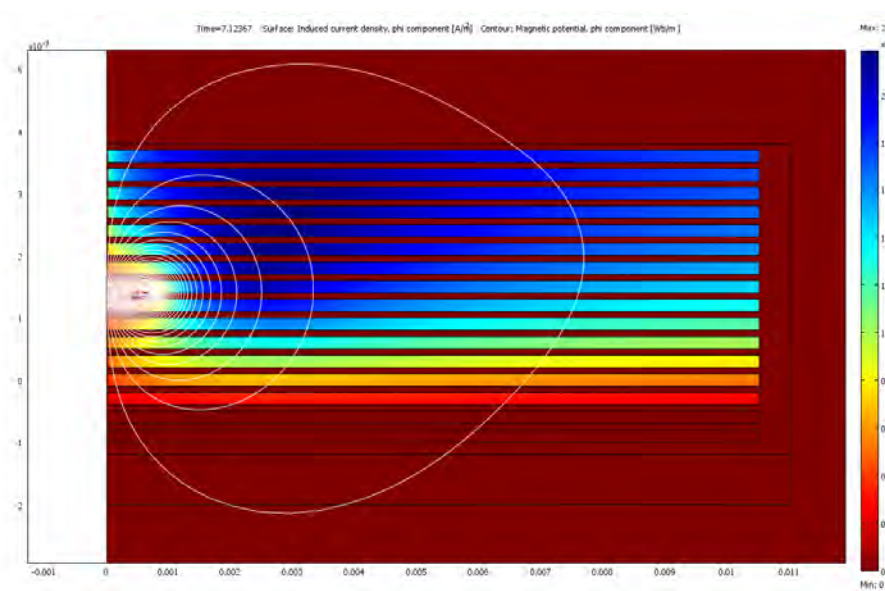
- Heat pulse in heater
 - peak at 14 W
 - ~ 18 J



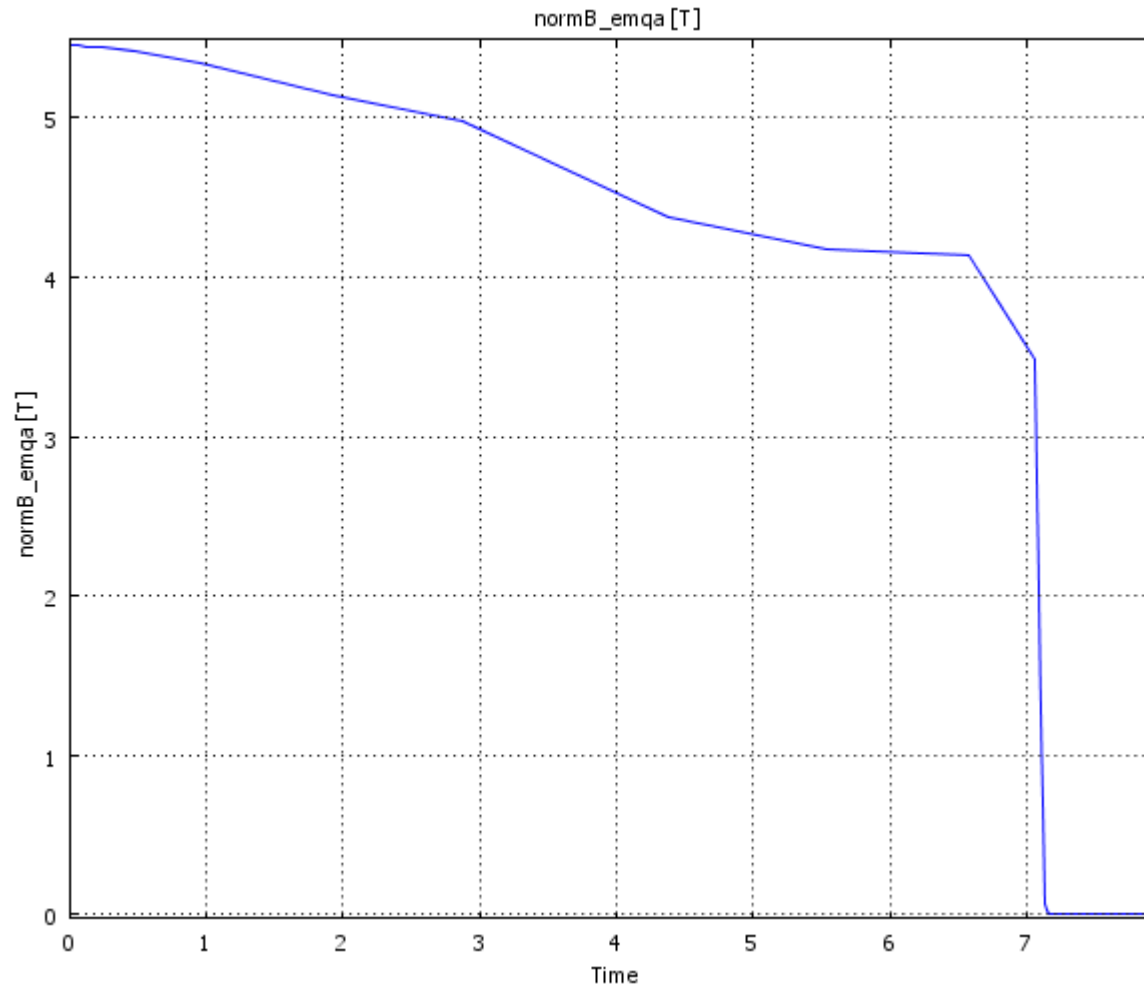
- Losses in superconductor
 - Peak ~0.6 mW
 - ~ 2 mJ
 - Depends on speed of flux variation



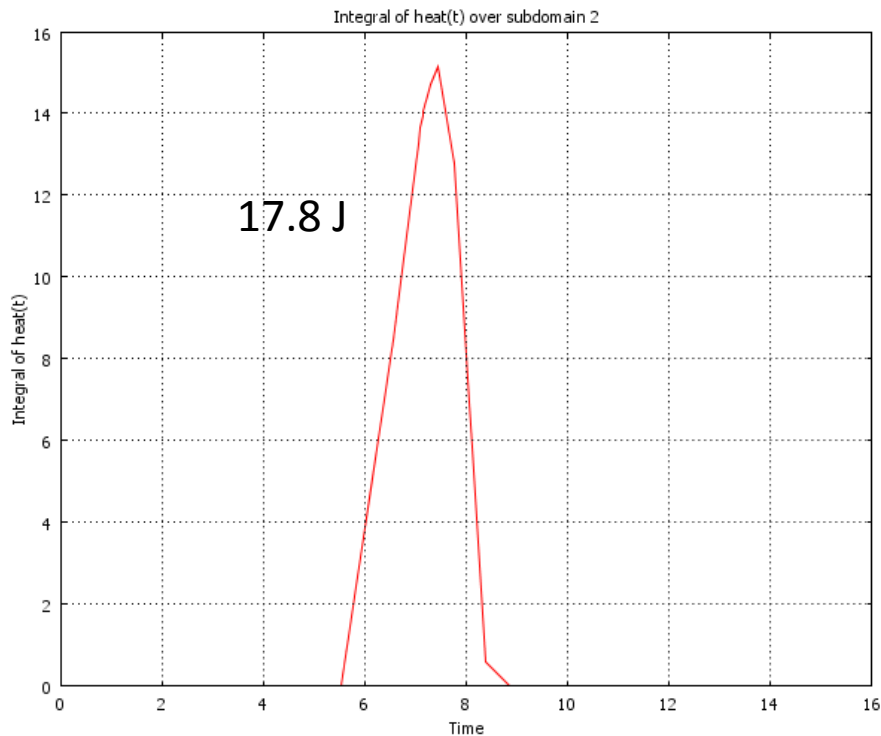
- In case of a large heat pulse trapped flux is dissipated



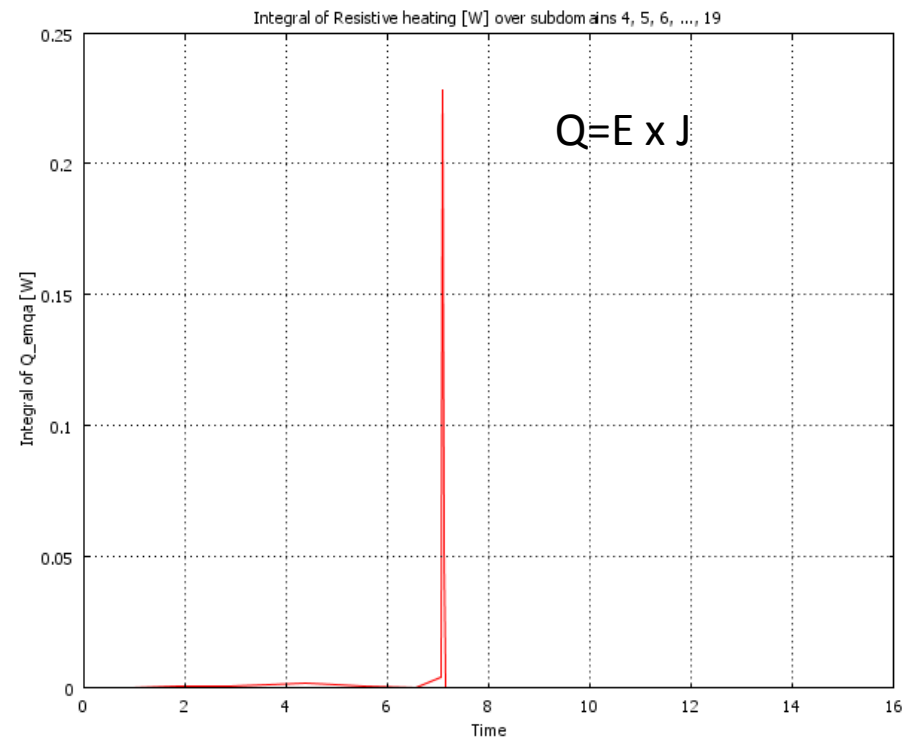
- All the energy is dissipated at the beginning of the heat pulse



- Heat pulse in heater
 - peak at 15 W
 - ~ 20 J



- Losses in superconductor
 - Peak ~0.22 W
 - ~ 20 mJ
 - Depends on speed of flux variation



- Multilayer TFMs are very promising
 - Remove existing limitations of bulk material
 - Allow for larger size
- Comsol allows for a better understanding of the physics of TFMs
- Comsol was able to handle the challenging simulation
 - Highly non linear problem
 - Electrical conductivity depending non-linearly on E
 - Non linear thermal properties
 - Electromagnetics-thermal coupling