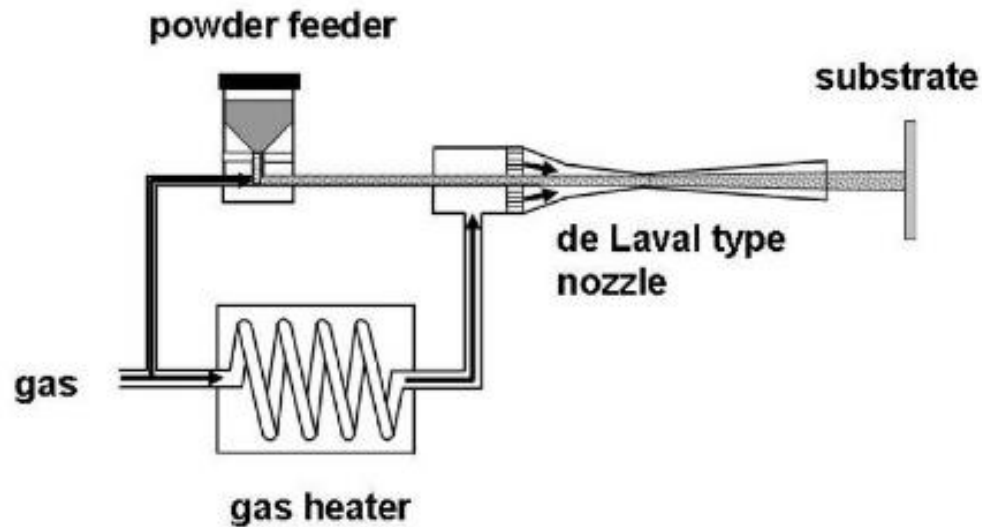


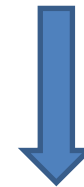
# **Oxidation of Titanium Particles during Cold Gas Dynamic Spraying**

# Cold Spray method



Process gases:

- Nitrogen
- Helium

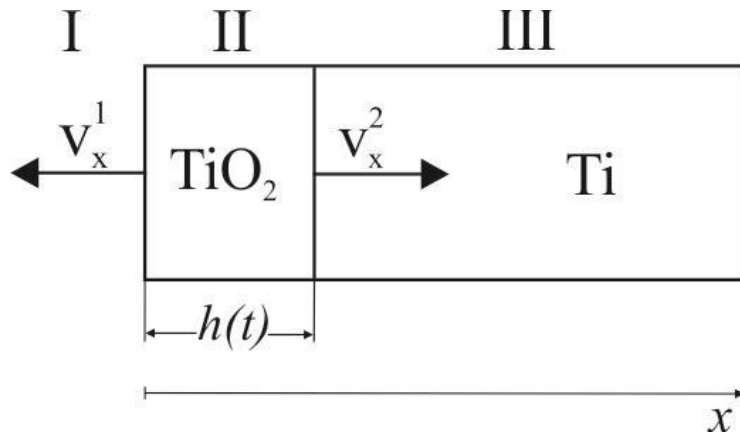


AIR ?

Fig 1. Schematic diagram of the cold spray process[1]

[1]J. Voyer, T. Stoltenhoff, H. Kreye, in: C. Moreau, B. Marple (Eds.), Thermal Spray 2003: Advancing the Science & Applying the Technology, ASM International, Materials Park, OH, USA, 2003, p. 71

# Oxidation model

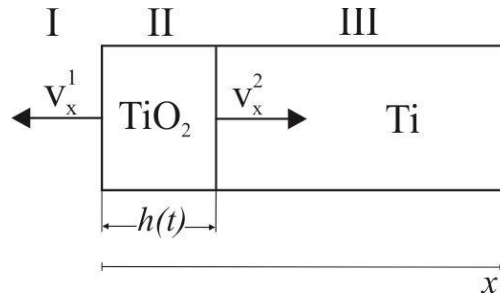


Regions:

I - the air surrounding the sample,  
II – formed titanium dioxide,  
III - titanium

Fig 2. Schemat of 1D oxidation problem

# Oxidation model



- **mass balance for O<sub>2</sub>:**

$$\frac{\partial c_{O_2}}{\partial t} - D_{(O_2, TiO_2)} \frac{\partial^2 c_{O_2}}{\partial x^2} = 0,$$

where:  $D_{(O_2, TiO_2)}$  - diffusion coefficient of oxygen in titanium dioxide with following boundary conditions:  
 $c_{O_2} = c_0$  at  $x = 0$ ,  $c_{O_2} = 0$  at  $x = h(t)$

- **velocity of air-titanium interface (I/II):**

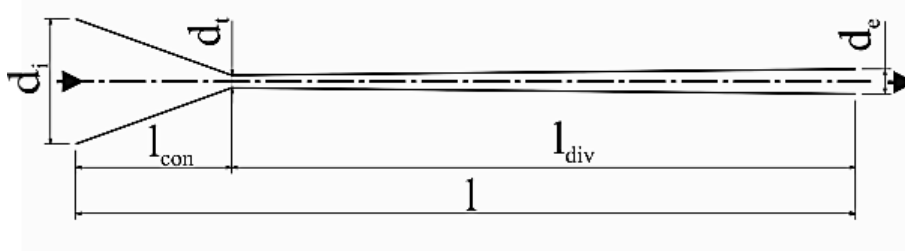
$$v_x^1 = -(1 - \gamma) \frac{R_i}{R_0} \frac{D_{(O_2, TiO_2)}}{c_{TiO_2}} \frac{\partial c_{O_2}}{\partial x} \Big|_{x=h(t)}$$

where:  $R_i$  – the length of titanium region (III),  $R_0$  – the length of oxidized titanium region (II),  
 $\gamma$  – the Pilling-Bedworth Ratio given by equation:  $\gamma \equiv \frac{c_{Ti}}{c_{TiO_2}} = \frac{\rho_{Ti}}{\rho_{TiO_2}} \frac{M_{(Ti)}}{M_{(TiO_2)}}$ ,  $c_{TiO_2} = 53.2$  kmole/m<sup>3</sup>,  
 $c_{Ti} = 93.9$  kmole/m<sup>3</sup>,  $c_0 = 12.5$  kmole/m<sup>3</sup>

- **velocity of the oxide-titanium interface (II/III)**

$$v_x^2 = - \frac{D_{(O_2, TiO_2)}}{c_{TiO_2}} \frac{\partial c_{O_2}}{\partial x} \Big|_{x=h(t)}$$

# Spraying parameters



Powder injection	$d_i$ [mm]	$d_t$ [mm]	$d_e$ [mm]	$l$ [mm]	$l_{con}$ [mm]	$l_{div}$ [mm]
axial	40	2	4	250	50	200

- Velocity of powder particles:**

$$m_p \cdot \frac{dv_p}{dt} = \frac{3 C_D \rho_g}{4 D_p \rho_p} (v_g - v_p) |v_g - v_p|$$

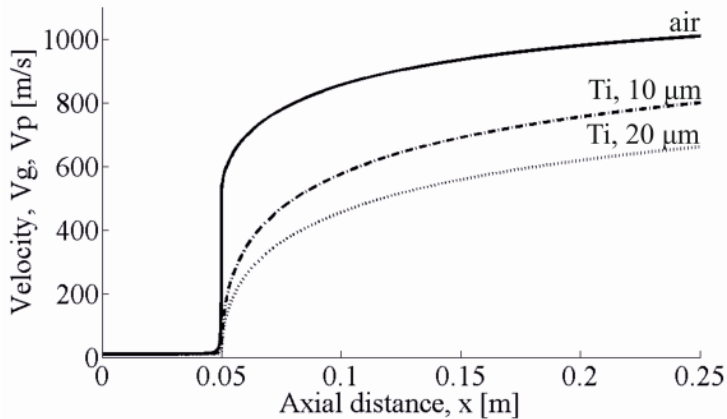
Where:  $C_D$  is the drag coefficient,  $v_p$  is particle velocity,  $v_g$  is gas velocity,  $\rho_p$  – density of particle material,  $\rho_g$  – density of gas

- Temperatures of powder particles**

$$\frac{dT_p}{dt} = v_p \cdot \frac{dT_p}{dx} = (T_g - T_p) \frac{6h}{c_{pp} \rho_p D_p}$$

where,  $T_p$  is particle temperature,  $T_g$  is gas temperature,  $c_{pp}$  is heat capacity of particle,  $v_p$  is particle velocity,  $C_{pg}$  is heat capacity,  $h$  is heat transfer coefficient related to the thermal conductivity of gas by Nusselt number (Nu)

# Spraying parameters



Particle's residence time in the nozzle  
 $\sim 0.0052$  s.

Fig 3. Titanium particles velocity during cold spraying

Diffusion coefficient[2]:

$$D_{(O_2, TiO_2)} = 870 \exp\left(-\frac{55535}{RT}\right)$$

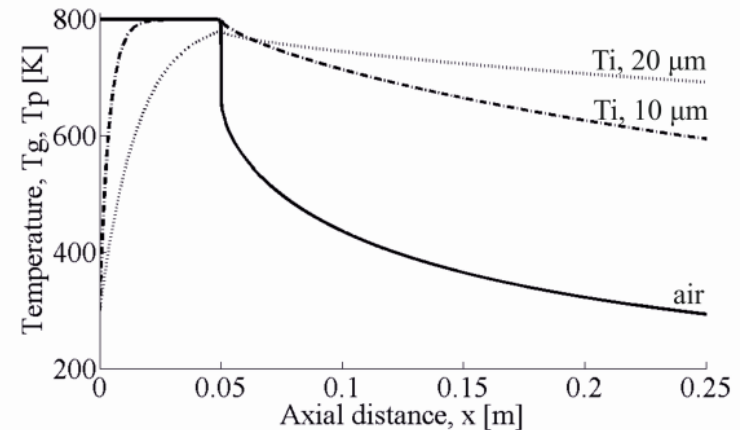


Fig 4. Titanium particles temperature during cold spraying

# Results

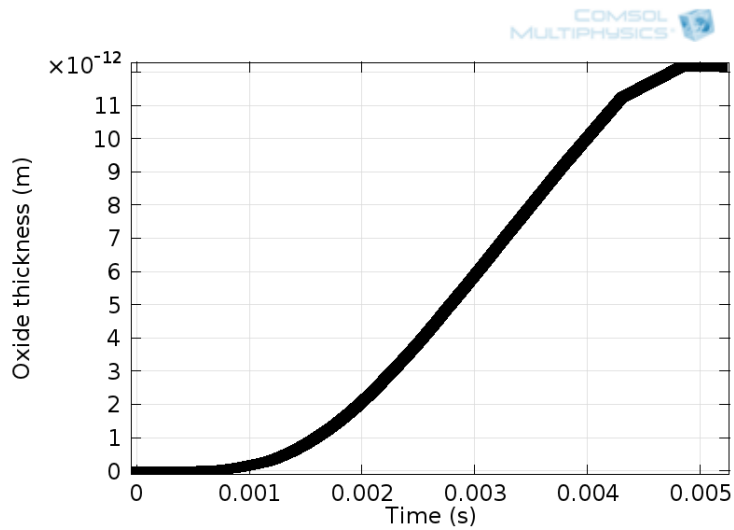


Fig 5. Oxide thickness grow during residence time in nozzle for particle  $10 \mu\text{m}$

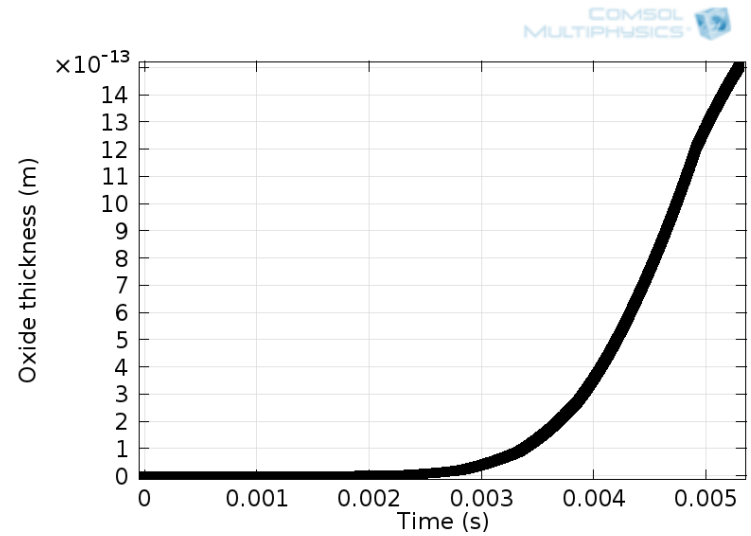


Fig 6. Oxide thickness grow during residence time in nozzle for particle  $20 \mu\text{m}$

# Conclusions

- oxide formation during the residence time in nozzle is negligible
- oxygen dissolution in titanium as well as the possibility of damage to the oxide layer may have an effect on the final oxidation of the sprayed coating
- long contact time between the air stream issuing from the nozzle and forming coating may cause an increase in oxide content



Thank you for your attention

