

COMSOL  
CONFERENCE  
ROTTERDAM2013

# MODELING OF A MAGNETOCALORIC SYSTEM FOR ELECTRIC VEHICLE

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# ICE PROJECT: OBJECTIVES

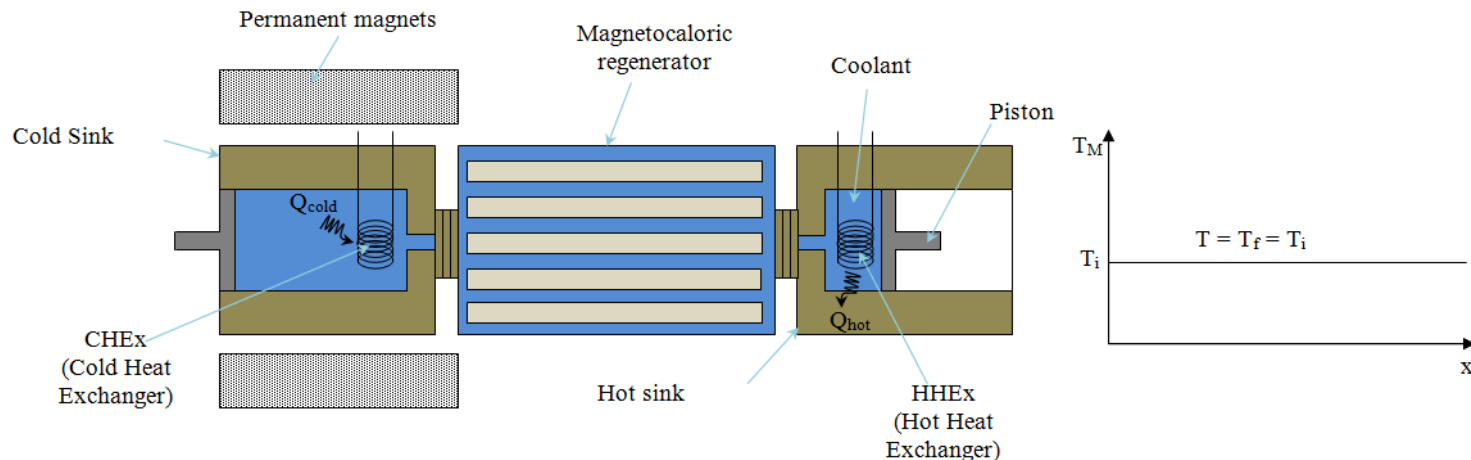
- Development of an efficient air-conditioning and heating system based on Magneto-Caloric heat pump
- New system architecture to fulfill the thermal comfort and energy requirements of a FEV

Heating power: 5 kW  
Cooling power: 3 kW  
Temperature span:  $-7^{\circ}\text{C}$ ,  $+50^{\circ}\text{C}$   
COP  $\geq 3$



# MAGNETOCALORIC HEAT PUMP

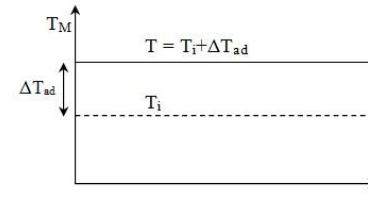
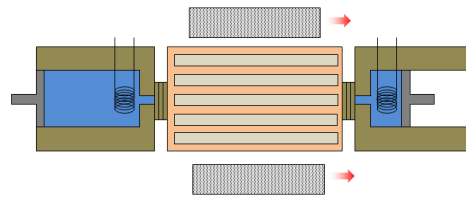
- Based on Magneto-Caloric Effect (MCE)
- MCE: temperature changing of a magneto-caloric material exposed to a changing magnetic field
- Active Magnetic Regenerator (AMR)



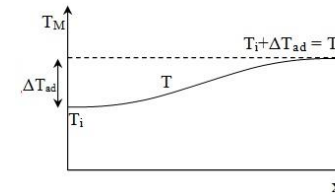
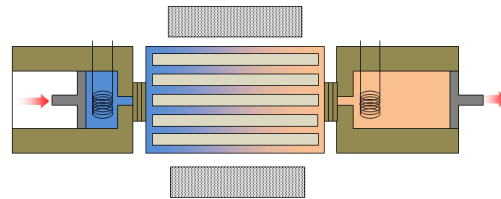
# MAGNETOCALORIC HEAT PUMP

## Active Magnetic Regenerator cycle (AMR cycle)

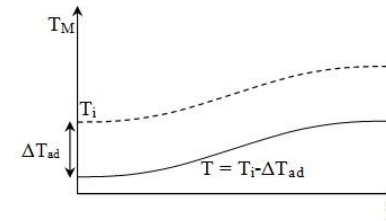
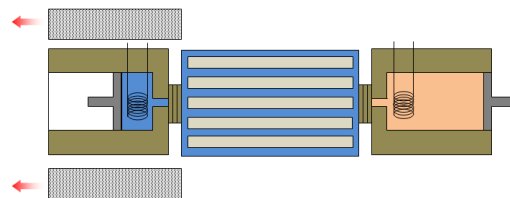
(1)  
Adiabatic magnetization



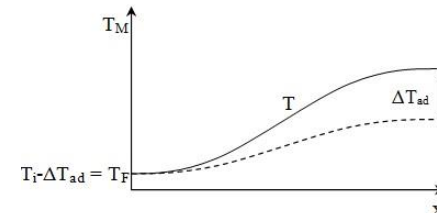
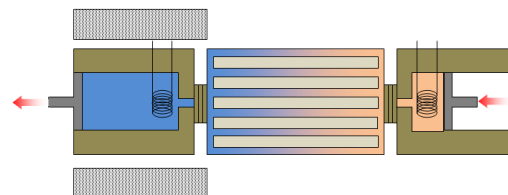
(2)  
Isofield cooling  
(Maximal magnetic field)



(3)  
Adiabatic demagnetization

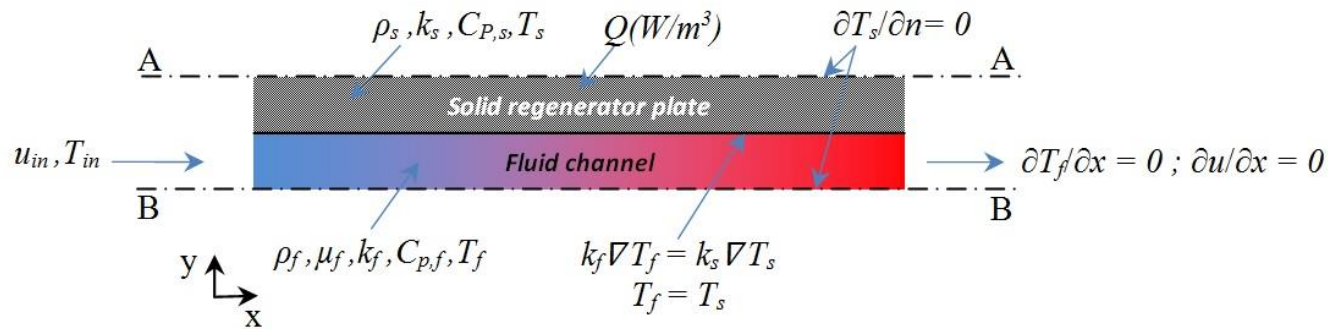


(4)  
Isofield heating  
(Minimal magnetic field)



# MODELING OF MAGNETOCALORIC HEAT PUMP

## Model of fluid flow and heat transfer in Minichannel



Mass conservation equation

$$\nabla \cdot \vec{u} = 0$$

Momentum equation

$$\rho_f (\vec{u} \cdot \nabla) \vec{u} = -\nabla p + \mu_f \nabla^2 \vec{u}$$

Energy equation for fluid domain

$$\rho_f C_{p,f} (\vec{u} \cdot \nabla T_f) = k_f \nabla^2 T_f$$

Energy equation for solid domain

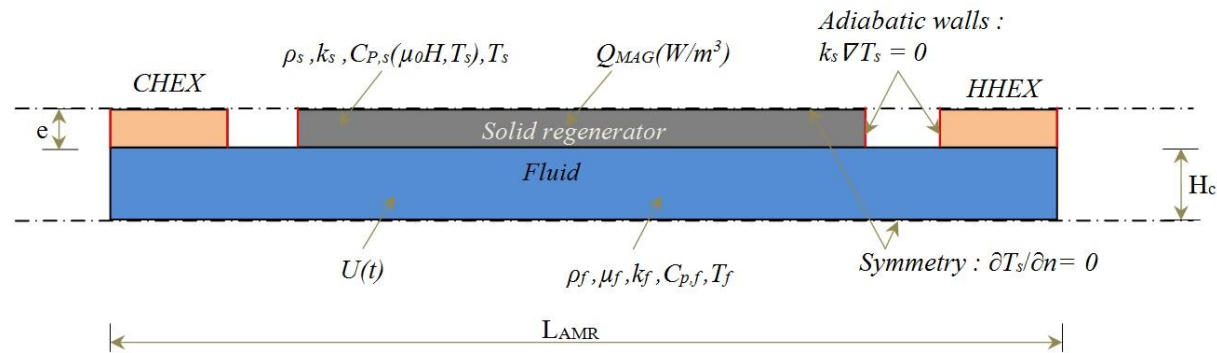
$$k_s \nabla^2 T_s + Q_0 = 0$$

Equation for heat transfer coefficient

$$h = \frac{q_{wall}}{T_{wall} - T_f}$$

# MODELING OF MAGNETOCALORIC HEAT PUMP

## Physical model of AMR cycle



Energy equation for fluid

$$\rho_f C_{p,f} \left( \frac{\partial T_f}{\partial t} + (\vec{u} \cdot \nabla) T_f \right) = \nabla \cdot (k_f \nabla T_f) - \dot{Q}_{TT}$$

Energy equation for solid

$$\rho_s C_{p,s} \frac{\partial T_s}{\partial t} = \nabla \cdot (k_s \nabla T_s) + \dot{Q}_{MAG} + \dot{Q}_{TT}$$

Equation of MCE source term

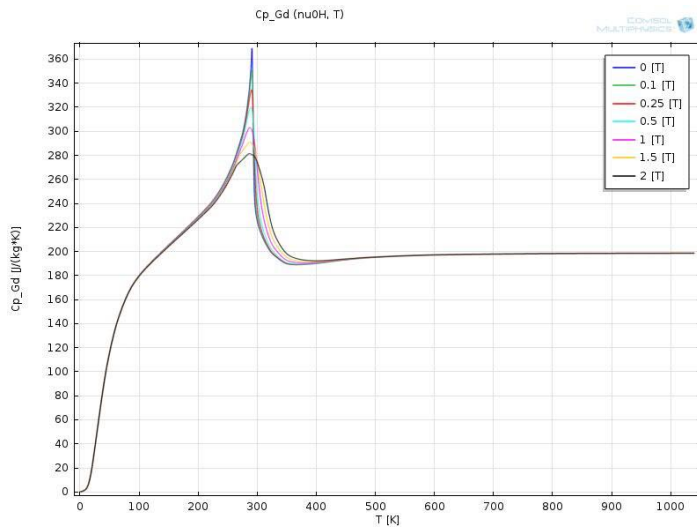
$$\dot{Q}_{MCE} = \rho_s C_{p,s} \left( \frac{\partial T_{ad}}{\partial H} \frac{dH}{dt} + \frac{\partial T_{ad}}{\partial T_s} \frac{dT_s}{dt} \right)$$

Equation of heat transfer between fluid and solid as source term

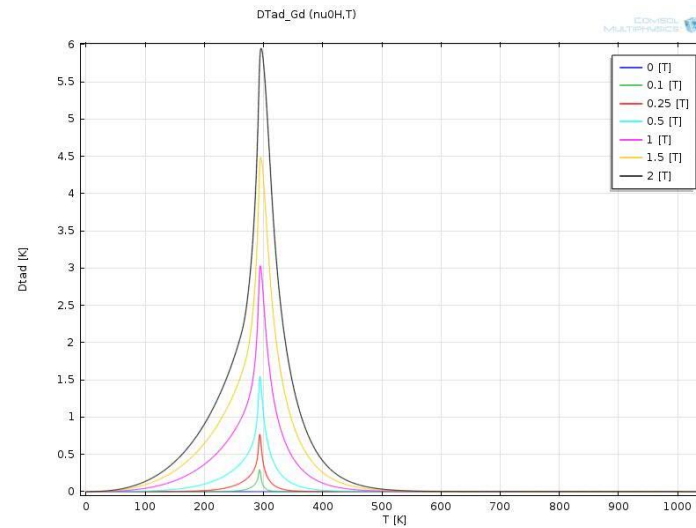
$$\dot{Q}_{TT} = h\beta (T_s - T_f)_{Int:f/s}$$

# MODELING OF MAGNETOCALORIC HEAT PUMP

## ◉ Interpolation of $C_p$ and $\Delta T_{ad}$ of Gadolinium



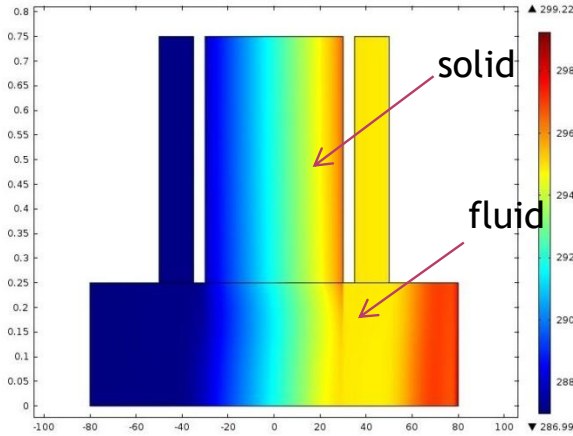
Variation of  $C_p$  with temperature, for  $0 \leq \mu_0 H \leq 2 \text{ T}$



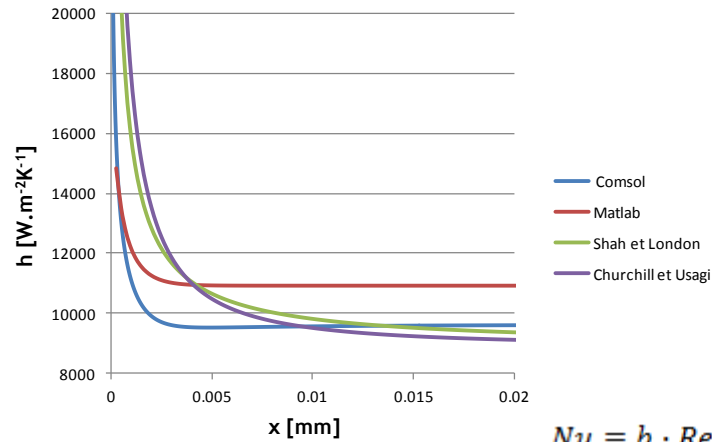
Variation of  $\Delta T_{ad}$  with temperature, for  $0 \leq \mu_0 H \leq 2 \text{ T}$

$$\dot{Q}_{MCE} = \rho_{Gd} C_{p_{Gd}}(T, \mu_0 H(t)) \frac{\Delta T_{ad_{Gd}}(T, \mu_0 H(t+dt)) - \Delta T_{ad_{Gd}}(T, \mu_0 H(t))}{dt}$$

# RESULTS AND CONCLUSION



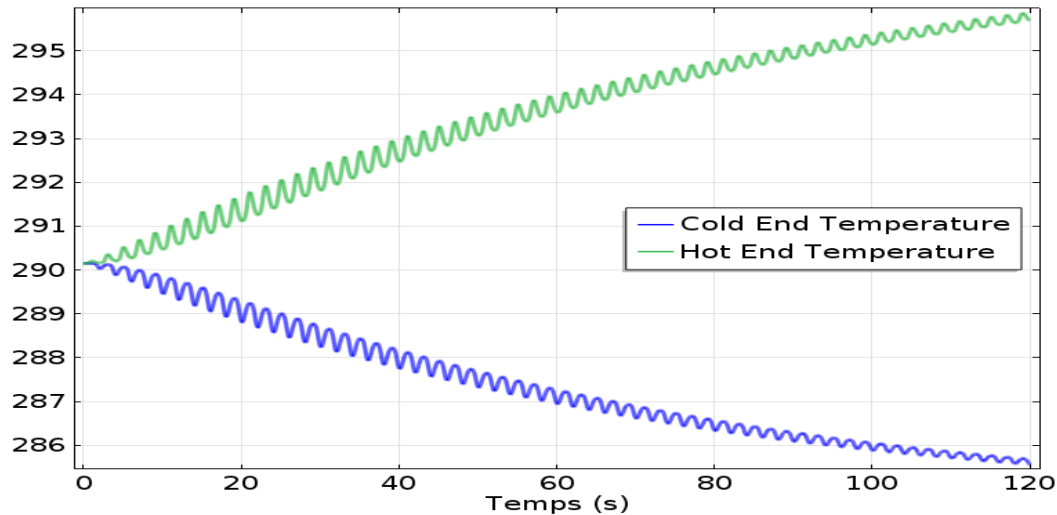
Temperature field



Heat transfer coefficient

$$Nu = b \cdot Re^m \cdot Pr^n$$

$$Nu = \frac{hD}{k_f}$$



Hot end and cold end temperatures of the cycle



# RESULTS AND CONCLUSION

## Contributions

- ◉ A different and accurate approach to calculate the QMCE
- ◉ An accurate determination of heat transfer coefficient

# ENCOUNTERED PROBLEMS

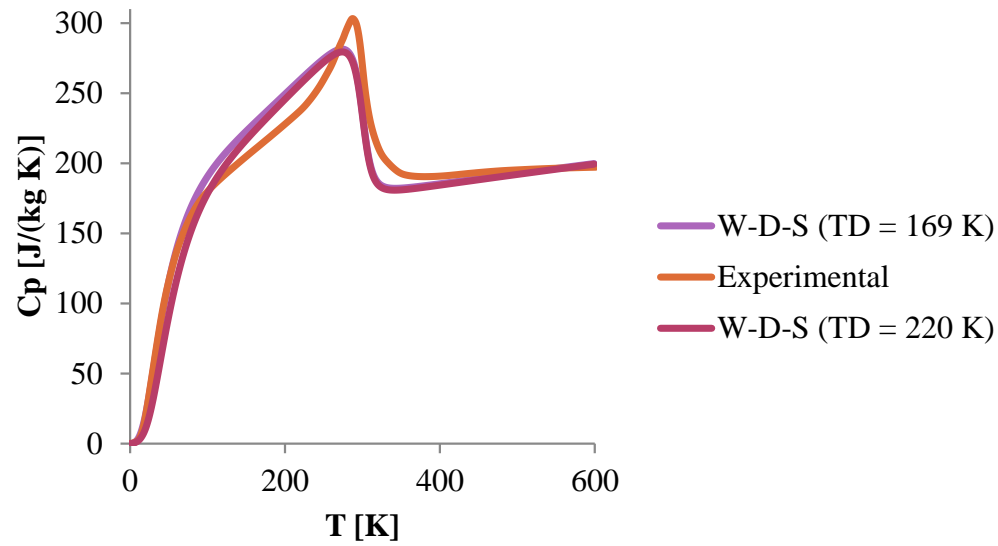
- ◉ Implementation of  $Q_{MCE}$
- ◉ Requirement of high quantity of memory

## FUTURE WORK

- ◉ Analyse the surface rugosity influence on the fluid flow and heat transfer in microchannels.
- ◉ Analyse the influence of the dimensions of the system (plate thickness, channel height) on the heat transfer quantities.

 **THANKYOU!**

$\mu_0 H = 1$  [T]



$\mu_0 H = 0$  [T]

