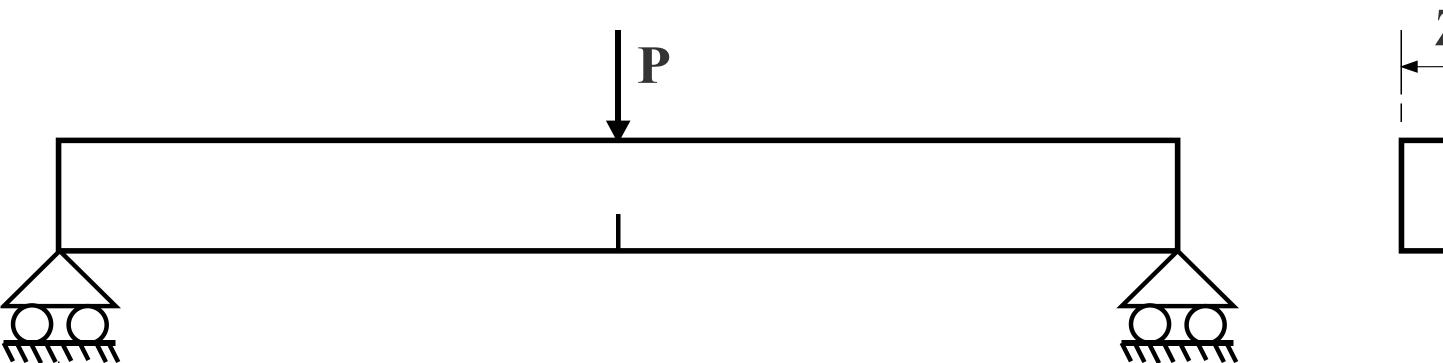
# Finite Element Evaluation of J-integral in 3D for Nuclear Grade Graphite using COMSOL Multiphysics A. Bhushan<sup>1</sup>, Dr. S. K. Panda<sup>1</sup>, S. K. Singh<sup>1</sup>, Dr. D. Khan<sup>1</sup> 1. Indian Institute of Technology (BHU), Varanasi - 221005, Uttar Pradesh, India

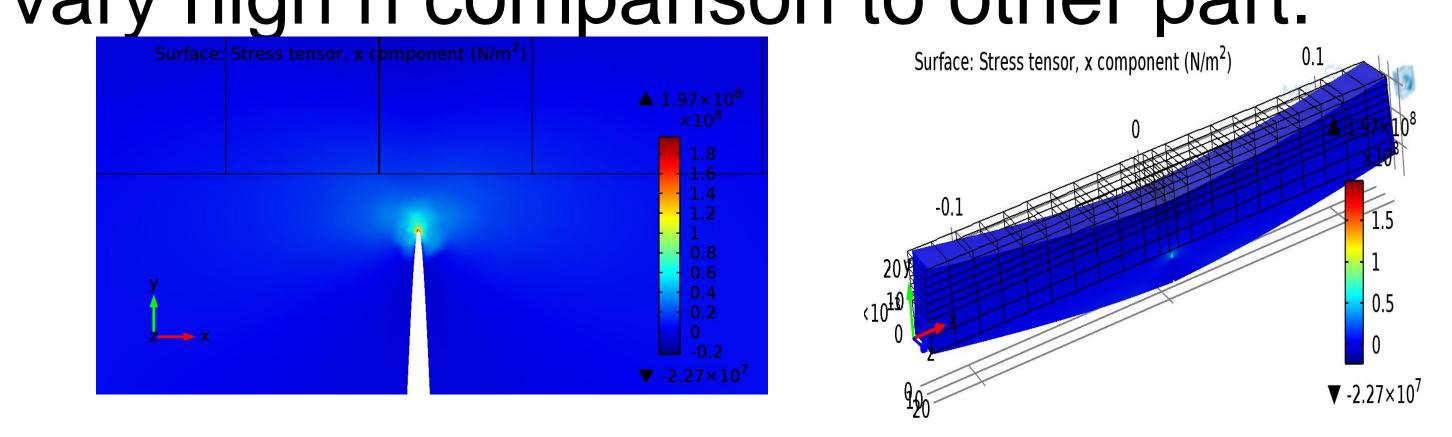
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**Introduction**: Effect of bi-modularity on Jintegral in cracked three point bend specimen has been presented here.



-250mm-

## **Results**: Stress around the crack-tip is vary high n comparison to other part.





### Figure 1 Cracked three Point Bend

**Computational Methods**: The problem is solved by stress dependent elasticity considering different Young's modulus of elasticity in tension and compression shown in table 1. J-integral for 3D geometry has been evaluated following equation in elastic bi-modular region given by Dodds, in1987 [1]  $J(s) = \oint \left( W^{e} n_{1} + W^{p} n_{1} - u_{i,1} T \right) d\tau + \oint \left( \left( \sigma_{ij} \varepsilon_{ij,1}^{p} \right) - \left( \left( \sigma_{i,3} u_{i,1} \right)_{3} \right) - W_{3}^{p} \right) dA$ In elastic bi-modular region plastic stress

**Figure 3**. Normal stress distribution in x- direction (a) around the Crack tip (b) for whole geometry

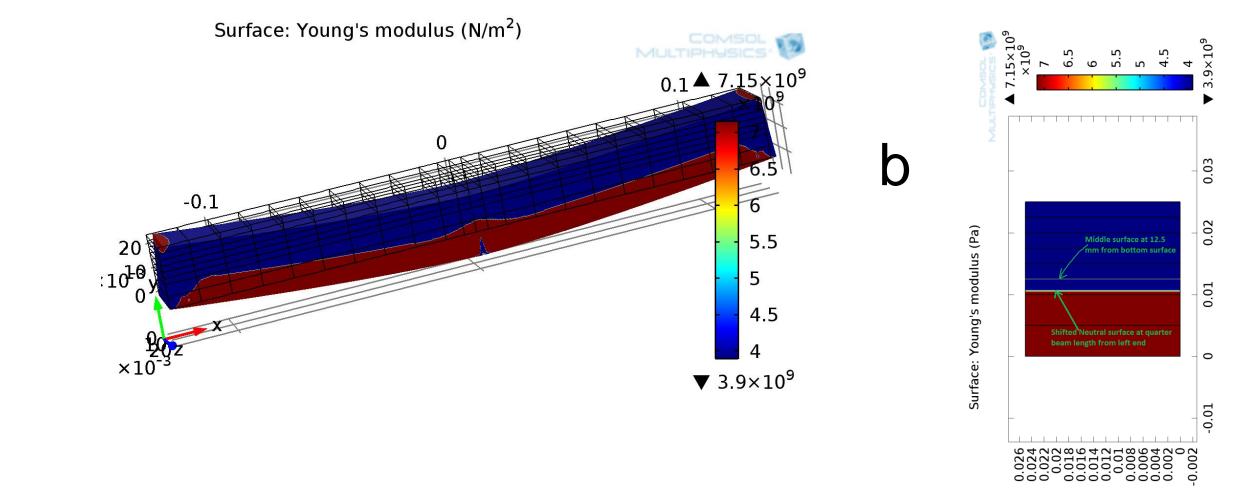
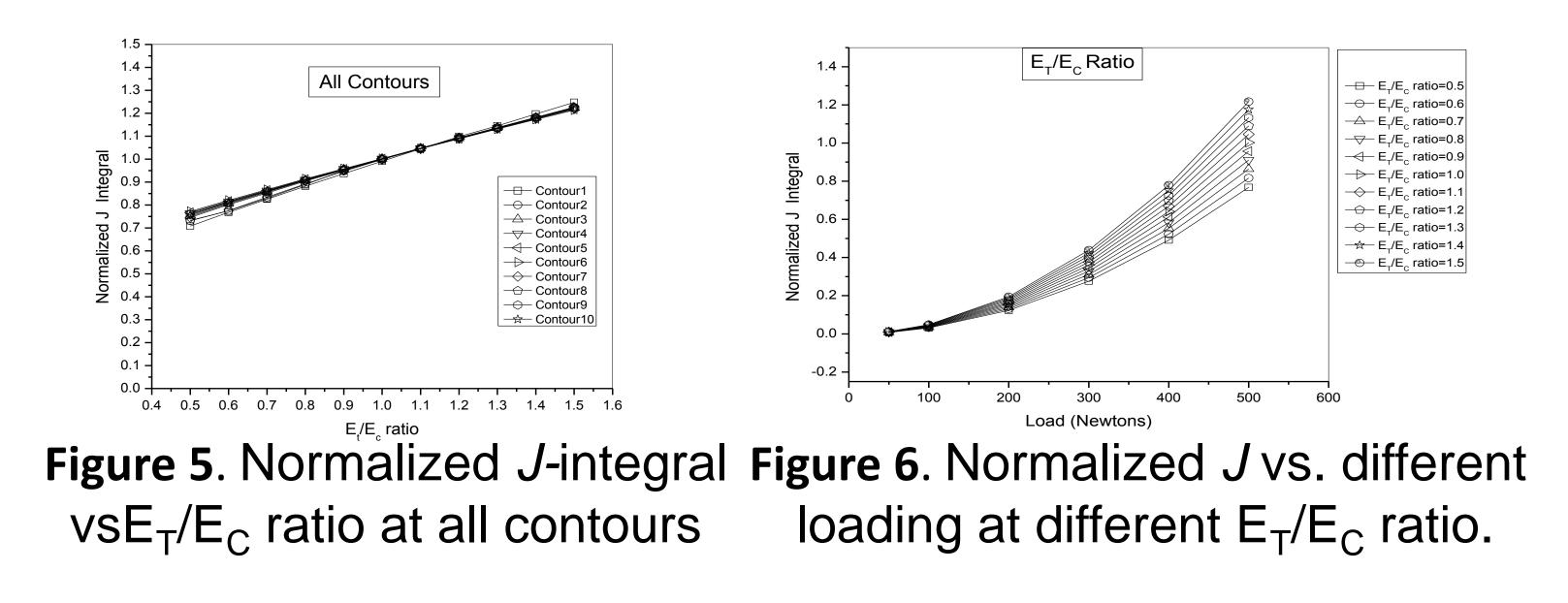
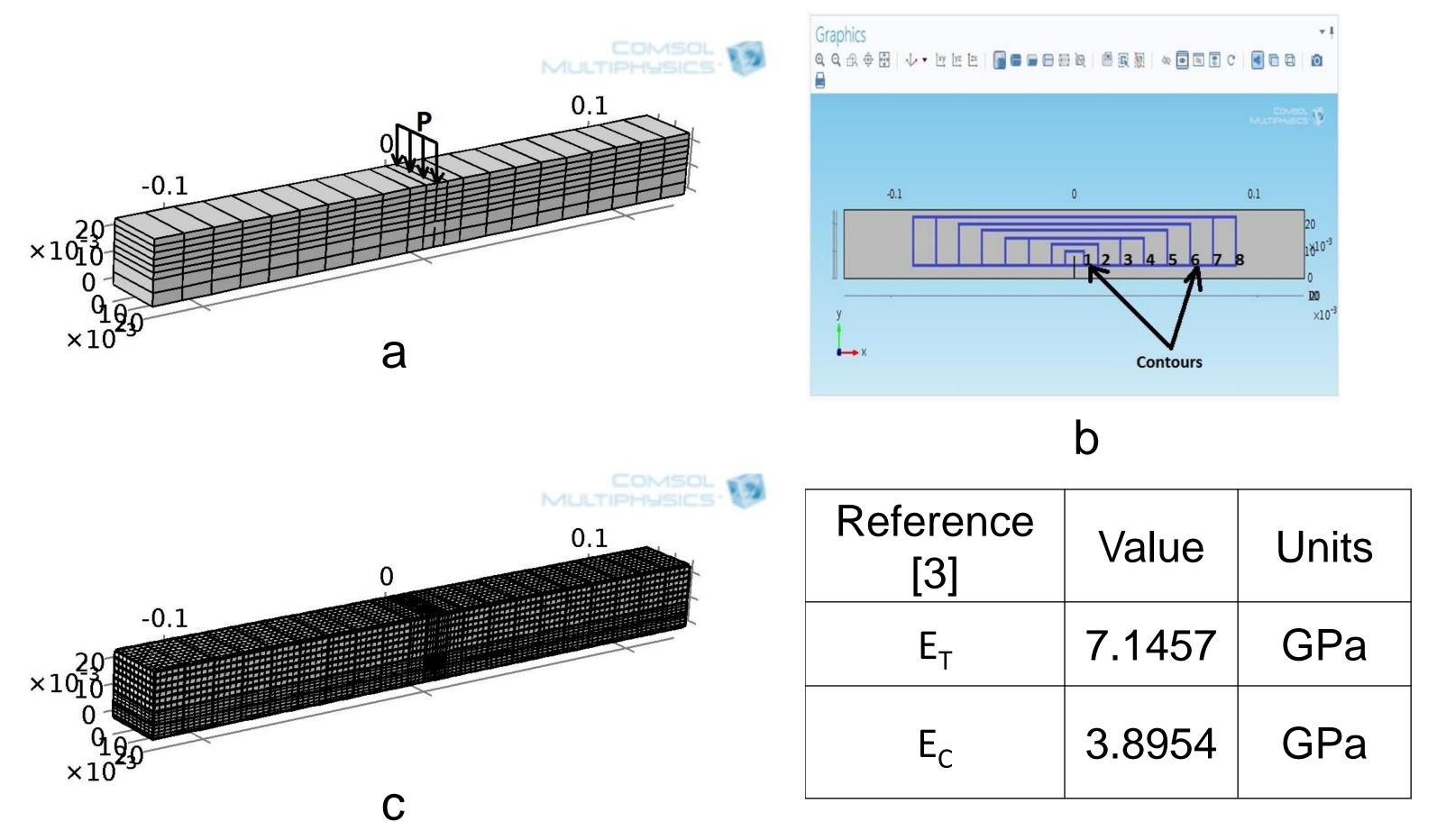


Figure 4. Young's Modulus plot (a) for the three point end specimen and (b) for x-section at quarter of the beam length at which neutral surface is represented



vanishes strain expression terms and reduced to

$$J(s) = \oint_{\Gamma} \left( W^e n_1 - u_{i,1} T \right) d\tau - \oint_A (\sigma_{i3} u_{i,1})_{,3} dA$$



**Conclusions**: The degree of path independency is going to be slightly inferior in nature as the  $E_T/E_C$  ratio deviates from the value of unity. The  $E_T/E_C$  ratio influences the value of the *J*-integral significantly.

For very low load level, it is apparent that all the *J*-values merge into a single parabolic curve for different  $E_T/E_C$ ratio, however with increase in load level, strong divergence in the J-value occur for different  $E_T/E_C$  ratio. Therefore, it is concluded that the effect of the bimodularity on the computation of *J*-integral values cannot

**Table 1**. Title of the table

**Figure 2**. (a)Comsol complex model for defining contour to evaluate J-integral, (b) Different contours, (c) Hexahedron Mesh representation

#### be neglected.

### **References**:

- Dodds, R.H., Jr., "Finite Element Evaluation Of J 1. Parameters In 3D<sup>"</sup>, International Journal of Fracture, vol. 33, pp. R7-R15, (1987).
- Rice, J.R., "A path independent integral and the 2. approximate analysis of strain concentration by notches and cracks." Trans. ASME, J. Appl. Mech., vol. 35, pp. 379-386, (1968).
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