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Phase Transformation and Deformation Model for Quenching Simulations

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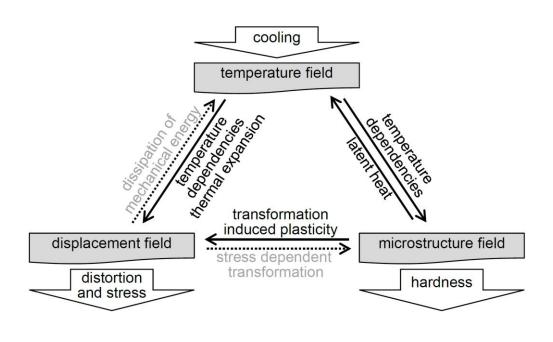
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Introduction



<u>Quenching</u> is the <u>rapid cooling</u> of a workpiece <u>to obtain certain material</u> <u>properties</u>. For instance, quenching can reduce the crystal grain size of metallic materials and increasing their hardness.



Quenching of the <u>advanced</u> <u>steel grades</u> is a challenging process since the <u>residual</u> <u>stress and deformation are</u> <u>pronounced</u> and the quality requirements of the customers are tighter.

A comprehensive <u>modelling</u> of the complex phenomena to estimate the residual stress and deformation is essential for developing an optimal process control.

Computational Methods: Temperature and Displacement Fields



Heat transfer in solids physics and solid mechanics physics are used.

All material properties depends on the temperature and microstructure. Linear mixture rules are used for $E, v, \sigma_{y0}, C_p, k$ and harmonic mixture rule is used for ρ .

$$E = f_{a}E_{a}(T) + f_{b}E_{b}(T) + f_{m}E_{m}(T)$$

$$\nu = f_{a}\nu_{a}(T) + f_{b}\nu_{b}(T) + f_{m}\nu_{m}(T)$$

$$\sigma_{y0} = f_{a}\sigma_{ay0}(T) + f_{b}\sigma_{by0}(T) + f_{m}\sigma_{my0}(T)$$

$$C_{p} = f_{a}C_{pa}(T) + f_{b}C_{pb}(T) + f_{m}C_{pm}(T)$$

$$k = f_{a}k_{a}(T) + f_{b}k_{b}(T) + f_{m}k_{m}(T)$$

$$\rho = \frac{1}{\frac{f_{a}}{\rho_{a}(T)} + \frac{f_{b}}{\rho_{b}(T)} + \frac{f_{m}}{\rho_{m}(T)}}$$

Latent heat of transformation as heat source $Q = L_{ab}\dot{f}_b + L_{am}\dot{f}_m$

Dilatation due to Temperature und microstructure change $dL = \sqrt[3]{\frac{\rho_a(T_{ref})}{\rho}} - 1$

Inelastic strains upon Creep and TRIP $\dot{ec}_{ij} = (A_{tr} + A_{cr}) \cdot n_{ij}^S$ $\dot{ec}_{eff} = \sqrt{\frac{2}{3}} \sum \dot{ec}_{ij}^2$ $A_{tr} = \{K_b^{GJ} \cdot \dot{f}_b \cdot \ln(f_b) + K_m^{GJ} \cdot \dot{f}_m \cdot \ln(f_m)\} \cdot \sigma_{eff}$

$$A_{\rm cr} = \left(\frac{\sigma_{\rm eff}}{\sigma_{\rm ref}(T)}\right)^{n_{\rm cr}(T)}$$

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Computational Methods: Microstructure Field



Two types of transformations are modelled:

(1) austenite to bainite transformation, which is diffusion controlled, needs an incubation time before the transformation starts. This transformation obeys Scheil's rule and JMAK (Johnson-Mehl-Avrami-Kolmogorow) equations:

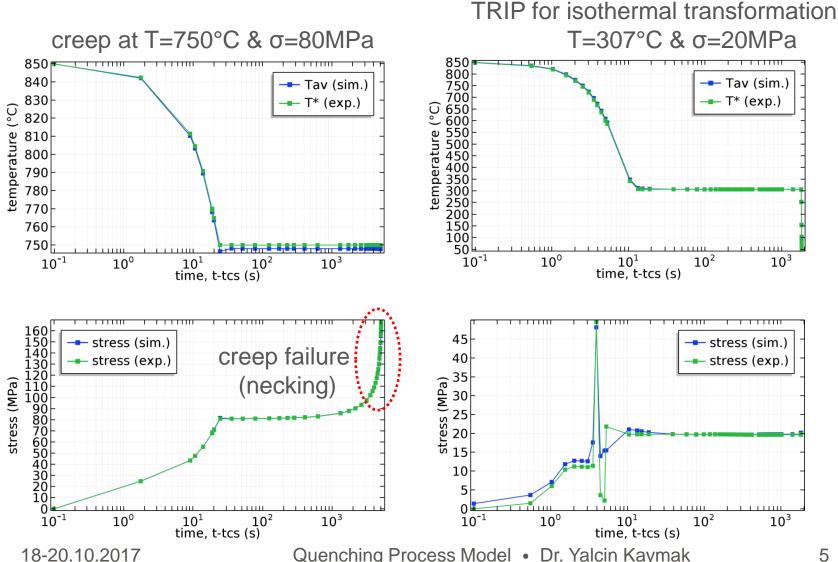
$$\dot{ss} = \frac{1}{Bs(T)}$$
 $\dot{f}_b = K \cdot n \cdot t^{n-1} \cdot \exp(-K \cdot t^n)$

(2) austenite to martensite transformation, which is diffusionless, is controlled only by temperature. This transformation is expressed by KM (Koistinen-Marburger) equation:

$$f_m = 1 - \exp(-0.011(M_s - T))$$

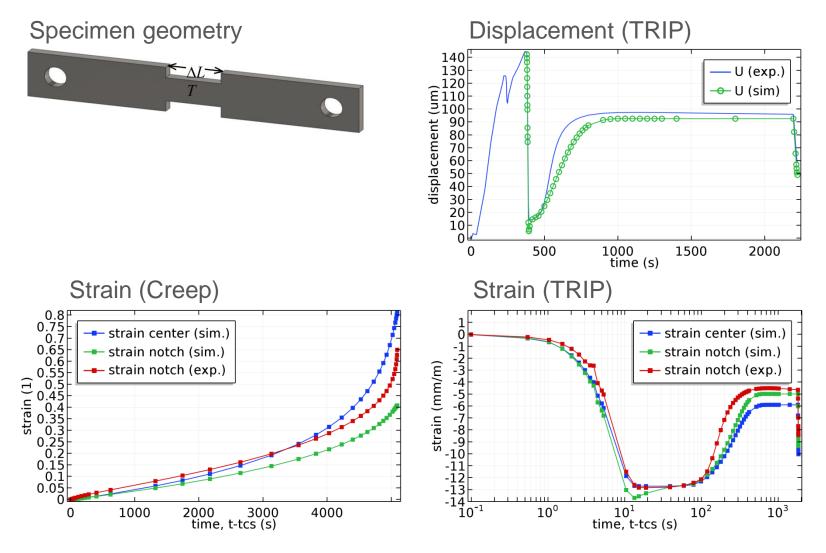
Results: Creep vs. TRIP deformation **Temperature and Mechanical Loading**





Results: Creep vs. TRIP deformation Deformation Response





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Results: Creep vs. TRIP deformation



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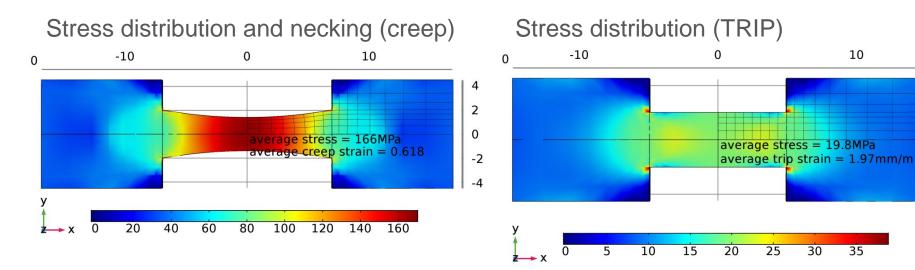
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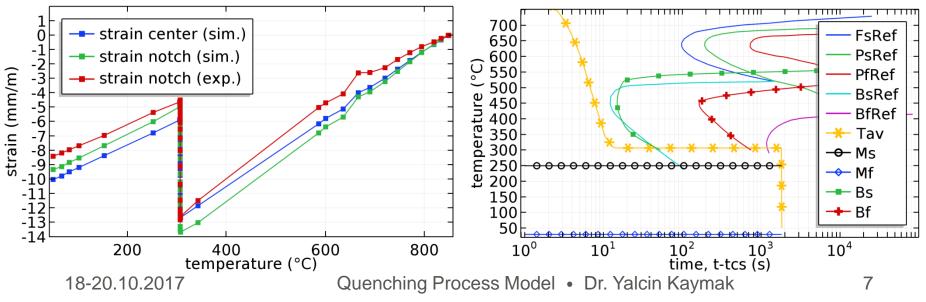
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Typical dilatometry curve for isothermal transformation and TTT diagram



Conclusions



- A complex <u>model for</u> the simulation of the <u>quenching process</u> has been introduced, which can be used in the heat treatment simulation of the advanced steel grades to <u>compute the residual</u> <u>stress and deformation</u> as well as the <u>microstructure</u>.
- The introduced model consists of a series of strongly <u>coupled</u> <u>physics</u>. The <u>temperature</u>, <u>microstructure</u> and <u>displacement fields</u> are solved by considering dilatation and nonlinear phenomena (plasticity, trip, creep, and large deformations).
- The constitutive <u>model</u> parameters as well as the isothermal and martensitic transformation kinetic parameters are <u>validated and</u> <u>calibrated by several dilatometry tests</u>.

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