

The Origin of Mass-change Sensitivity in PEMC sensors: *Experimental and FEM Vibrational Analysis*

Blake Johnson and Raj Mutharasan

Department of Chemical and Biological Engineering

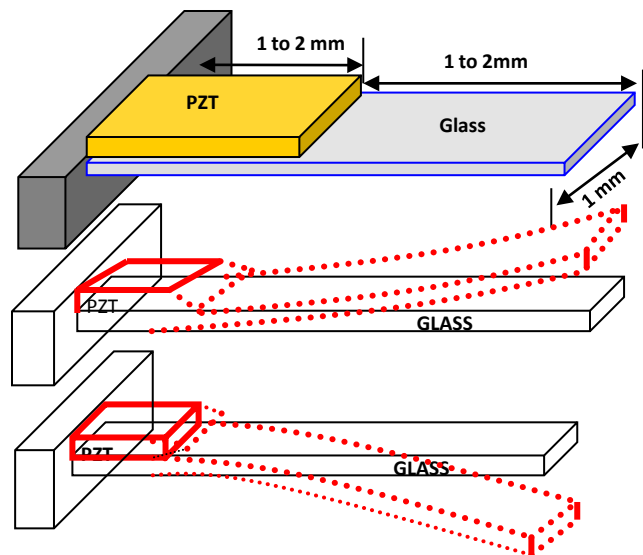
Drexel University

Philadelphia, PA 19104



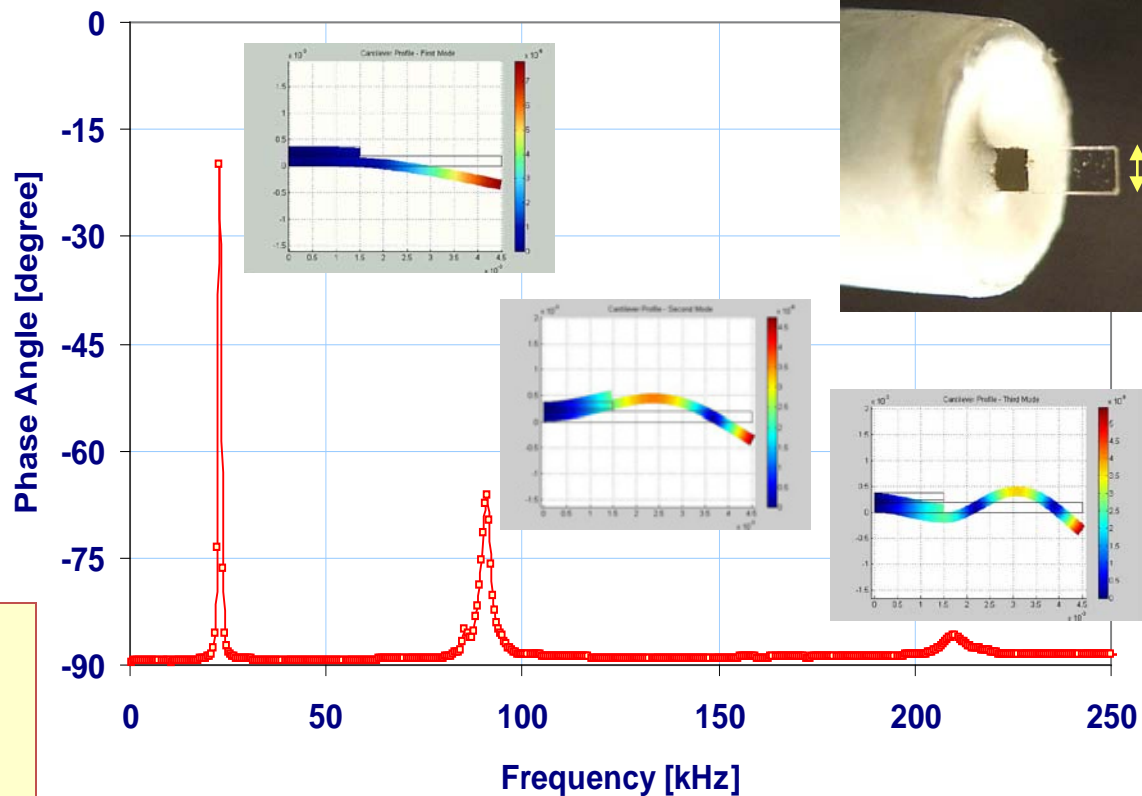


Piezoelectric-Excited Millimeter-sized Cantilever (PEMC) Sensors



Sensing Principle

- Resonant frequency depends on cantilever's mass.
- Surface is immobilized with a recognition molecule (eg. Antibody; ssDNA).
- When target attaches to the cantilever, mass changes, and resonant frequency changes.

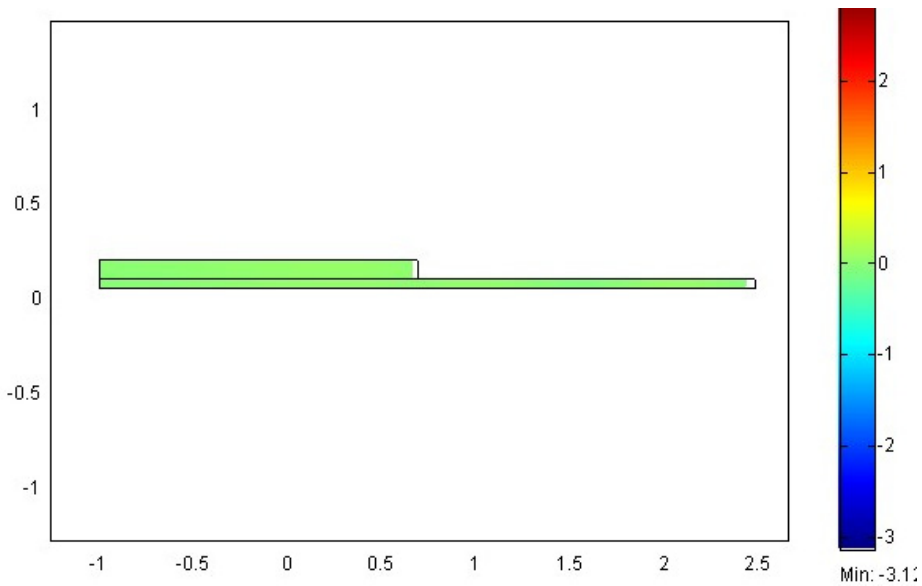
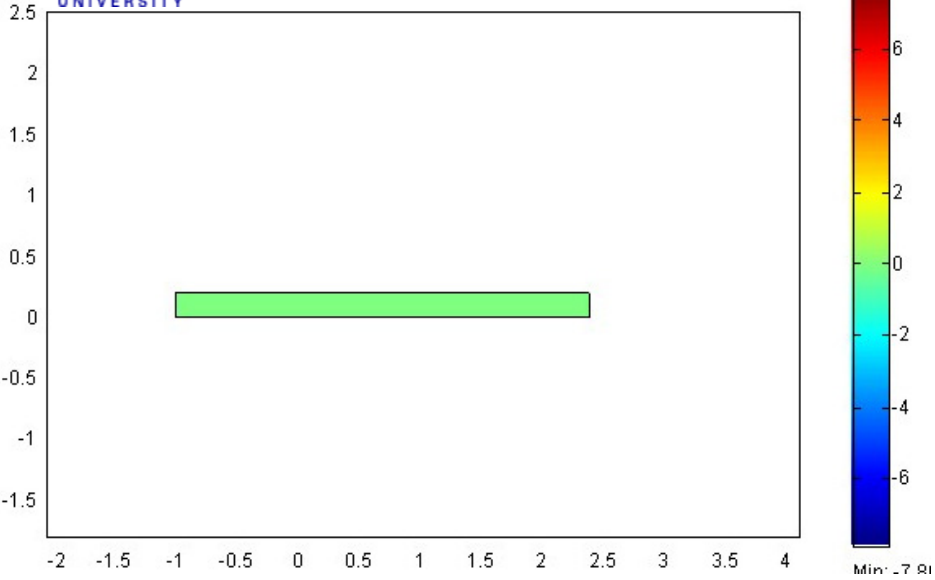


Typical spectrum measured experimentally, we want to predict this behavior.



Oscillation characteristics of PEMC Sensors

PZT only – fixed at one end

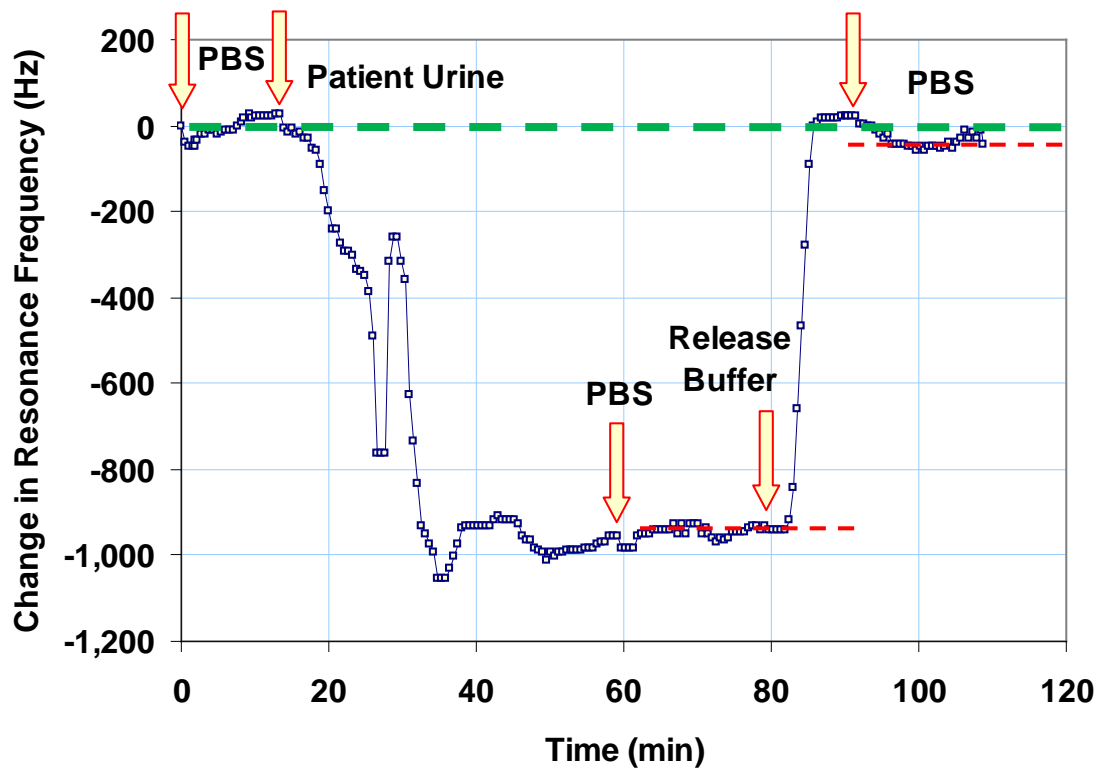


PZT-bonded to **Low** modulus base

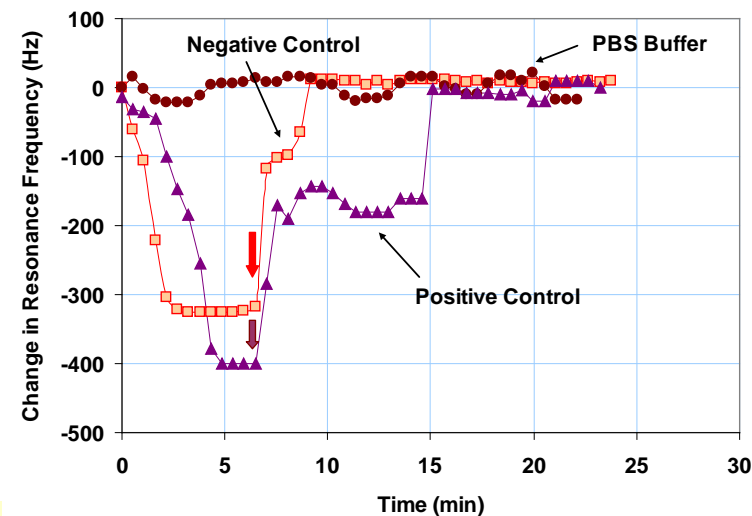
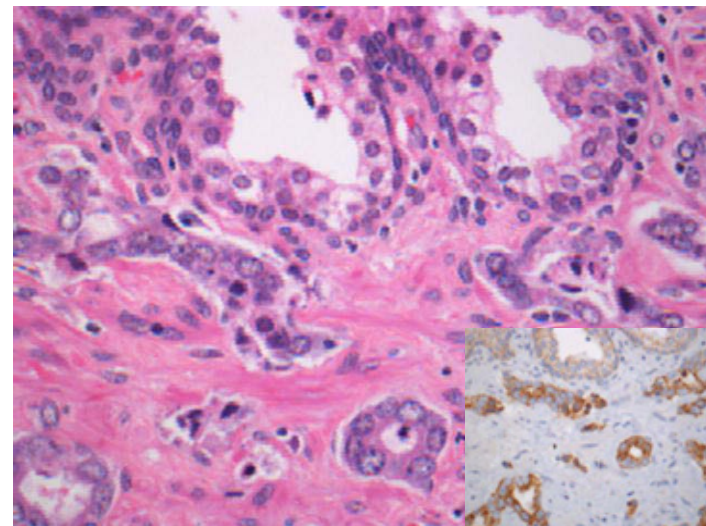
PZT-bonded to **High** modulus base



AMACR in patient urine – Patient 3



Prostate cancer biomarker:
 α -methylacyl-CoA racemase (AMACR)



Case #	Age	Gleason Score	Post Biopsy Stage	PSA Value	PEMCA Response	PEMCA Control Urine
Case 1	61	7	pT2c	11.6 ng/mL	-4,314±35 Hz	10±21 Hz
Case 2	83	6	pT2a	12.6 ng/mL	-269±17 Hz	10±6 Hz
Case 3	64	8	pT2c	78.4 ng/mL	-977±64 Hz	-63±14 Hz
Case 4	59	7	pT2b	4.6 ng/mL	-600±31 Hz	-35±24 Hz
Case 5	65	7	PT2c	2.0 ng/mL	-801±81 Hz	-20±15 Hz



Notable detection applications and Motivation

Detection Application	Sensitivity
<i>Bacillus anthracis</i> (Anthrax) spores in air	5 spores/L
<i>E. coli</i> O157:H7 in food media	1 cell/mL
Prostate cancer biomarker (AMACR) in urine	2 fg/mL

Motivation:

- Vibration characteristics of PEMC sensors are complex and remain unexplored.
- Understand the origin of mass-change sensitivity in PEMC sensors using modeling.
- Use simulation as tool for creation of other sensitive structures.
- Structure the model to simulate the quantities we measure experimentally.

Campbell, C; Mutharasan, R. **2007**. *Biosensors and Bioelectronics*, 23: 1039 – 1045

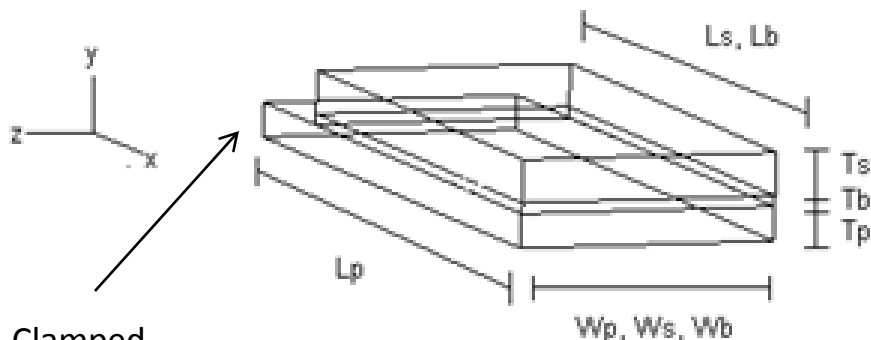
Campbell, C; Mutharasan, R. **2007**. *Analytical Chemistry*, 79 (3): 1145 – 1152

Campbell, C; Mutharasan, R. **2007**. *Environmental Science and Technology*, 41 (5): 1668 – 1674

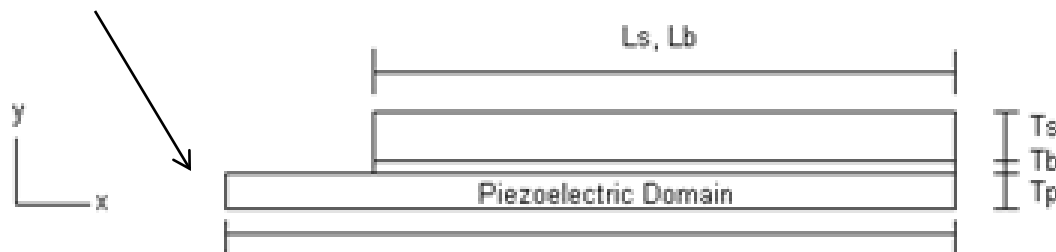
Maraldo, D; Garcia, F; Mutharasan, R. **2007**. *Analytical Chemistry*, 79 (20): 7683 - 7690



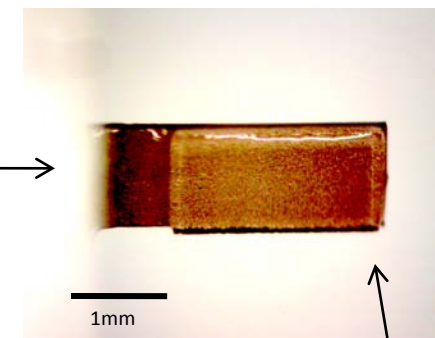
Schematic of PEMC sensor and Experimentally Fabricated Sensor



Clamped edge



Clamped edge



Free edge

Cantilever Dimensions:

- Length (L) ~ 2.5 mm
- Width (W) ~ 1 mm
- Thickness (T) ~ 200 μm

Excitation and Measurement Principle:

- Actuation via harmonic E-field along polarization axis of PZT.
- Inverse piezoelectric effect generates expansion/contraction of the PZT material.
- The resonant frequencies are measurable by the electrical impedance of the piezoelectric domain.



Use of *COMSOL Multiphysics*

COMSOL Modules Used:

- *Structural Mechanics Module*
- *Piezoelectric effects*
- *Piezo Plane Stress*
 - *Damped Eigenfrequency Analysis*
 - *Frequency Response Analysis*
- *Simulations in vacuum*

*Piezoelectric Material Constitutive Relations
(anisotropic)*

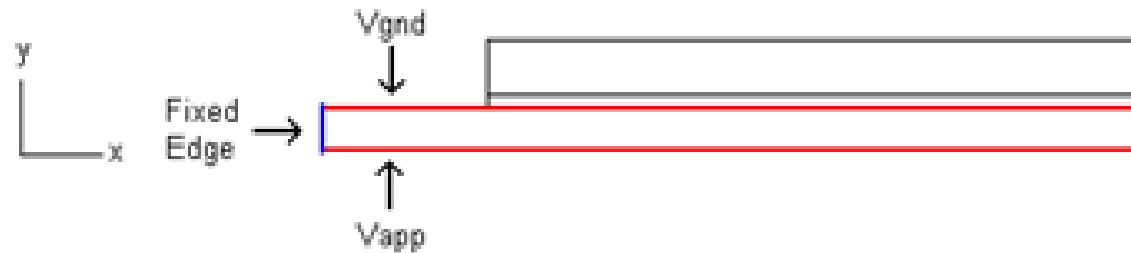
$$\sigma = c\varepsilon - e^T E$$

Electromechanical coupling

$$D = e\varepsilon + \epsilon E$$

Boundary Conditions

- Material polarized in y-direction.
- E-field applied in the y-direction.



Voltage applied = $0.1 \sin(\omega t)$



Frequency Response Analysis

Scalar potential equation:

$$-\nabla (\epsilon_0 \epsilon_r \nabla V) = \rho_v$$

Quasi-static electric currents equation:

$$-\nabla ((\sigma_B + j\omega \epsilon_0 \epsilon_r) \nabla V) = \rho_v$$

Additional expressions employed:

- excitation frequency: $freq_smpz3d$
- electrical impedance: $V/abs(I)$
- phase angle: $\tan^{-1} [Im(I)/Re(I)]$

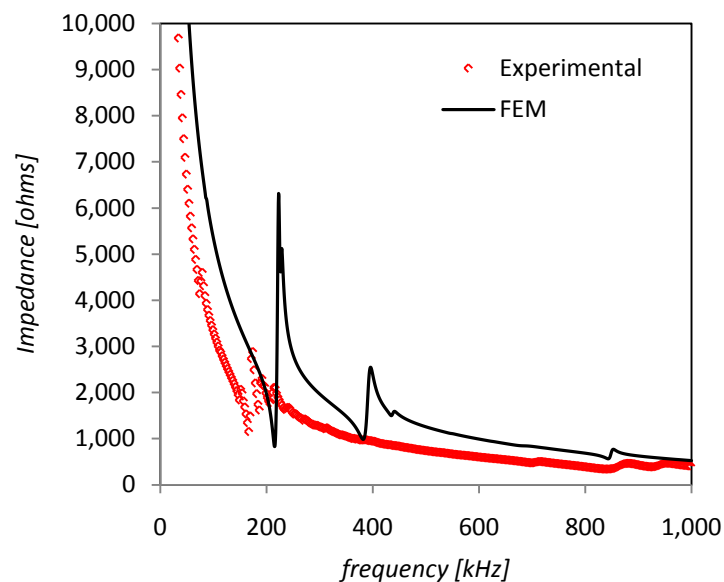
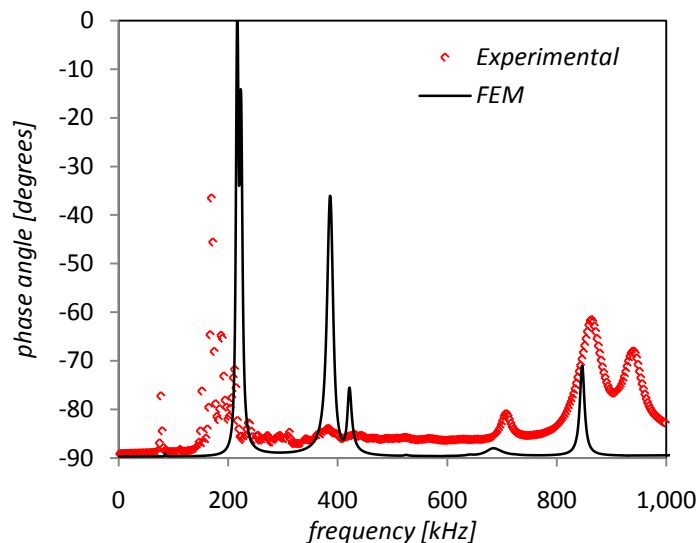
Loss factor damping:

$$G^* = G' + jG'' = (1 + j\eta)G'$$

$$\text{Loss Factor} = \eta = \frac{G''}{G'}$$

G^* , G' , and G'' are stress relaxation function of viscoelastic material, storage modulus, and loss modulus, respectively.

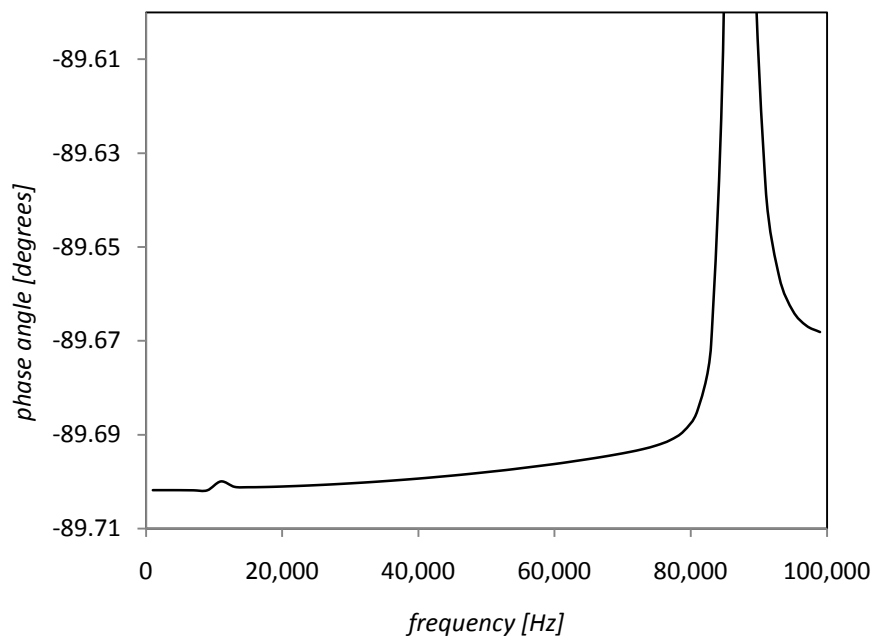
(Simulation time ~ 30 min)





Fundamental Mode Range (0 – 100 kHz):

FEM frequency response analysis



* Contains modes of vibrations sensitive to mass-changes.

* 2nd mode (~80 kHz) used most frequently for detection due to high Q- factor.

* Only 2 resonances in the range of 0 – 100 kHz are electrically measurable using impedance.

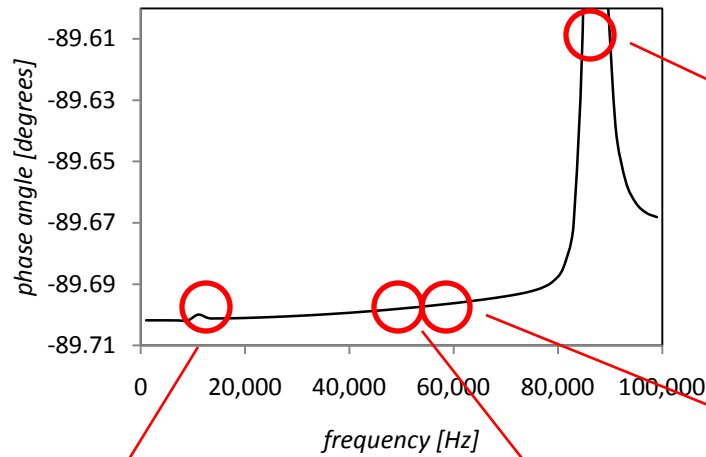


Damped Eigenfrequency Analysis

$$M\ddot{U} + KU = F$$

$$\omega^2 = M^{-1}K$$

$$f_n = k_n \sqrt{\frac{K}{M_e}}$$

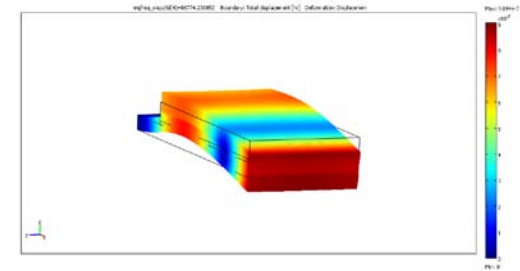


Electrically Observable

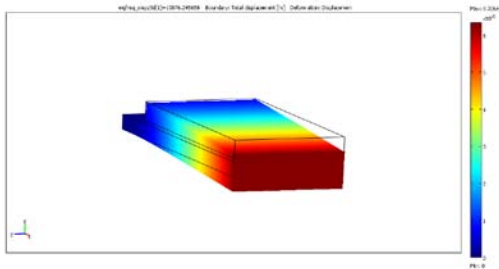
Not electrically observable

Electrically Observable

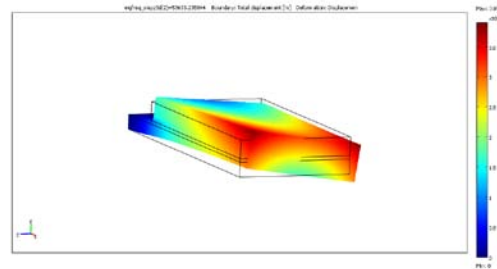
(Simulation time ~ 1 min)



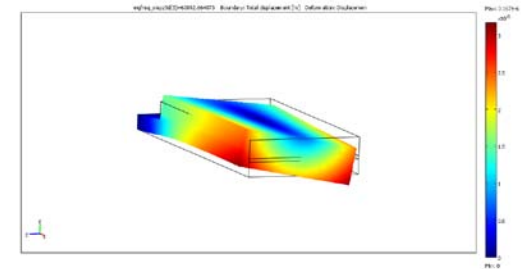
2nd bending mode (86.8 kHz)



Fundamental bending mode (10.0 kHz)



Fundamental torsional mode (53.6 kHz)



2nd torsional mode (60.0 kHz)



Summary

- Used *COMSOL Multiphysics* to simulate the frequency response of the PEMC sensor by impedance characterization.
- Simulation qualitatively predicts the experimentally measured frequency response.
- Assessed the lower order modes of vibration that have been used experimentally for detection using *COMSOL's* eigenfrequency analysis.
- PEMC sensor is sensitive in the bending mode.
- Torsional modes of vibration do not give rise to electrically observable resonances using impedance characterization.



Recommendations

- Recommendations to *COMSOL Multiphysics* developers
 - *Modeling of nonlinear stress-strain material effects.*
 - *Modeling of nonlinear piezoelectric effects.*
 - *Addition of more realistic damping models.*

- Acknowledgements
 - *Advisor: Dr. Raj Mutharasan*
 - *This work was made possible by National Science Foundation Grant CBET-0828987.*