

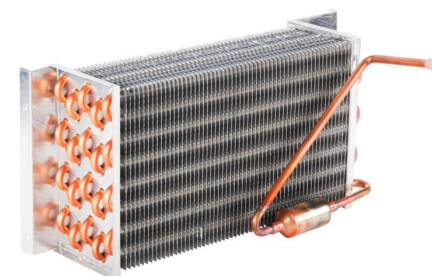
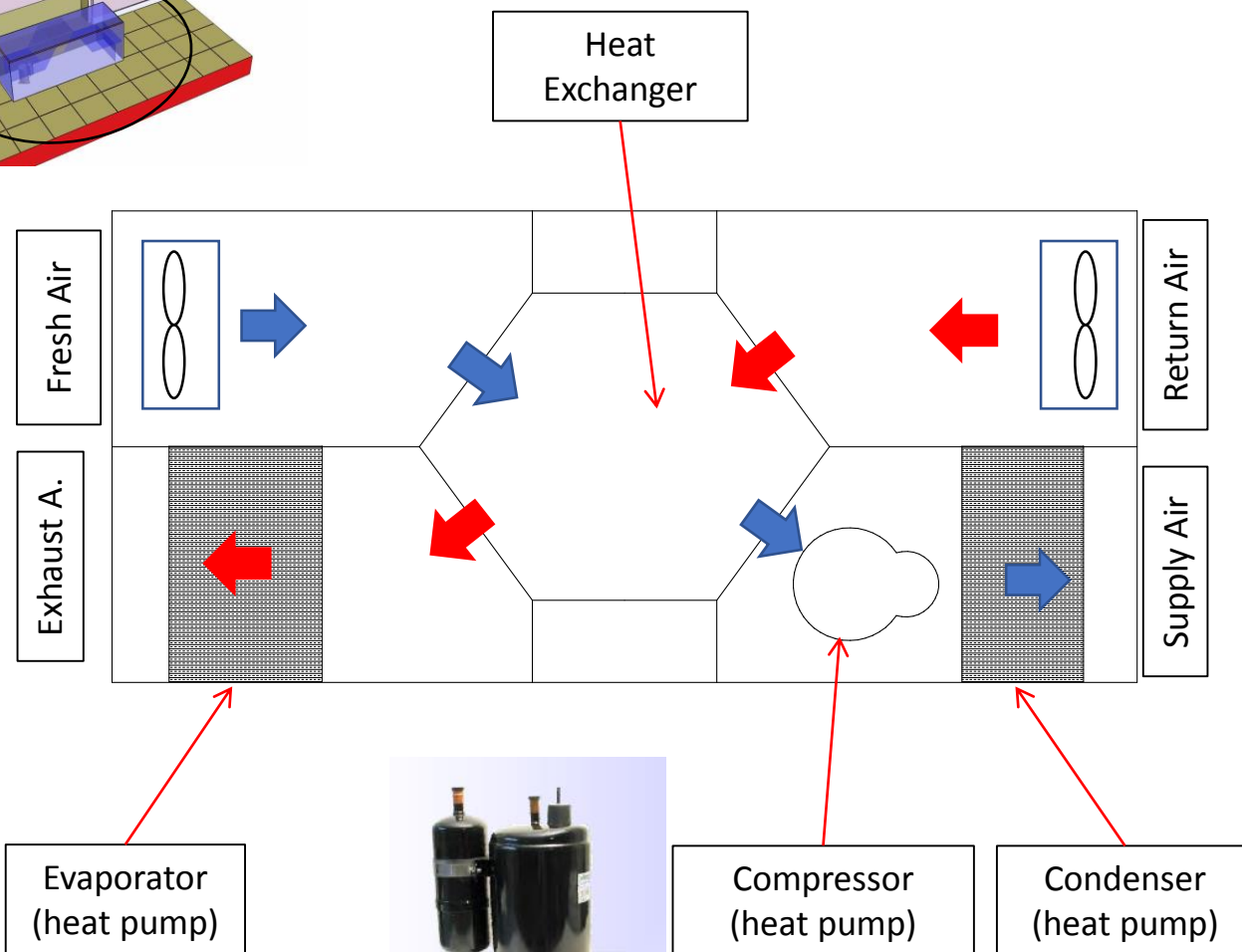
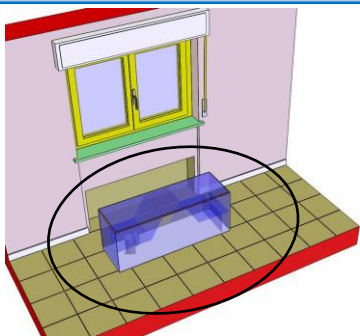
# Flow Optimization of a MVHR combined with an Exhaust air Heat Pump by means of CFD Simulation

Fabian Ochs<sup>1</sup>, Marco Romani<sup>2</sup>, Michele Bianchi Janetti<sup>1</sup>

<sup>1</sup>University of Innsbruck

<sup>2</sup>Cetra Air Handling Units, Galletti Group, Altedo, Italy

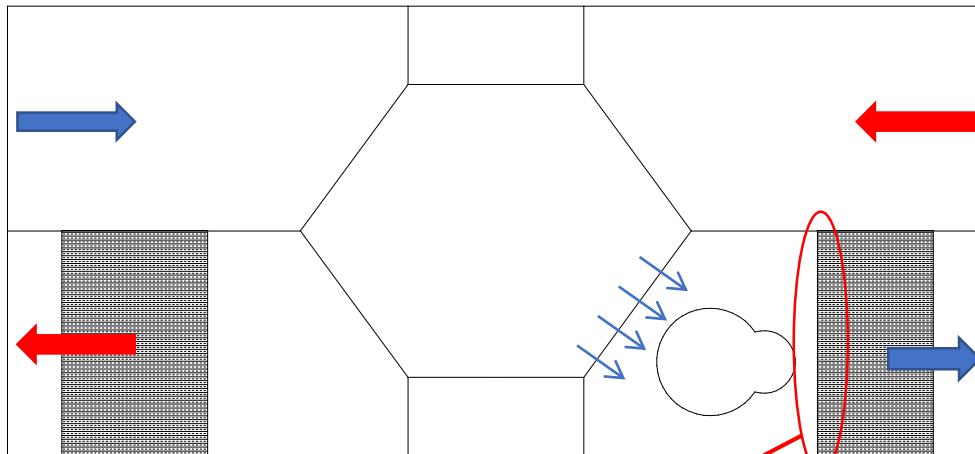
# MVHR (Mechanical Ventilation Heat Recovery) + Heat Pump



# Aims

1 – CFD Model Implementation

2 – Flow optimization



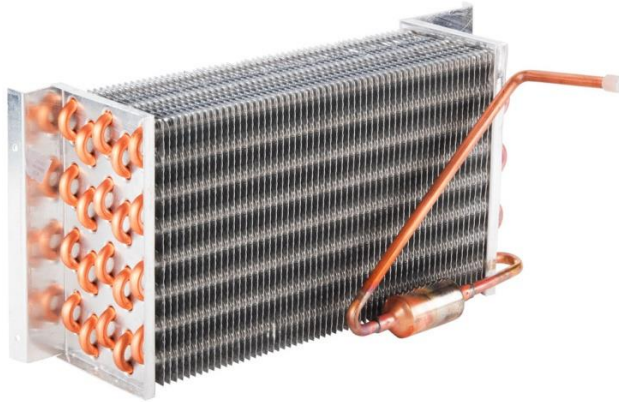
Homogeneous  
Flow?

$\Delta p$ ?

Condenser



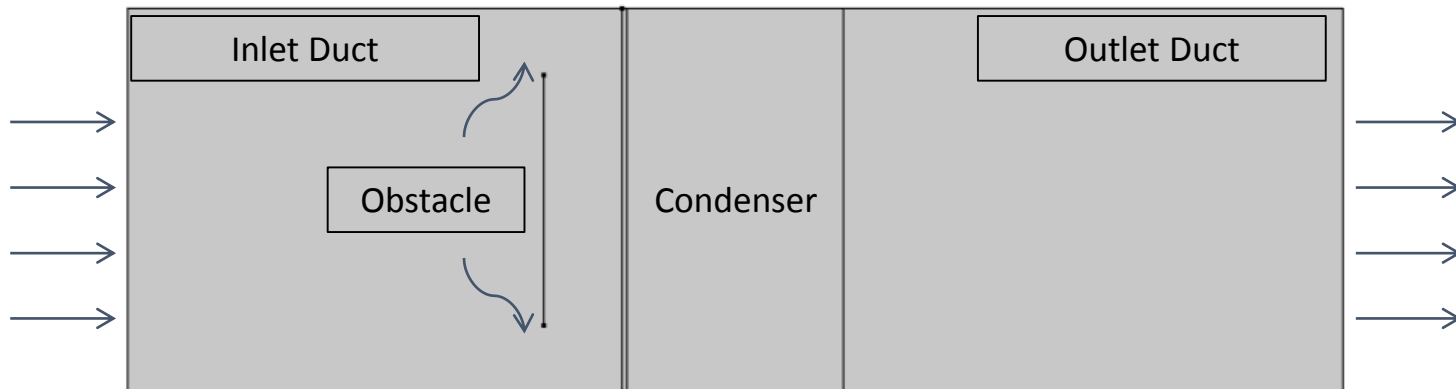
# Modeling of the Condenser



~~Complex geometry  
=  
>10<sup>6</sup> Mesh elements~~

1. Pressure drop
2. Fins effect

## Model Calibration (COMSOL®)



# Condenser – “Porous Model”

Brinkman equations

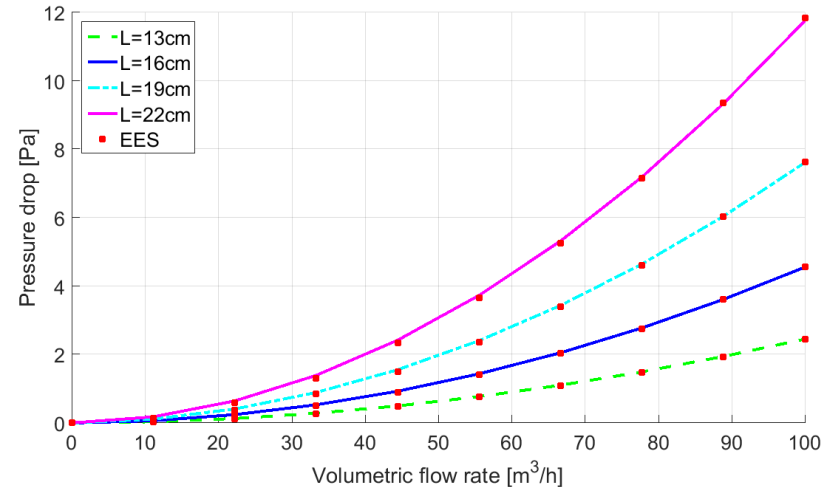
$$\frac{1}{\varphi} \left( \frac{\partial \bar{u}_i}{\partial t} + u_j \frac{\partial \bar{u}_i / \varphi}{\partial x_j} \right) = -\frac{1}{\rho_0} \frac{\partial P}{\partial x_i} + \frac{\partial}{\partial x_j} \left[ \frac{\nu}{\varphi} \left( \frac{\partial \bar{u}_i}{\partial x_j} + \frac{\partial \bar{u}_j}{\partial x_i} \right) \right] + \frac{1}{\rho_0} F_i$$

Pressure drop

$$F_i = - \left( \sum_{j=1}^3 \frac{\mu}{K_{ij}} u_j + \sum_{j=1}^3 \frac{C_F \rho}{\sqrt{K_{ij}}} |u| u_j \right)$$

$$\frac{\Delta P}{L} = a \cdot |u| + b \cdot |u|^2$$

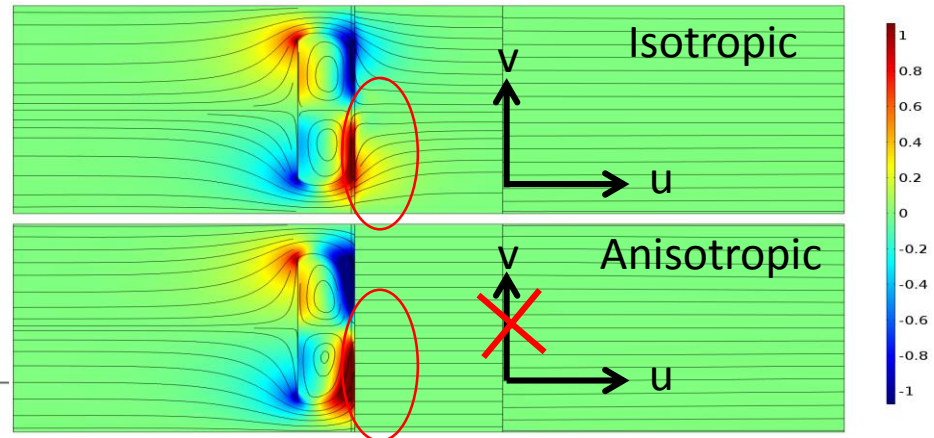
EES: Engineering Equation Solver



Modelling of the fins

$$K = \begin{pmatrix} K_{xx} & K_{xy} & K_{xz} \\ K_{yx} & K_{yy} & K_{yz} \\ K_{zx} & K_{zy} & K_{zz} \end{pmatrix}$$

$$K_{xx} \gg K_{yy} \Rightarrow u \gg v$$

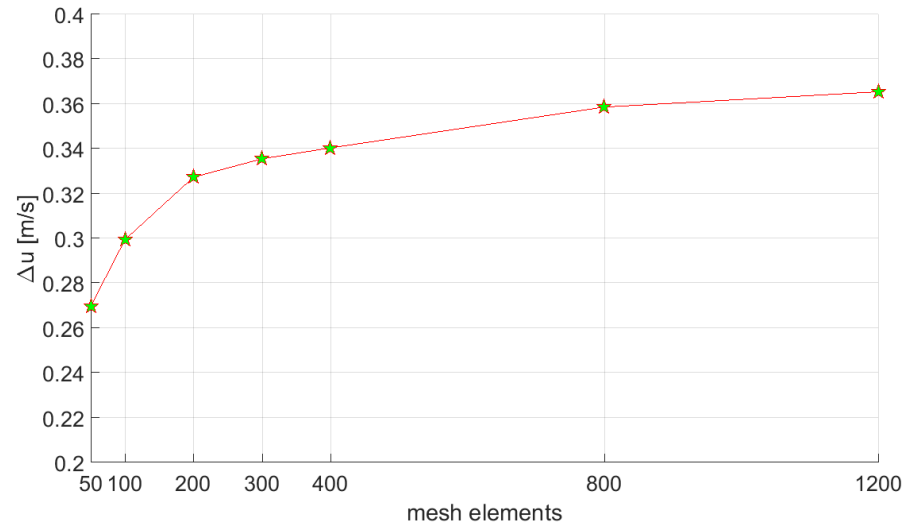
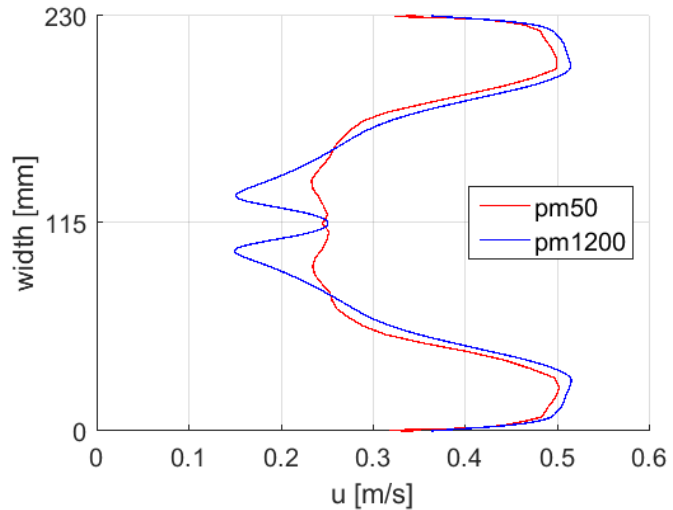


# Mesh Optimization

Pressure drop

$\Delta P$ : max. error = 0.08%

Velocity profile at the condenser's inlet



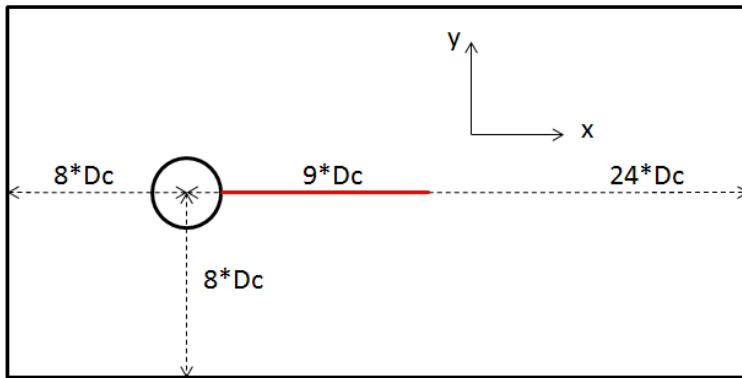
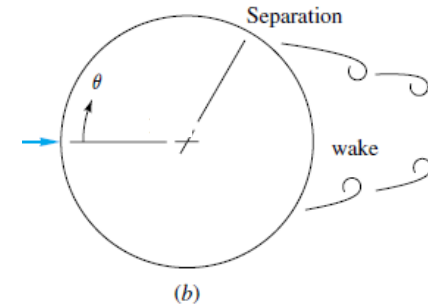
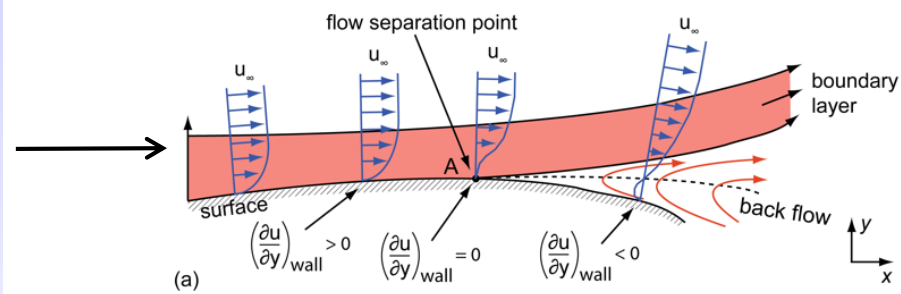
$\Delta u$ : max. error = 40%

# Turbulence Models

COMSOL®: turbulent flow



Compressor:  $Re_D = 2500$



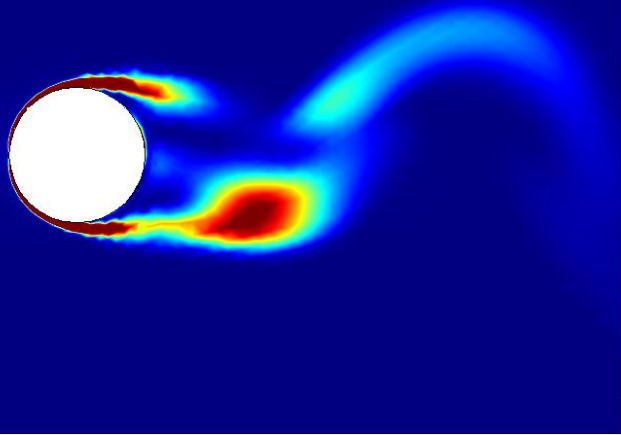
Benchmark:

*Schiller-Linke* → transitional boundary layer

# Turbulence Models – Transition

Standard k- $\epsilon$

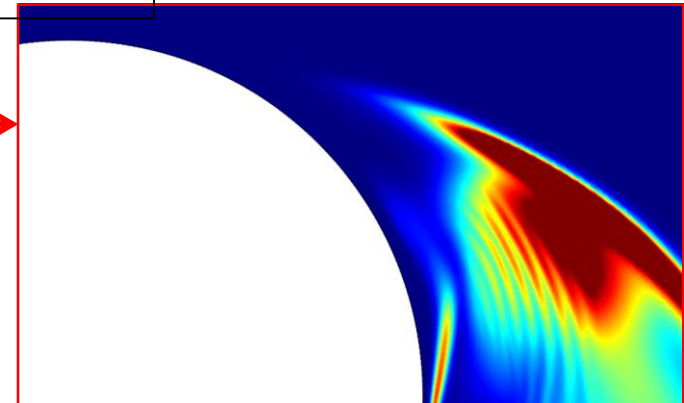
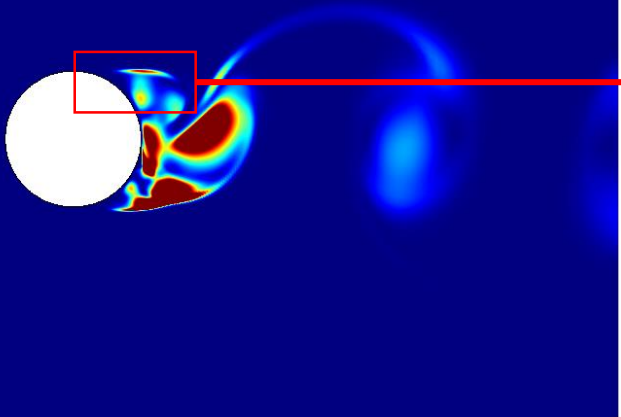
High-Reynolds-Number  
Model



Turbulent kinetic energy  
production  
[W/m<sup>3</sup>]

A-K-N k- $\epsilon$

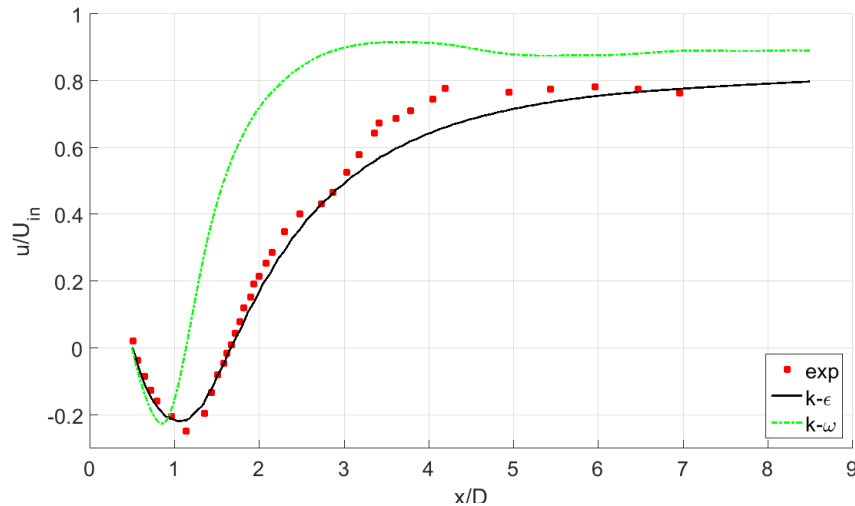
Low-Reynolds-Number  
Model



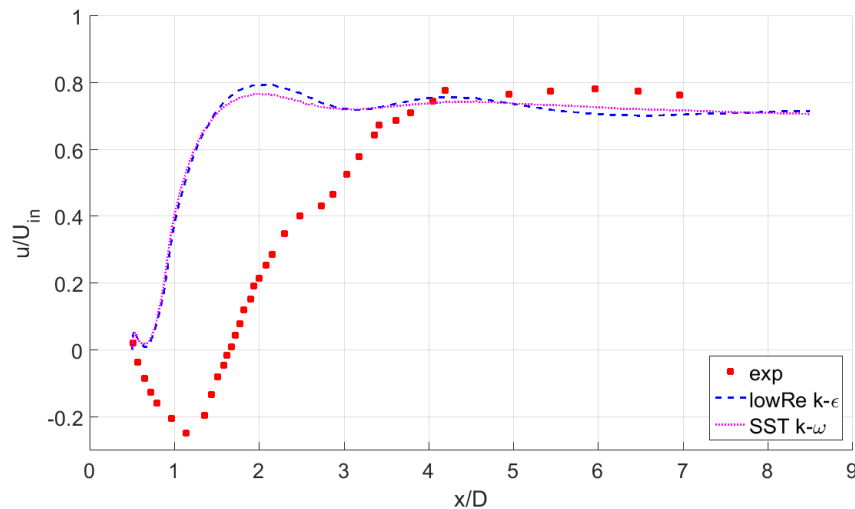


# Turbulence Model – Recirculation Length

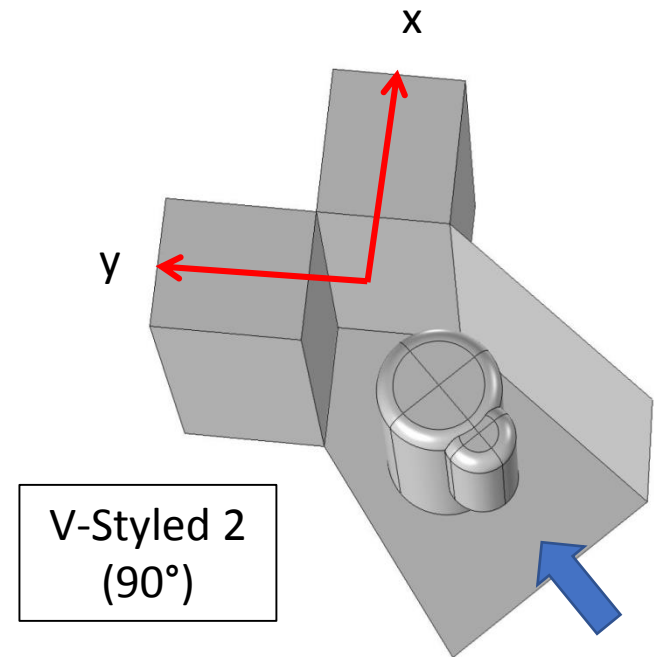
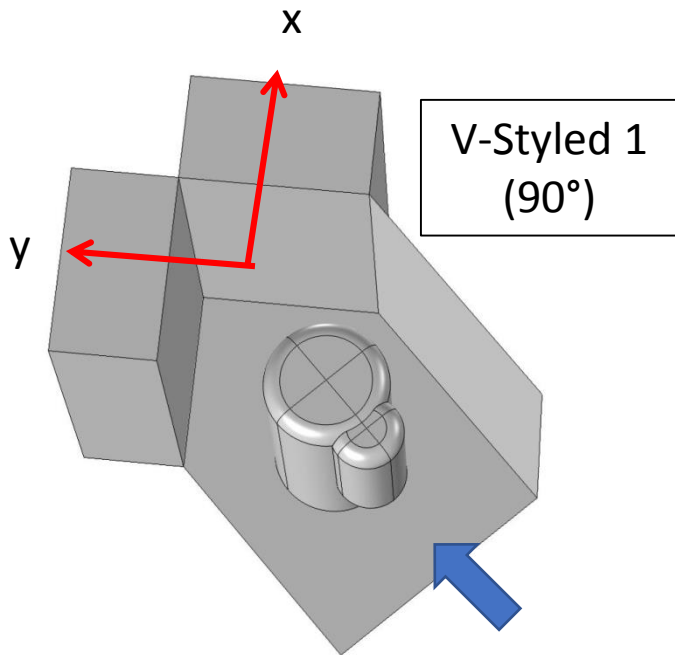
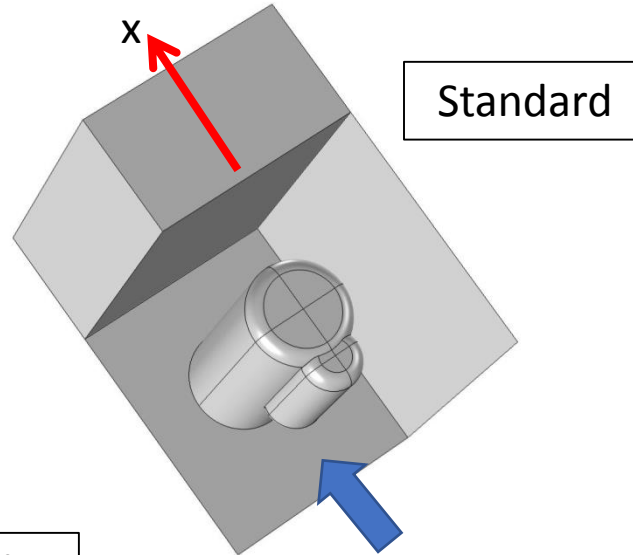
High-Reynolds-Number  
Models



Low-Reynolds-Number  
Models



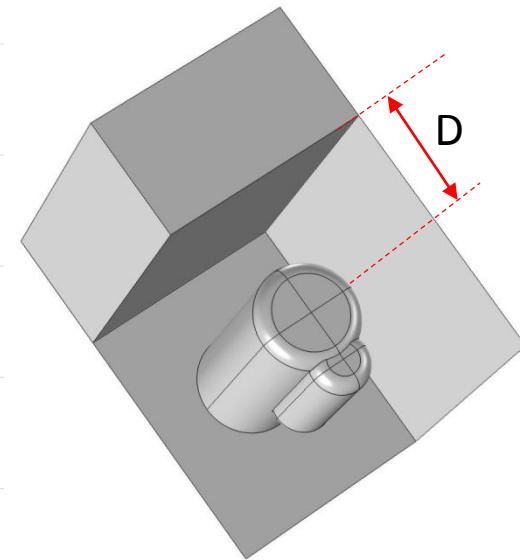
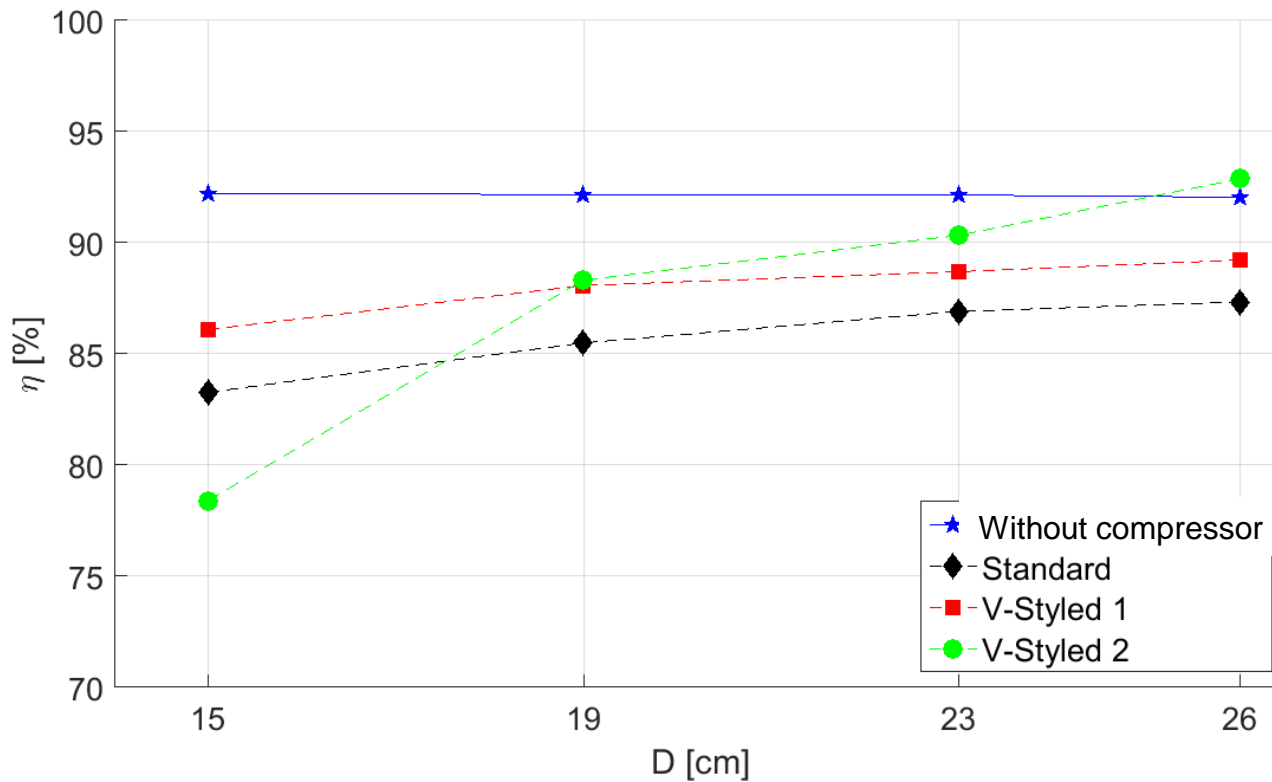
# Optimization – Investigated variants



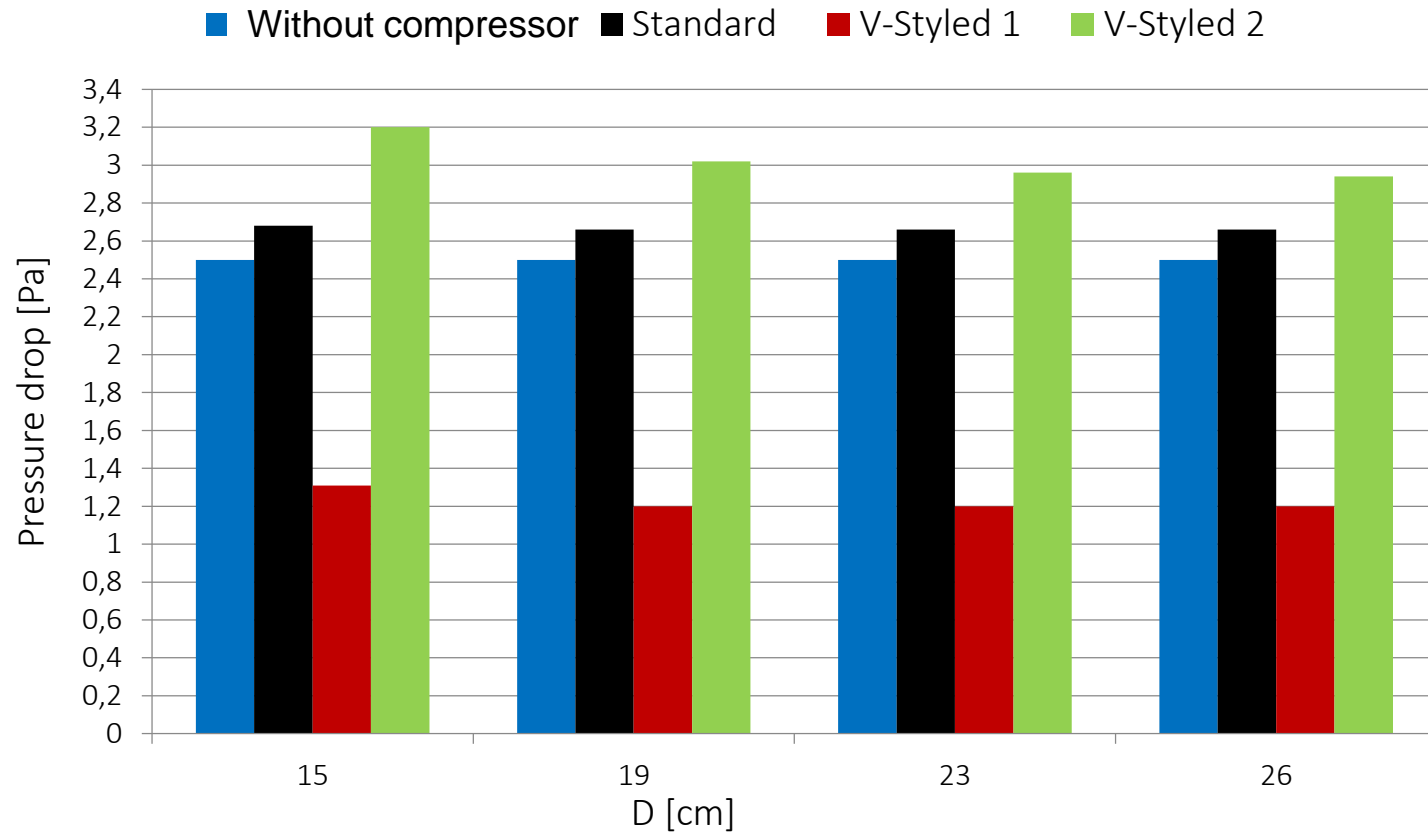
# Optimization – Flow Homogeneity

$$\eta(u) = 100 - \left( \frac{s_N}{u_{mean}} \right) \cdot 100$$

$$s_N = \sqrt{\frac{\sum_i^N (u_i - u_{mean})^2}{N}}$$



# Optimization – Pressure Drop



# Conclusions

1. "Porous" Model:
  - Low computational cost
  - correct pressure drop prediction
  - velocity profile very sensitive to the mesh quality
1. Turbulence models: Turbulent viscosity vs. transitional flow
2. Optimization: V-styled condensers > Lower pressure drop with the "large" inlet duct (V-Styled 1)

# Future Work

1. Validation of the "Porous" Model via CFD simulation of the flow through the heat exchanger
2. Validation of the models through comparison with 3D- benchmarks

**Thank you for your attention**