Force and Torque Predictions in a Large-Gap Magnetic Suspension System

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INTRODUCTION: Wind tunnel Magnetic Suspension and Balance Systems (MSBS) are an example of "largegap" suspensions, where a small ferromagnetic core is well separated from relatively large electromagnets producing the levitation fields¹. The systems are openloop unstable (require feedback control), so accurate prediction of forces and moments as a function of electromagnet currents is important.



Figure 1. ODU/NASA "6-inch" MSBS

THEORETICAL BACKGROUND: The forces and moments on a permanent magnet can be derived from volume integrals, or by integrals of the Maxwell stress tensor over virtual or physical surfaces². The latter technique must be applied with care as the integrand exhibits sharp peaks at physical corners but is more general.

$$F = \mu_0 \iiint (\boldsymbol{M} \cdot \nabla \boldsymbol{H}) dV ; T = \mu_0 \iiint (\boldsymbol{M} \times \boldsymbol{H}) dV$$
$$\frac{dF}{dS} = -\frac{\mu_0}{2} \boldsymbol{H}^2 \hat{\boldsymbol{n}} + \mu_0 (\boldsymbol{H} \cdot \hat{\boldsymbol{n}}) \boldsymbol{H}$$

COMSOL's formulation differs but is equivalent. The volume integrals can be evaluated from fields with the magnetic core removed. Virtual work methods cannot be used, since the system's stored energy is very large, but the forces of interest are quite small³.

COMPUTATIONAL METHODS: Calculations herein rely on the steady magnetic field interface (mf). The reference electromagnet geometry is depicted in Figures 2 & 3, with an example of fields and the distribution of Maxwell stress over a levitated core shown in Figure 4. The magnetization direction is vertical, and the applied fields produce a force in the xdirection, which is transverse to the cylinder axis. Improved accuracy appears possible by introduction of a control surface surrounding the core, a cube with sides 2 times the core diameter in this case.



Figure 2. Electromagnet Assembly

Figure 3. Magnet Surface Mesh





Figure 4. Field and Maxwell Stress Distribution over Magnetic Core

Figure 5. Control Volume (example - cube)

| Case | Fx (N) |
|---|--------|
| Analytic evaluation at centroid | 24.870 |
| Analytic evaluation, 2nd order integration | 24.591 |
| COMSOL fine grid (user-controlled, general physics) | 24.213 |
| Add boundary layer elements (4 layers) | 25.118 |
| Cubic control volume, L=2D | 24.215 |

 Table 1. Summary of Force Estimates

RESULTS: Scatter in results between different evaluations is of the order of $\pm 2\%$, marginally inadequate for the current work. A more complete analysis will determine criteria for choice of grid refinement, control volume shape/size, etc.

CONCLUSIONS: Accurate force calculations for this type of configuration are challenging. Results are sensitive to grid refinement owing to the peaks of the Maxwell stress integrand at physical edges. Integration over surrounding control volumes may be superior. Best accuracy is a topic of further study.

REFERENCES:

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